

Produced Water Pilot Project Notice of Intent to Discharge

For Department Use Only:

Agency Interest Number	
PRD Assigned	

Ga	ge Herrmann	Work Phone: (432) 288-4622
901	1 W Missouri Ave	Cell/Home Phone: (432) 288-4622
Mi	dland TX, 79701	Fax:
_		Email: gherrmann@tascosaep.com
2.	Name and position of person completing form:	
G	age Herrmann – Midstream Manager	Work Phone: (432) 288-4622
		Cell/Home Phone: (432) 288-4622
		Fax:
		Email: gherrmann@tascosaep.com
3. 4.	Research Focus (PWRC Research Category): Is the proposed use of the treated produced wate industry? Inside	er to be used inside or outside of the oil and gas
5.	Does the location for testing the technology take	place inside or outside of the oil and gas field? Inside
6.	Physical location of the research site including si township, range, section, county, distance from county as an attachment.	ze and boundaries of site (include, street address, closest town or landmark, directions to facility.
7.	Topographic and aerial map(s) showing: (please s	see attached)
	 land status and adjacent land status 100-year flood plain, 	
	 dwellings and occupied establishme 	
		ches, wetlands, lakes, karst and soils
	 water wells (types) or springs site security 	
	site plan showing locations of relevant	nt structures
8.	List any regulatory, governmental and non-governmental and non-governmental have authority on the testing location. Provide	nmental agencies, including municipalities or counties de as an attachment.
9.	Provide a description of your signage plan for the	e testing site. Provide as an attachment.
10.	Provide a description of your site security plan, in	ncluding training and site restriction methods.
11.	See attached List of adjacent landowners and confirmation tha proposed pilot project. Provide as an attachment	
12.		g basin of origin. Describe how the produced water will in and disposal locations and onsite storage safety

precautionary methods. Provide as an attachment.

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New Mexico Environment Department Ground Water Quality Bureau

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Produced Water Treatment Pilot Project Background Information

For Use in NMED Treatment Permit Discussions 2023

1. Applicant Summary Information:

Company: (Tascosa Energy Partners LLC, 901 W Missouri Ave, Midland TX 79701)

Points of Contact	Company	Email	Phone
Alyssa Davanzo	Tascosa Energy Partners	adavanzo@tascosaep.com	(720) 244-4417
Gage Herrmann Tascosa/Reprise		gage@pearlwm.com	(432) 288-4622

Company Description and Produced Water Treatment Experience:

Tascosa Energy Partners, LLC is an established exploration and production company located in Midland, Texas. Founded in 2018, TEP, is focused on maximizing value for our partners and growing the company through accretive acquisitions and drilling. Our leadership team takes great pride building a strong reputation and continues to develop exploration and production technologies

Application Date: 4/13/2023

Pilot Date: 5/1/2023

Type and scale of Project: (Bench-scale/Pilot-scale)

Project Funding: (Private Funded)

Project Collaborators: (if any)

Group/Company	Role	Contact Info
Hydrozonix	Supplier/Advisor	Mark Patton - mpatton@hydrozonix.com
Reprise Midstream	Advisor/Operations	Gage Herrmann – gage@pearlwm.com

2. Project Site Location and Description:

• Basin: Delaware

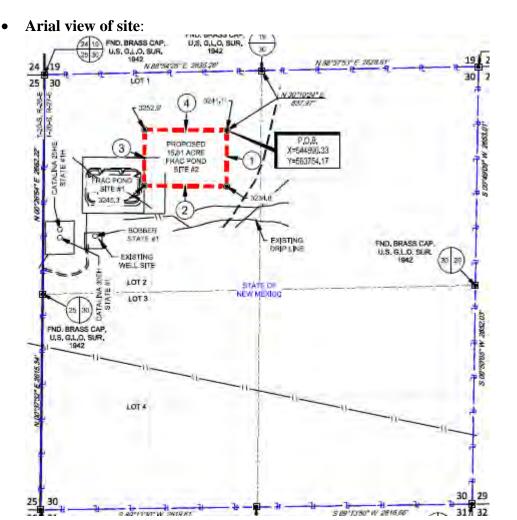
• **Location**: (From Carlsbad NM head W on Hwy 285 N for 11.1 Miles, turn right onto Capitan Reef Rd and continue for 3.9 miles then turn right and continue for 1.6 miles then turn right and continue for 0.3 miles then turn left and continue for 0.7 miles) **Coordinates:** (32.546820, -104.32684)

- **General Directions**: (From Carlsbad NM head W on Hwy 285 N for 11.1 Miles, turn right onto Capitan Reef Rd and continue for 3.9 miles then turn right and continue for 1.6 miles then turn right and continue for 0.3 miles then turn left and continue for 0.7 miles)
- **Site Description**: (Catalina Containment and Recycling Facility Addition of Containment #2 to 2RF-157)
- Land Status: (New Mexico State)



Produced Water Treatment Pilot Project Background Information

For Use in NMED Treatment Permit Discussions 2023



• **Produced Water Source and Quality**: (Please see attached water analysis)

3. Executive Summary:

(Tascosa Energy Partners would like to install the Hydrozonix Smart Evaporation System at their Catalina Recycling Facility in Eddy County NM)

4. Proposed Reuse Application of Treated Water: (following statement required)

For the purposes of this test, there will be no discharge of the produced water. The distillate will be collected in a holding tank for sampling before being blended back with the concentrated brine for reinjection into the SWD.

5. Similar or related permits/notification needed with other agencies, or nearby properties:

(The closest nearby operator is Mewbourne and they are already aware of the project)



Produced Water Treatment Pilot Project Background Information

For Use in NMED Treatment Permit Discussions 2023

6. Pilot-System Process and Design: Please see attached "SMART Pilot Application" from Hydrozonix

7. Project Goals and Objectives: (Summary of objectives and KPI's similar to below) Feed water analysis attached*

The pilot project is expected to operate for up to '520' weeks, treating up to '14,000' bbls/day of produced water of a water quality compatible with reuse for frac water. It is expected the concentrate and distillate will have the following beginning and final qualities.

Additionally, (i.e. solids and ammonia recovery will be evaluated for economic reuse of those recovered minerals). The following Key Performance Indicators (KPI's) will be evaluated to assess system and process cost effectiveness and overall performance:

Operational throughput - 500 bbls/hr
Operational efficiency - 19 hrs/day
Downtime - 34 average hrs/wk
Meet water quality target - NA % of time
Max. water quality variation - NA average % above target level
Energy use/cost per bbl treated - x kwh/bbl, x btu/bbl, and \$x/bbl TBD
Treatment vs pre and post treatment costs of operation - y in % NA
Distillate and concentrate revovery - xaverage bbls/bbls treated TBD
Mineral recovery - x tons per day per bbls treated TBD
(Additional KPI's as required)

The data collected will be utilized to help develop of design of larger-scale treatment systems to support enhanced operations efficiencies and reduce full-scale treatment costs.

8. Summary of Risk and Toxicology Sampling, Testing, and Analysis: (Following Statement Required)

The KPI's noted above will be measured daily on-site with simple field testing systems and monitors.

Risk and Toxicology testing and analysis of thee treated produced water will be coordinated and managed through the NMPWRC. Samples will be taken and tested using the Consortium's sampling protocol, and their Risk and Toxicology testing protocol. Bechtel will coordinate with the NMPWRC so they can to collect and prepare Risk and Toxicology analysis samples to ensure proper care, custody, and control. The Consortium will collect up to two set of samples once routine operations have been established to provide information on process efficacy and reliability relative to potential future treated water safety.



Produced Water Treatment Pilot Project Background Information

For Use in NMED Treatment Permit Discussions 2023

9. Equipment Vendor and Associated Suppliers: (Identify as appropriate)

Equipment or Vendor Name/Description	Role	
Hydrozonix	Equipment Supplier and Advisor	
Reprise Midstream	Advisor and Evaporation System Operations	

10. Expected Produced Water Users: (Required Statement)

The effluent for the pilot operations will be recombined and placed in an SWD and residuals disposed as noted below.

11. Disposal and Decommissioning: (Required information)

Equipment: None - Reuse for testing at other sites

Material: Secondary containment and expendables for the treatment system will be......

Water: All water will be disposed by ie SWD injection

Soil: Any contaminated soil will be disposed at the following permitted

12. Expected Operational Testing, Reporting, and Proposed Review Schedule

Pilot mobilization, set up, and shakedown: April-May 2023

Pilot Operations: 2023-2028

Draft Report: TBD

Company POC Date 4/14/2023

Pilot System Process and Design

SMART Evaporation is a patent pending technology that uses specialized nozzles that limit mist drift. A control system monitors real time humidity, wind speed, wind direction, temperature, and flow rate. Flow rate controls droplet size which with all of the other parameters control mist drift and salt drift. The operating system uses a formula that controls drift.

Figure 1: Mist Modeling

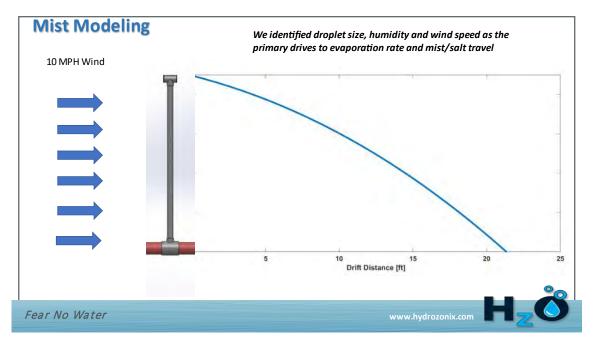


Figure 2: Spray Nozzle Pat ern and Drift

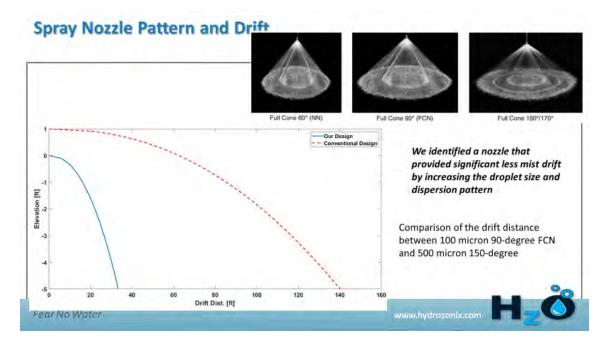


Figure 3: Working Conditions

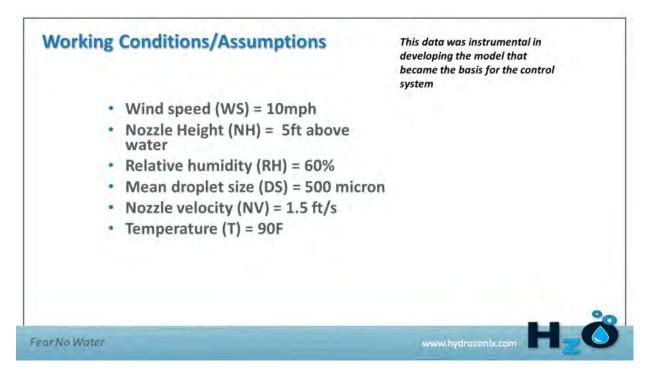
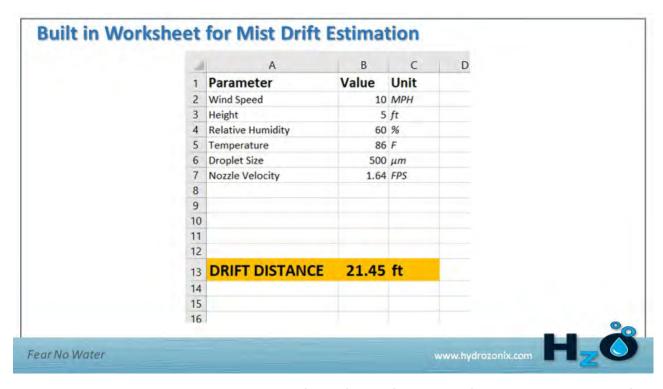


Figure 4: Mist Drift Calculation



This proprietary control system calculates the drift and if the drift distance is farther than the distance of the modules to the edge of the pit the systems shuts off.

The system is configured using multiple square modules. The number of modules is limited by the surface area of the pit. A minimum distance is required between the modules and the edge of the pit to allow mist and slat to drop out in the pit.

Figure 5 Module Design

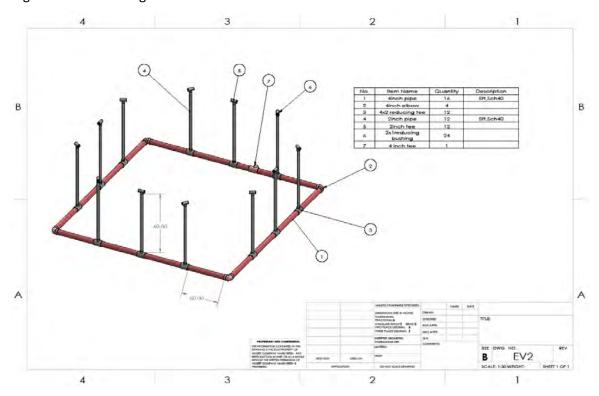


Figure 6: Sample Layout in a Pit

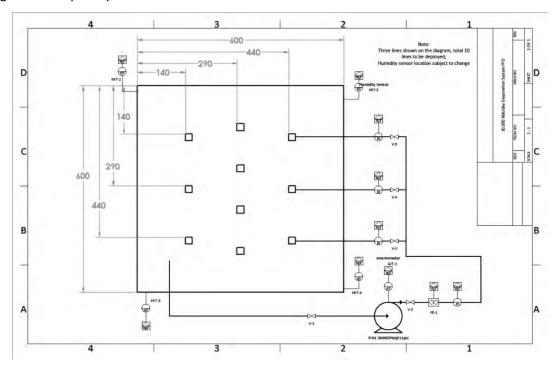


Figure 7: Control System with Modules

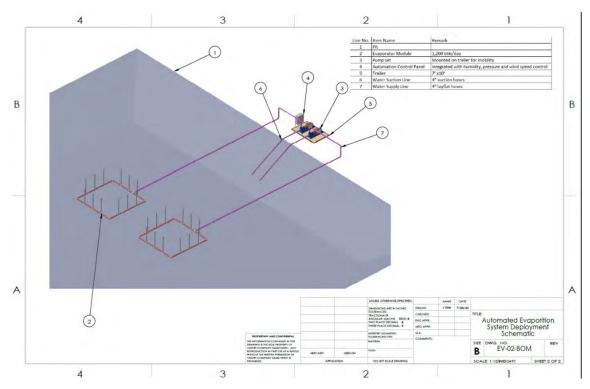
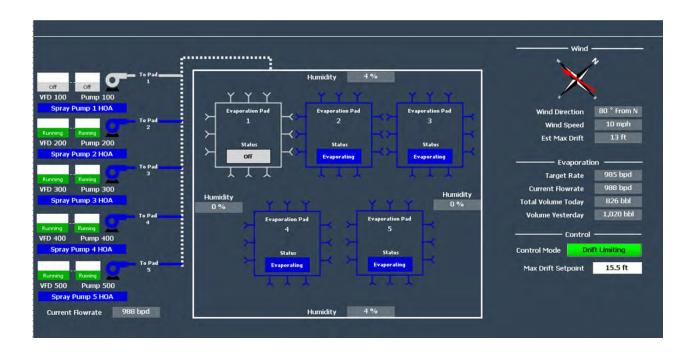


Figure 8: Automated Control System



The entire SMART evaporation system is fully automated while collecting real time data for continuous review. The data is data logged in a cloud based storge program.

Expected Operational and Proposed Review Schedule

Pilot Mobilization, set up and shakedown.

Mobilization will commence within 7 days of notice to proceed. Days 1-3 will be for set-up and shakedown.

Pilot Operation

Pilot operation will commence on day 4 after mobilization

Draft Report

At 30 days a draft report will be compiled and be available to all appropriate stakeholders.

C-147 Registration/Modification for Catalina Containment and Recycling Facility Addition of Containment #2 to 2RF-157 Section 30, T20S, R27E, Eddy County

Volume 1

Transmittal Letter C-147 Survey Stamped Design Drawings and Specifications Design/Construction, O&M, and Closure Plans



View south showing Catalina Containment #1 on the right just below the horizon. Catalina Containment #2 is proposed to the east (left) of Containment #1. The line of vegetation below the horizon is the mis-mapped USGS intermittent stream that is described in this registration.

Prepared for: Tascosa Energy LLC Midland, Texas

Prepared by: R.T. Hicks Consultants, Ltd. 901 Rio Grande NW F-142 Albuquerque, New Mexico

R. T. HICKS CONSULTANTS, LTD.

901 Rio Grande Blvd NW ▲ Suite F-142 ▲ Albuguergue, NM 87104 ▲ 505.266.5004 ▲ Since 1996

June 22, 2022

Mr. Mike Bratcher NMOCD District II 811 S. First St. Artesia, NM 88210 Via E-Mail Ms. Victoria Venegas NMOCD District II 811 S. First St. Artesia, NM 88210 Via E-Mail

RE: Tascosa Energy Partners, Catalina Recycling Facility and Containment Modification Addition of Containment #2 to 2RF-157 Section 30 T20S R27E, Eddy County

Dear Mr. Bratcher and Ms. Venegas:

On behalf of Tascosa Energy Partners, Hicks Consultants is pleased to submit the C-147 Modification for the above-referenced project. Rule 34 requires no variances for the containment. Specifically,

- Tascosa will install a 4-strand barbed wire fence over the proposed game fence to comply with the specific language of the Rule if requested by the District Office,
- The 40-mil HDPE secondary liner is "equivalent with a hydraulic conductivity no greater than 1 x 10-9 cm/sec" and meets or exceeds the "EPA SW-846 method 9090A or subsequent relevant publications" and is therefore consistent with the criteria of the Rule,
- The Mega Blaster Pro Sonic Bird Repeller "is otherwise protective of wildlife, including migratory birds" and is therefore consistent with the criteria of the Rule,
- In compliance with 19.15.34.10, the C-147 is copied to the surface owner, the State of New Mexico.
- All of these design features were accepted by OCD for the Catalina #1 registration

As attested in the Catalina #1 registration, I affirm as a Professional Geologist with more than 30 years of experience with NMOCD permits, hearings, rulemaking, and field work in the Permian Basin of New Mexico, that the siting criteria demonstration is consistent with the Rule and the location meets the specified siting criteria. Volume 2 of this submission states:

- The containment lies within an area mapped by the BLM as high karst potential. The 2020 registration addressed the potential of unstable ground in detail and the discussion in this modification is provided verbatim.
- In 2020 and 2022, we examined several channels that do or could drain to the mapped watercourse south of the Containments. We determined no channels, including the USGS mapped watercourse, meet the NMOCD definition of a watercourse. In the Pleistocene, when the climate was quite different than today, the USGS mapped channel may have exhibited a bed and bank.
- Erosional channels within an active alluvial fan uphill (north) of Containment #2 do not exist within 400 feet of Containment #2 as all flow infiltrates below the break in slope between the alluvial fan and the broad alluvial valley to the south.

June 22, 2022 Page 2

The Design/Construction Plan, Operation and Maintenance Plan and Closure Plan are consistent with the Rule. Unless instructed by OCD, we will employ the analytical tests for closure listed in the Rule.

Please contact me if you have any questions or concerns.

Sincerely,

R.T. Hicks Consultants

Randall Hicks, PG

Principal

Copy: Tascosa Energy Partners LLC

State Land Office

C-147

<u>District I</u> 1625 N. French Dr., Hobbs, NM 88240 District II
811 S. First St., Artesia, NM 88210
District III 1000 Rio Brazos Road, Aztec, NM 87410 District IV 1220 S. St. Francis Dr., Santa Fe, NM 87505

State of New Mexico **Energy Minerals and Natural Resources** Department Oil Conservation Division 1220 South St. Francis Dr.

Form C-147 Revised April 3, 2017

Santa Fe, NM 87505

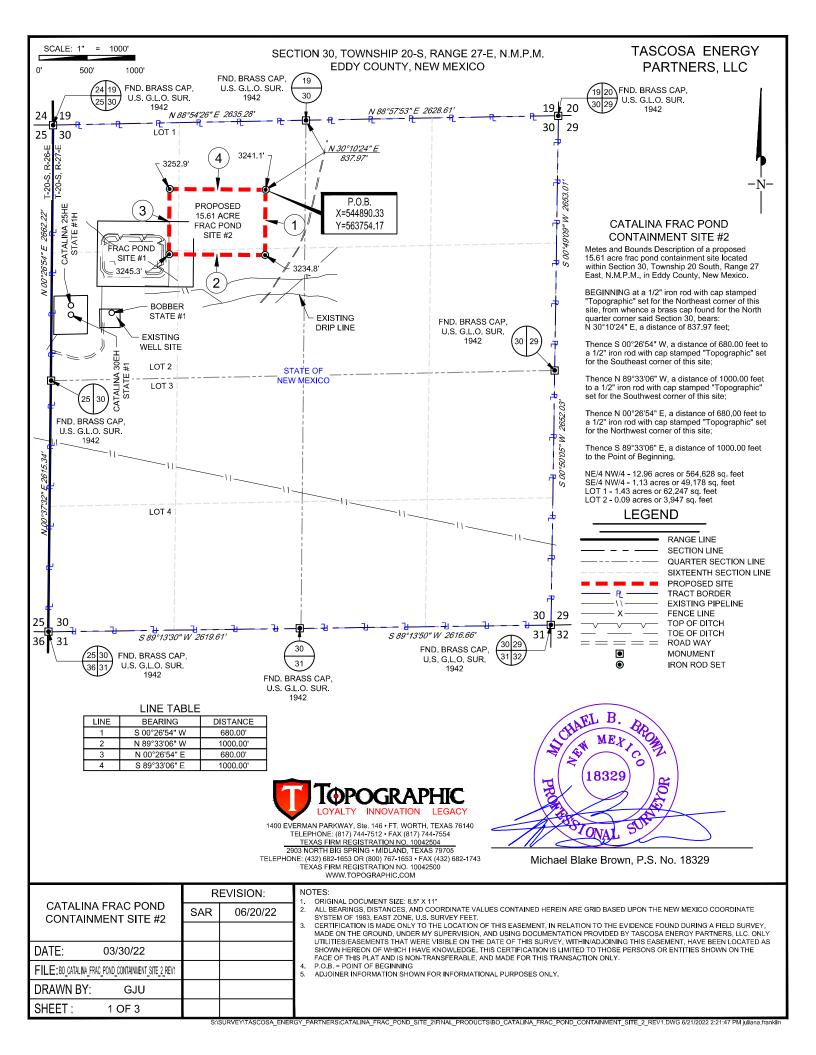
Recycling Facility and/or Recycling Containment			
Type of Facility: Recycling Facility Recycling Containment*			
Type of action: ☐ Permit ☐ Registration			
Modification Extension			
Closure Other (explain)			
At the time C-147 is submitted to the division for a Recycling Containment, a copy shall be provided to the surface owner.			
e advised that approval of this request does not relieve the operator of liability should operations result in pollution of surface water, ground water or the environment. or does approval relieve the operator of its responsibility to comply with any other applicable governmental authority's rules, regulations or ordinances.			
1. Operator:			
Address: 901 W. Missouri, Midland, Texas 79701			
Facility or well name (include API# if associated with a well):			
OCD Permit Number:(For new facilities the permit number will be assigned by the district office)			
U/L or Qtr/Qtr C, D Section30 _ Township20S _ Range27E County:Eddy			
Surface Owner: ☐ Federal ☐ State ☐ Private ☐ Tribal Trust or Indian Allotment			
2.			
Recycling Facility:			
Location of (if applicable): Latitude 32.546820, -104.32684 Longitude .			
Proposed Use: ☐ Drilling* ☐ Completion* ☐ Production* ☐ Plugging *			
*The re-use of produced water may NOT be used until fresh water zones are cased and cemented			
Other, requires permit for other uses. Describe use, process, testing, volume of produced water and ensure there will be no adverse impact on			
groundwater or surface water.			
☐ Fluid Storage			
Activity permitted under 19.15.36 NMAC explain type: Other explain			
For multiple or additional recycling containments, attach design and location information of each containment			
Closure Report (required within 60 days of closure completion): Recycling Facility Closure Completion Date:			
3.			
Recycling Containment: Two (2) in-ground containments			
Annual Extension after initial 5 years (attach summary of monthly leak detection inspections for previous year)			
Center of Recycling Containment (if applicable) Pond Lat 32.549018 Long -104.3230528 (approx.) NAD 83			
For multiple or additional recycling containments, attach design and location information of each containment			
☐ Liner type: Thickness <u>Secondary 40 mil Primary 60- mil</u> LLDPE ☐ HDPE ☐ PVC ☐ Other			
☐ String-Reinforced			
Liner Seams: Welded Factory Other Volume: Dimensions <u>See Attachment</u> 1			
Recycling Containment Closure Completion Date:			

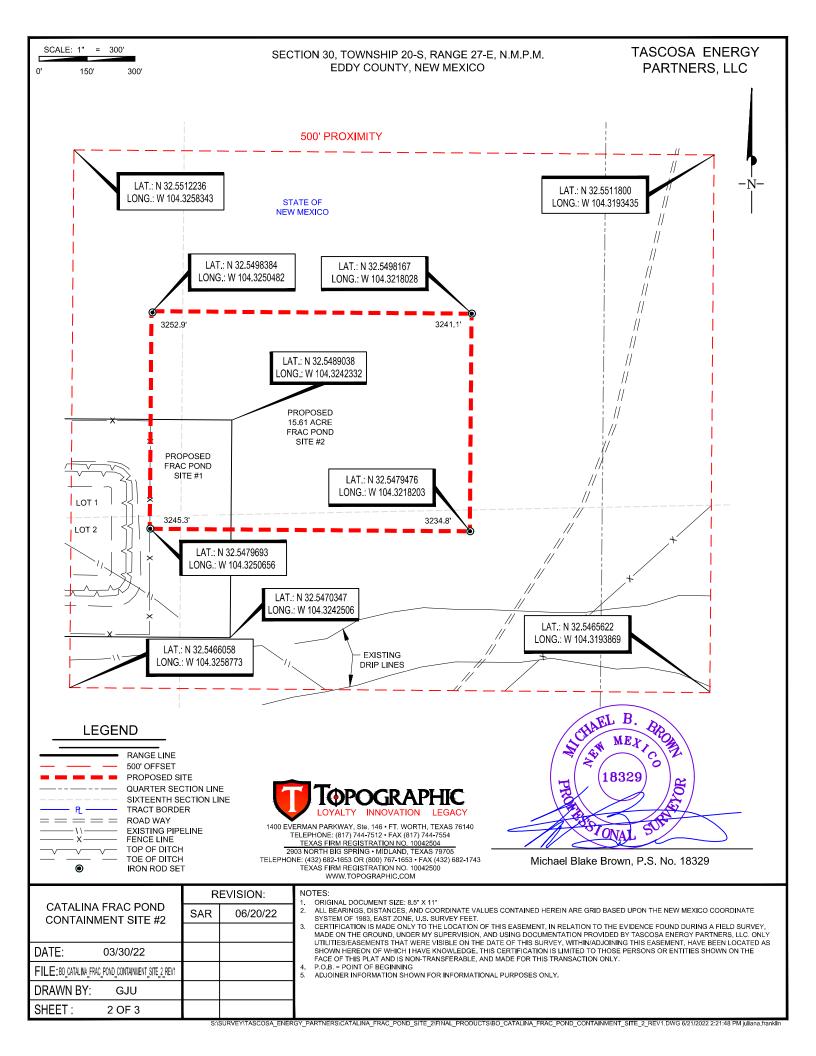
4. Bonding:			
 \text{Sovered under bonding pursuant to 19.15.8 NMAC per 19.15.34.15(A)(2) NMAC (These containments are limited to only the wells owned or \overline{\text{Sovered under bonding pursuant to 19.15.8 NMAC per 19.15.34.15(A)(2) NMAC (These containments are limited to only the wells owned or \overline{\text{Sovered under bonding pursuant to 19.15.8 NMAC per 19.15.34.15(A)(2) NMAC (These containments are limited to only the wells owned or \overline{\text{Sovered under bonding pursuant to 19.15.8 NMAC per 19.15.34.15(A)(2) NMAC (These containments are limited to only the wells owned or \overline{\text{Sovered under bonding pursuant to 19.15.8 NMAC per 19.15.34.15(A)(2) NMAC (These containments are limited to only the wells owned or \overline{\text{Sovered under bonding pursuant to 19.15.8 NMAC per 19.15.34.15(A)(2) NMAC (These containments are limited to only the wells owned or \overline{\text{Sovered under bonding pursuant to 19.15.8 NMAC per 19.15.34.15(A)(B) NMAC (These containments are limited to only the wells owned or \overline{\text{Sovered under bonding pursuant to 19.15.8 NMAC per 19.15.34.15(A)(B) NMAC			
operated by the owners of the containment.)			
☐ Bonding in accordance with 19.15.34.15(A)(1). Amount of bond \$_See Transmittal Letter (work on these facilities cannot common the common transmittal Letter (work on these facilities cannot common transmittal Letter (work on the common transmittal Letter (wo	nence until		
bonding amounts are approved)			
Attach closure cost estimate and documentation on how the closure cost was calculated.			
5.			
Fencing:			
☐ Four-foot height, four strands of barbed wire evenly spaced between one and four feet			
Alternate. Please specify:_and game fence to protect terrestrial wildlife			
6.			
<u>Signs</u> :			
🛛 12"x 24", 2" lettering, providing Operator's name, site location, and emergency telephone numbers			
☐ Signed in compliance with 19.15.16.8 NMAC			
7.			
<u>Variances:</u>			
Justifications and/or demonstrations that the proposed variance will afford reasonable protection against contamination of fresh water, he the environment.	uman health, and		
Check the below box only if a variance is requested:			
☐ Variance(s): Requests must be submitted to the appropriate division district for consideration of approval. If a Variance is request variance information on a separate page and attach it to the C-147 as part of the application.	ted, include the		
If a Variance is requested, it must be approved prior to implementation.			
8. Siting Criteria for Recycling Containment			
Instructions: The applicant must provide attachments that demonstrate compliance for each siting criteria below as part of the applicate examples of the siting attachment source material are provided below under each criteria.	ntion. Potential		
General siting			
Ground water is less than 50 feet below the bottom of the Recycling Containment. NM Office of the State Engineer - iWATERS database search; USGS; Data obtained from nearby wells FIGURES 1-2	☐ Yes ⊠ No ☐ NA		
Within incorporated municipal boundaries or within a defined municipal fresh water well field covered under a municipal ordinance	□ v □ n.		
adopted pursuant to NMSA 1978, Section 3-27-3, as amended.	☐ Yes ☑ No ☐ NA		
- Written confirmation or verification from the municipality; written approval obtained from the municipality FIGURE 3			
Within the area overlying a subsurface mine. - Written confirmation or verification or map from the NM EMNRD-Mining and Minerals Division FIGURE 4	☐ Yes ⊠ No		
Within an unstable area.			
 Engineering measures incorporated into the design; NM Bureau of Geology & Mineral Resources; USGS; NM Geological Society; topographic map FIGURE 5 	☐ Yes ⊠ No		
Within a 100-year floodplain. FEMA map FIGURE 6	☐ Yes ⊠ No		
Within 300 feet of a continuously flowing watercourse, or 200 feet of any other significant watercourse, or lakebed, sinkhole, or playa	☐ Yes ⊠ No		
lake (measured from the ordinary high-water mark). - Topographic map; visual inspection (certification) of the proposed site FIGURE 7			
Within 1000 feet from a permanent residence, school, hospital, institution, or church in existence at the time of initial application. - Visual inspection (certification) of the proposed site; aerial photo; satellite image FIGURE 8	☐ Yes ⊠ No		
Within 500 horizontal feet of a spring or a fresh water well used for domestic or stock watering purposes, in existence at the time of	☐ Yes ⊠ No		
initial application. FIGURES 1 and 7			
- NM Office of the State Engineer - iWATERS database search; visual inspection (certification) of the proposed site			
Within 500 feet of a wetland. FIGURE 9 US Fish and Wildlife Wetland Identification map; topographic map; visual inspection (certification) of the proposed site	☐ Yes ⊠ No		

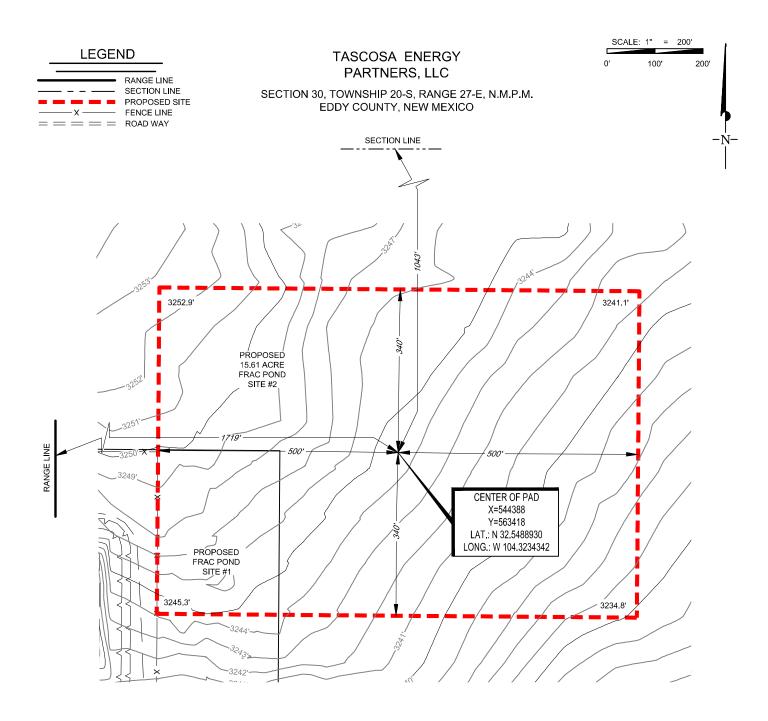
9. Recycling Facility and/or Containment Checklist: Instructions: Each of the following items must be attached to the applications:	cation. Indicate, by a check n	nark in the box, that the documents are attached.
Desire Blow based among the among price acquirements		
 Design Plan - based upon the appropriate requirements. Operating and Maintenance Plan - based upon the appropriate requ 	irements	
Closure Plan - based upon the appropriate requirements.	memens.	
Site Specific Groundwater Data -		
☑ Certify that notice of the C-147 (only) has been sent to the surf	ace owner(s)	
10.		
Operator Application Certification:		
I hereby certify that the information and attachments submitted with this	application are true, accurate	and complete to the best of my knowledge and belief.
Name (Print):Kevin Herrmann	Title: Engir	neer
Signature:	Date:5/30	/22
e-mail addresskherrmann@tascosaep.com	Telephone:	432-696-6970
OCD Representative Signature:		Approval Date:
Title: OCD Permit Number:		ber:

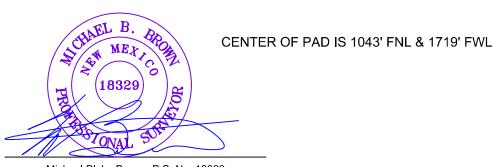
□ OCD Conditions
 □ Additional OCD Conditions on Attachment

SURVEY FOR CONTAINMENT AND RECYCLING FACILITY









Michael Blake Brown, P.S. No. 18329

ALL BEARINGS, DISTANCES, AND COORDINATE VALUES CONTAINED HEREON ARE GRID BASED UPON THE NEW MEXICO COORDINATE SYSTEM OF 1983, EAST ZONE, U.S. SURVEY FEET. ELEVATIONS USED ARE NAVD88, OBTAINED THROUGH AN OPUS SOLUTION.

ARE NAVDBB, OBTAINED THROUGH AN OPUS SOLUTION.

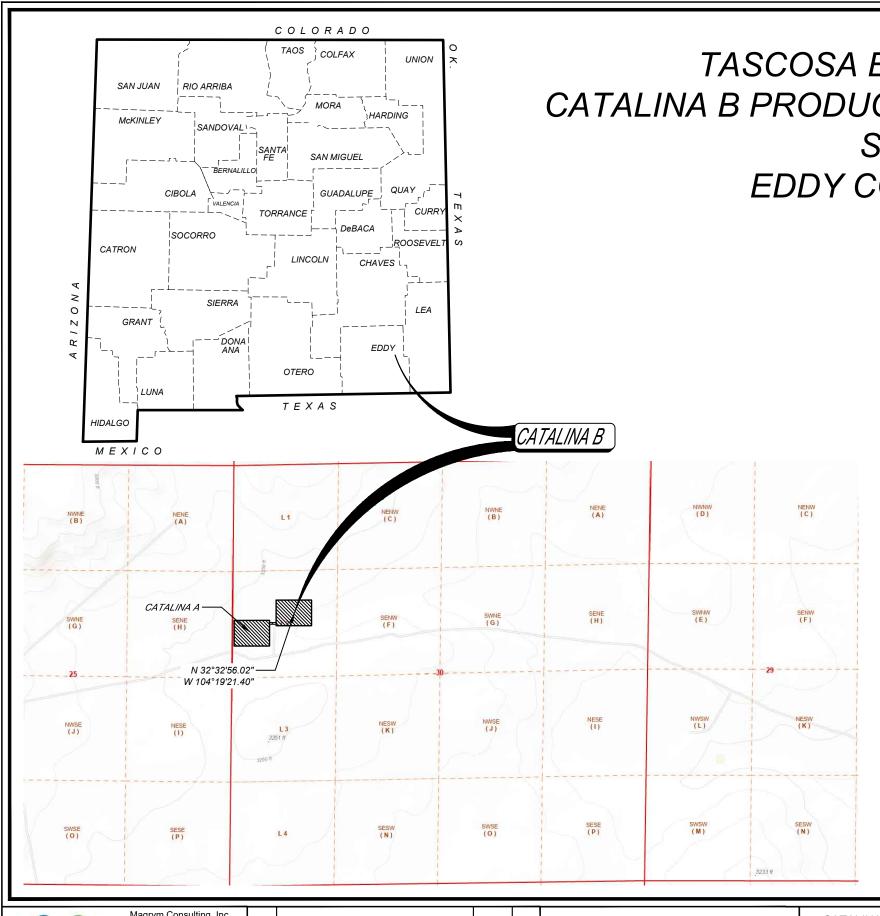
THIS PROPOSED PAD SITE LOCATION SHOWN HEREON HAS BEEN SURVEYED ON THE GROUND UNDER MY SUPERVISION AND PREPARED ACCORDING TO THE EVIDENCE FOUND AT THE TIME OF SURVEY, AND DATA PROVIDED BY TASCOSA ENERGY PARTNERS, LLC. ONLY THE DATA SHOWN ABOVE IS BEING CERTIFIED TO, ALL OTHER INFORMATION WAS INTENTIONALLY OMITTED. THIS PLAT IS ONLY INTENDED TO BE USED FOR A PERMIT AND IS NOT A BOUNDARY SURVEY. THIS CERTIFICATION IS MADE AND LIMITED TO THOSE PERSONS OR ENTITIES SHOWN ON THE FACE OF THIS PLAT AND IS NON-TRANSFERABLE. THIS SURVEY IS CERTIFIED FOR THIS TRANSACTION ONLY.

RECYCLING CONTAINMENT DESIGN DRAWINGS

40-MIL HDPE SPECIFICATIONS

EQUIVALENCY DEMONSTRATION OF 40-MIL HDPE

AVIAN SPECIES HAZING EQUIPMENT



TASCOSA ENERGY PARTNERS, LLC CATALINA B PRODUCED WATER RECYCLING FACILITY S30, T20S, R27E EDDY COUNTY, NEW MEXICO



C-100 - COVER SHEET

C-101 - EXISTING CONDITIONS

C-102 - OVERALL SITE PLAN C-103 - PROPOSED SITE PLAN

C-104 - PROPOSED LINER AND FENCE PLAN

C-105 - SUMMARY OF QUANTITIES

C-106 - GRADING PLAN

C-107 - CROSS SECTIONS PLAN

C-108 - LEAK DETECTION SYSTEM DETAILS C-109 - MISCELLANEOUS DETAILS

C-110 - LEVEE AND PAD DETAILS

C-111 - FENCE DETAILS

C-112 - GAGE / LADDER DETAILS



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ISSUED FOR CONSTRUCTION R2 ISSUED FOR CLIENT REVIEW DESCRIPTION TX #F-19848 | ND #28610PE | OK #8561PE REVISIONS (OR CHANGE NOTICES)

Tascosa Energy Partners, LLC 901 W. Missouri Avenue Midland, TX 79701

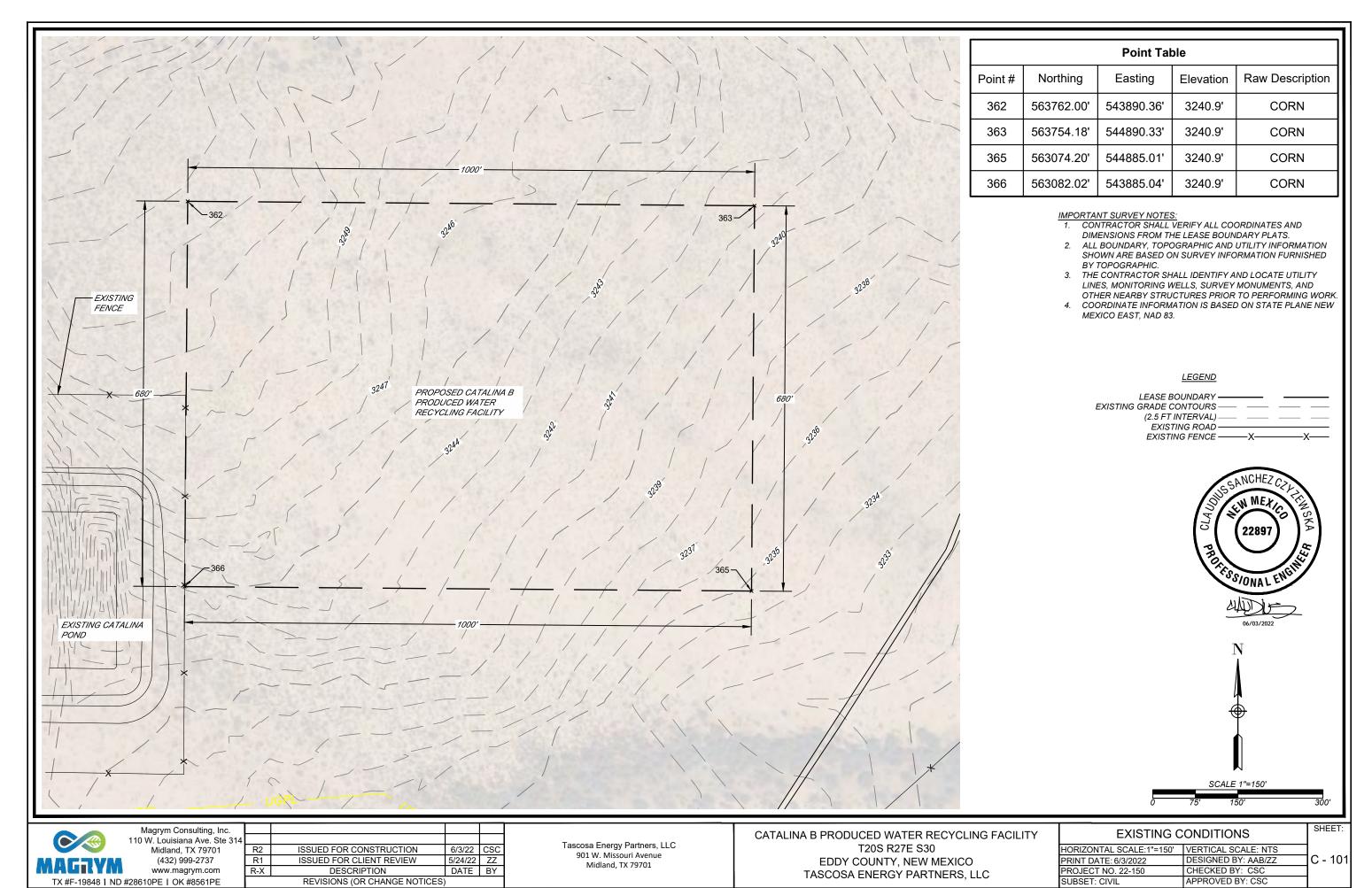
6/3/22 CSC

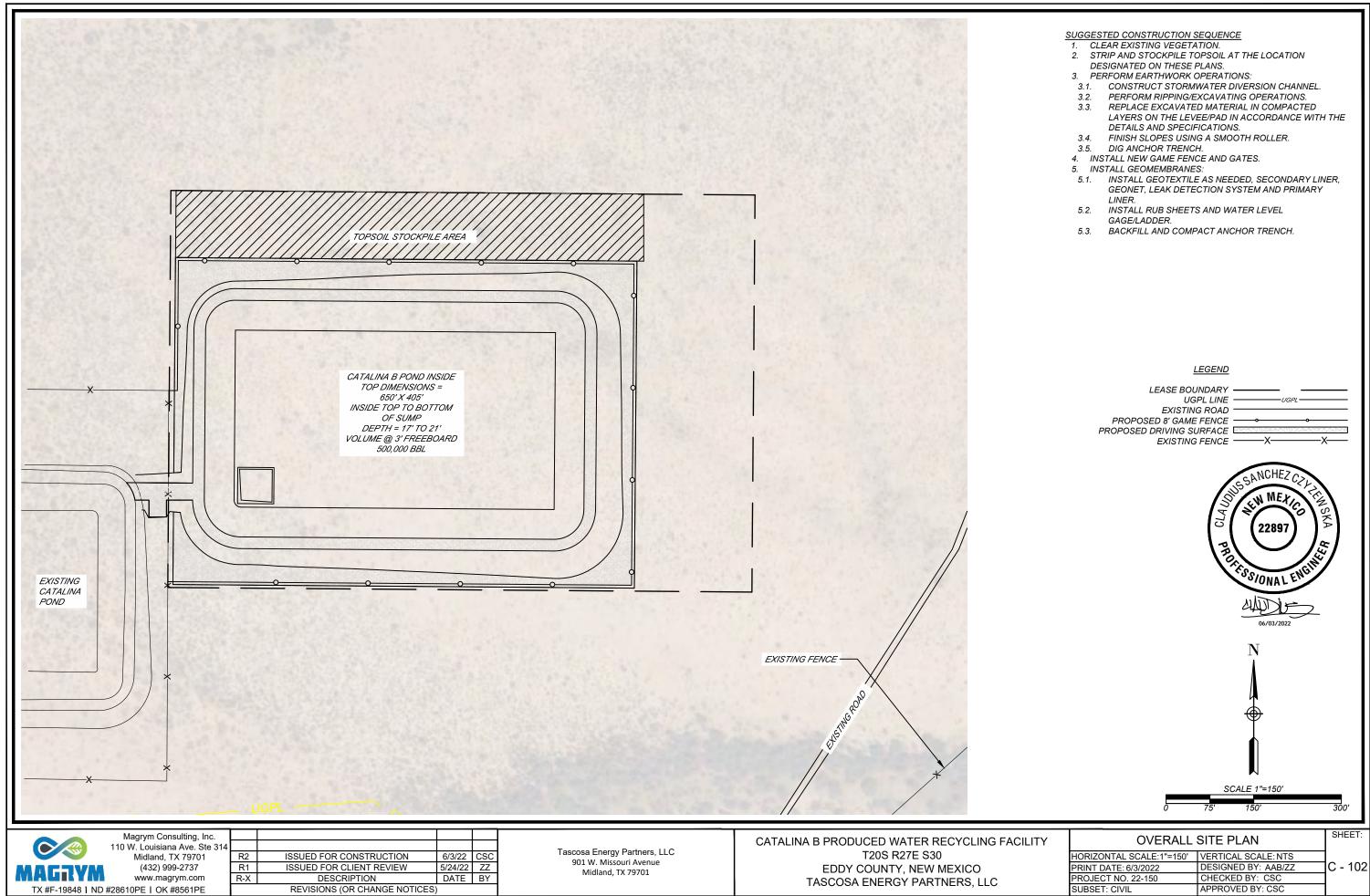
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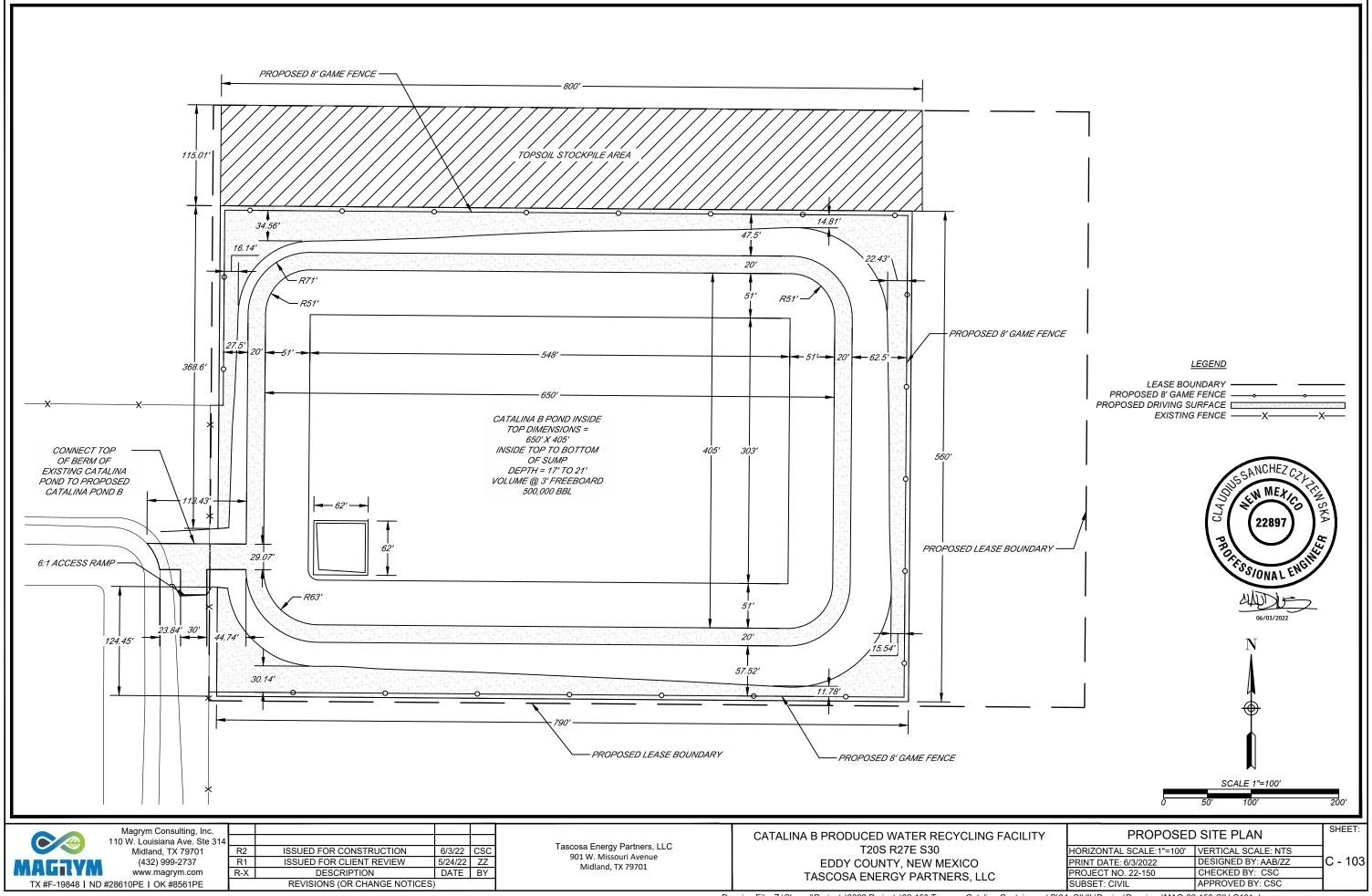
DATE BY

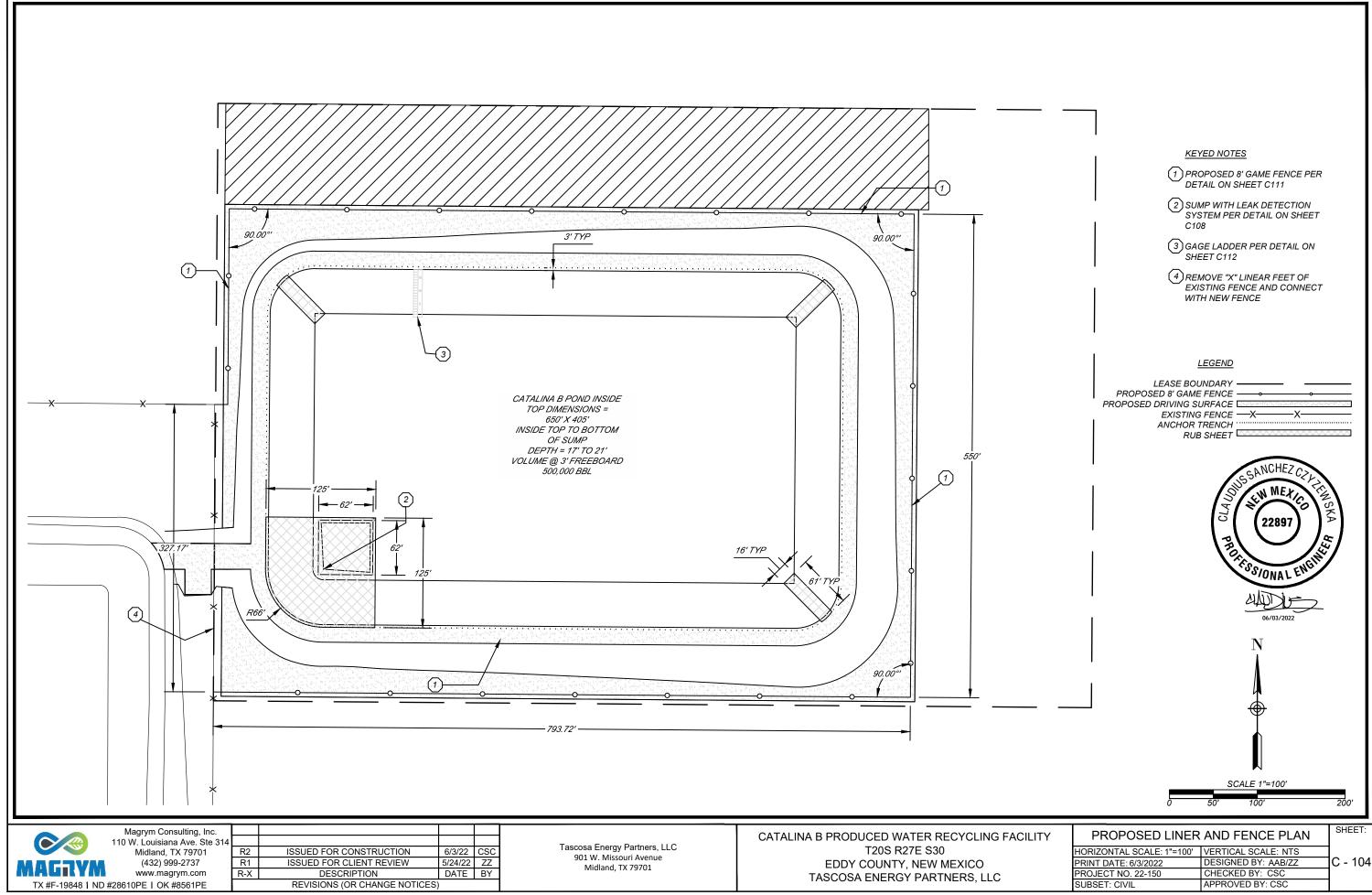
CATALINA B PRODUCED WATER RECYCLING FACILITY T20S R27E S30 EDDY COUNTY, NEW MEXICO TASCOSA ENERGY PARTNERS, LLC

COVER	RSHEET	SHEE
ORIZONTAL SCALE: NTS	VERTICAL SCALE: NTS	1
RINT DATE: 6/3/2022	DESIGNED BY: AAB/ZZ]C - 10
ROJECT NO. 22-150	CHECKED BY: CSC	
IBSET: CIVII	APPROVED BY: CSC	1









GENERAL NOTES

- NEW MEXICO ADMINISTRATIVE CODE TITLE 19, CHAPTER 15, PART 34, DESIGN CRITERIA FOR RECYCLING CONTAINMENTS SHALL APPLY TO THIS
- ALL BOUNDARY, TOPOGRAPHIC AND UTILITY INFORMATION SHOWN ARE BASED ON SURVEY INFORMATION FURNISHED BY TOPOGRAPHIC.
- THE CONTRACTOR SHALL IDENTIFY AND LOCATE UTILITY LINES. MONITORING WELLS. SURVEY MONUMENTS, AND OTHER NEARBY STRUCTURES PRIOR TO PERFORMING WORK.
- COORDINATE INFORMATION IS BASED ON STATE PLANE COORDINATES, NEW MEXICO EAST, NAD 83.
- THE CONTRACTOR SHALL IDENTIFY ANY DISCREPANCIES PRIOR TO PROCEEDING WITH CONSTRUCTION AND CONTACT THE ENGINEER IN WRITING.
- THE CONTRACTOR SHALL IMPLEMENT AND MAINTAIN BEST MANAGEMENT PRACTICES (BMPS) TO MINIMIZE EROSION AND CONTROL SEDIMENT TO PROTECT SURFACE WATER QUALITY DURING STORM EVENTS.

EARTHWORK NOTES

- THE CONTRACTOR SHALL USE WATER FOR COMPACTION AT ALL TIMES. THE CONTRACTOR SHALL ENSURE THEIR BID INCLUDES CONSTRUCTION WATER. NO EARTHWORK OPERATIONS SHALL TAKE PLACE IF CONSTRUCTION WATER IS NOT AVAILABLE ONSITE.
- THE CONTRACTOR SHALL BUILD THE LEVEES USING COMPACTED LAYERS. UNCONTROLLED AND INCONSISTENT PUSHING AND PILING OF MATERIAL FOR LEVEE CONSTRUCTION IS NOT ACCEPTABLE. THE CONTRACTOR SHALL DEVELOP A SUCCESSFUL COMPACTION PATTERN EARLY IN THE PROCESS, VERIFIED THROUGH NUCLEAR DENSITY OR SAND CONE TESTING, AND SHALL MAINTAIN CONSISTENCY IN THE COMPACTIVE EFFORT AS LONG AS THE MATERIALS ENCOUNTERED REMAINS CONSISTENT. IF ONSITE SOILS ENCOUNTERED CHANGE, THE CONTRACTOR SHALL DEVELOP A NEW COMPACTION PATTERN
- FILL FOR LEVEES SHALL BE PLACED AND COMPACTED IN HORIZONTAL LIFTS WITH MAXIMUM LOOSE LIFT THICKNESS OF 10 INCHES, OR AS DIRECTED BY ENGINEER. CONSTRUCT EACH LAYER CONTINUOUSLY AND APPROXIMATELY HORIZONTAL FOR THE WIDTH AND LENGTH OF THE LEVEE. FILL SHALL BE COMPACTED TO AT LEAST 95 PERCENT OF MAXIMUM DRY DENSITY DETERMINED BY THE ASTM D698 AND AT MOISTURE CONTENT WITHIN +2% TO -2% OF OPTIMUM MOISTURE CONTENT AS DETERMINED BY A STANDARD PROCTOR SOILS TEST ON SAMPLES FROM THE SOURCE AREA
- FILL SHALL NOT BE PLACED AND COMPACTED WHEN THE MATERIALS ARE TOO WET TO PROPERLY COMPACT. MATERIAL WHICH IS TOO WET SHALL BE SPREAD ON THE FILL AREA AND PERMITTED TO DRY, ASSISTED BY HARROWING IF NECESSARY, UNTIL THE MOISTURE CONTENT IS REDUCED TO ALLOWABLE LIMITS. IF THE ENGINEER DETERMINED THAT ADDED MOISTURE IS REQUIRED, WATER SHALL BE APPLIED UNIFORMLY OVER THE AREA TO BE TREATED, AND GIVE COMPLETE AND ACCURATE CONTROL OF THE AMOUNT OF WATER TO BE USED. IF TOO MUCH WATER IS ADDED, THAT AREA SHALL BE PERMITTED TO DRY BEFORE COMPACTION IS CONTINUED.
- PERFORM ONE NUCLEAR DENSITY GAGE TEST PER 2500 CY MINIMUM OR AS DIRECTED BY THE ENGINEER.
- EARTHWORK CONTRACTOR SHALL PERFORM A VISUAL INSPECTION OF THE FINISHED COMPACTED POND BOTTOM AND SIDE SLOPES BEFORE HDPE LINER INSTALLATION, REMOVING ALL DEBRIS, SHARP OBJECTS AND GRAVEL LARGER THAN 3/4 INCH.
- EARTHWORK CONTRACTOR SHALL ROLL SURFACE WITH A SMOOTH ROLLER TO ELIMINATE RUTS.

- LINER CONTRACTOR SHALL INSPECT GRADED SURFACE FOR DEBRIS, ROCKS OR OTHER MATERIAL THAT MAY DAMAGE THE LINER AND COORDINATE WITH OWNER IF ADDITIONAL SUBGRADE RESURFACING IS NEEDED PRIOR TO PERFORMING WORK.
- LINER CONTRACTOR TO PROVIDE SUBMITTAL OF LINER PANEL LAYOUT.
- LINER CONTRACTOR TO SIGN SUBGRADE ACCEPTANCE FORM (PROVIDED BY OWNER REPRESENTATIVE) DAILY PRIOR TO INSTALLATION.
- LINER TO BE INSTALLED PER GRI SPECIFICATIONS, GUIDES AND PRACTICES.
- CONTRACTOR SHALL PLACE SANDBAGS ON LINER DURING INSTALLATION AS REQUIRED TO PREVENT WIND UPLIFT UNTIL POND IS FILLED TO A
- CONTRACTOR SHALL USE BLACK 60 MIL HDPE SMOOTH GEOMEMBRANE AS THE PRIMARY LINER AND BLACK 40 MIL HDPE SMOOTH GEOMEMBRANE AS THE SECONDARY LINER.
- A 3' DIAMETER MINIMUM PIECE OF 40MIL LINER SHALL BE EXTRUDED WELDED WHERE THE PIE SHAPED CORNER SECTIONS MEET FOR SEAM
- INSTALL A FULL DOUBLE WIDTH SECTION OF BLACK OR WHITE 60 MIL TEXTURED HDPE GEOMEMBRANE RUB SHEET. EXTRUDE WELD TO LINER. WELDS SHALL BE 2" LONG AND SPACED EVERY 12" ALONG BOTH SIDES OF THE SHEET. DO NOT WELD END EDGES. SECTION SHALL EXTEND FROM SUMP AND INSTALLED INTO LINER ANCHOR TRENCH AS SHOWN.
- LINER SHALL BE PROTECTED WITH A 8 OZ. NONWOVEN GEOTEXTILE IF ROCK OR OTHER ANGULAR MATERIALS WITH A DIMENSION GREATER THAN 3/4 INCH ARE PRESENT.
- 10. SUMPS SHALL BE BACKFILLED WITH NON-ANGULAR MAXIMUM 3/8 INCH SIZED PEA GRAVEL.
- ALL SEAMS MUST BE WELDED WITH A 6" MINIMUM OVERLAP.
- 12. CONTRACTOR SHALL NON-DESTRUCTIVELY TEST ALL SEAMS THEIR FULL LENGTH USING AN AIR PRESSURE OR VACUUM TEST, THE PURPOSE OF THIS TEST IS TO CHECK THE CONTINUITY OF THE SEAM.
- 13. FOR AIR PRESSURE TESTING (ASTM 5820), THE FOLLOWING PROCEDURES ARE APPLICABLE TO THE SEAMS WELD WITH DOUBLE SEAM FUSION WFI DFR
 - THE EQUIPMENT USED SHALL CONSIST OF AN AIR TANK OR PUMP CAPABLE OF PRODUCING A MINIMUM 35 PSI AND A SHARP NEEDLE WITH A PRESSURE GAUGE ATTACHED TO INSERT INTO THE AIR CHAMBER.
 - SEAL BOTH ENDS OF THE SEAM BY HEATING AND SQUEEZING THEM TOGETHER. INSERT THE NEEDLE WITH THE GAUGE INTO THE AIR CHANNEL. PRESSURIZE THE AIR CHANNEL TO A MINIMUM OF 35 PSI. NOTE TIME STARTS AND WAIT A MINIMUM OF 5 MINUTES TO CHECK. IF PRESSURE AFTER 5 MINUTES HAD DROPPED LESS THAN 2 PSI THE TEST IS SUCCESSFUL (THICKNESS OF MATERIAL MAY CAUSE VARIANCE).
- c. CUT OPPOSITE SEAM END AND LISTEN FOR PRESSURE RELEASE TO VERIFY FULL SEAM HAS BEEN TESTED.
- IF THE TEST FAILS, FOLLOW THESE PROCEDURES.
 - I. WHILE CHANNEL IS UNDER PRESSURE WALK THE LENGTH OF THE SEAM LISTENING FOR A LEAK.
- II. WHILE CHANNEL IS UNDER PRESSURE APPLY A SOAPY SOLUTION TO THE SEAM EDGE AND LOOK FOR BUBBLES FORMED BY AIR ESCAPING. iii. RE-TEST THE SEAM IN SMALLER INCREMENTS UNTIL THE LEAK IS FOUND.
- ONCE LEAK IS FOUND USING ONE OF THE PROCEDURES ABOVE, CUT OUT THE AREA AND RETEST THE PORTIONS OF THE PORTIONS OF THE SEAMS BETWEEN THE LEAK AREAS PER 6A AND 6B ABOVE. CONTINUE THIS PROCEDURE UNTIL ALL SECTIONS OF THE SEAM PASS THE PRESSURE TEST.
- REPAIR THE LEAK WITH A PATCH AND VACUUM TEST.
- 14. ALL NON-DESTRUCTIVE TESTS WILL BE NOTED IN THE NON-DESTRUCTIVE LOGS.
- 15. LINER GAS VENTS SHALL BE SPACED ALONG THE INSIDE SLOPE AT APPROXIMATELY 100 FEET ON CENTER OR MINIMUM 2 VENTS PER SIDE.
- 16. WHEN ANY PIPING EQUIPMENT, INLET, OR OUTLET IS IN DIRECT CONTACT WITH THE LINER, AN APRON CONSISTING OF 60 MIL HDPE MATERIAL SHALL BE INSTALLED BENEATH THE EQUIPMENT OR STRUCTURE TO PROTECT THE PRIMARY LINER.
- 17. LAY BOTH LINERS IN ANCHOR TRENCH. BACKFILL ANCHOR TRENCH IN 2 LIFTS AND COMPACT.

STAGE STORAGE		
POND ELEVATION (FT)	REVELATION POND VOLUME (BBL)	
3233.90	0	
3234.90	186	
3235.90	807	
3236.90	5,236	
3237.90	24,106	
3238.90	54,127	
3239.90	85,065	
3240.90	116,929	
3241.90	149,728	
3242.90	183,474	
3243.90	218,175	
3244.90	253,841	
3245.90	290,483	
3246.90	328,109	
3247.90	366,730	
3248.90	406,355	
3249.90	446,995	
3250.90	488,659	
3251.90	531,357	
3252.90		
3253.90		
3254.90		



SUMMARY OF QUANTITIES				
ITEM NUMBER	ITEM	UNIT	QTY	
1	CLEARING AND GRUBBING	ACRES	13	
2	STRIP AND STOCKPILE TOPSOIL (6" AVERAGE)	CUBIC YARD	8,391	
3	ESTIMATED CUT (BELOW EXISTING GRADE)*	CUBIC YARD	58,022	
4	ESTIMATED FILL (ABOVE EXISTING GRADE)**	CUBIC YARD	51,214	
5	8' GAME FENCE	LINEAR FEET	3,238	
6	20' DOUBLE GATE	LINEAR FEET	1	
7	RUB SHEET 60 MIL HDPE GEOMEMBRANE (TEXTURED)***	SQUARE FEET	18,626	
8	PRIMARY 60 MIL HDPE GEOMEMBRANE (SMOOTH)***	SQUARE FEET	275,670	
9	200 MIL GEONET***	SQUARE FEET	275,670	
10	SECONDARY 40 MIL HDPE GEOMEMBRANE (SMOOTH)***	SQUARE FEET	275,670	
11	8 OZ. GEOTEXTILE***	SQUARE FEET	275,670	
12	6" HDPE DR11 PIPE WITH PERFORATIONS IN SUMP	LINEAR FEET	90	
13	GAGE LADDER	EACH	1	
14	DRAIN ROCK	CUBIC YARD	1	
15	ANCHOR TRENCH	LINEAR FEET	2,057	
17	CONSTRUCTION WATER	ALLOWANCE	•	
18	MATERIALS TESTING	ALLOWANCE	ALLOWANCE	
19	EROSION CONTROL BMP'S	ALLOWANCE	ALLOWANCE	

– MAX FLUID LEVEL

IMPORTANT QUANTITY NOTES:

- CUT QUANTITY (ITEM NUMBER 3) INCLUDES TOPSOIL QUANTITY (ITEM NUMBER 2). GEOTECHNICAL INFORMATION WAS <u>NOT AVAILABLE</u> AT THE TIME THESE PLANS WERE PREPARED. 20% FILL FACTOR WAS ASSUMED AND APPLIED TO THE FILL QUANTITY. THE CONTRACTOR SHALL FIELD VERIFY SHRINKAGE AND SWELLING OF EXISTING SOILS. CUT AND FILL QUANTITIES SHOWN ON THIS TABLE PERTAIN TO THE ENTIRE PROJECT AREA. LEVEE, PAD AND ADJACENT DRIVING SURFACE ARE INCLUDED IN THE FILL QUANTITY.
- THESE ARE COMPLETE-IN-PLACE QUANTITIES. OVERLAP, ANCHOR, WRINKLE, SCRAP AND/OR SPOIL QUANTITIES ARE NOT INCLUDED IN THIS BID ITEM. THE CONTRACTOR SHALL ACCOUNT FOR THESE ADDITIONAL QUANTITIES IN THEIR BID.

TX #F-19848 | ND #28610PE | OK #8561PE

Magrym Consulting, Inc. 110 W. Louisiana Ave. Ste 31 Midland, TX 79701 (432) 999-2737 www.magrvm.com

ISSUED FOR CONSTRUCTION 6/3/22 CSC ISSUED FOR CLIENT REVIEW 5/24/22 ZZ DATE BY R-X DESCRIPTION REVISIONS (OR CHANGE NOTICES)

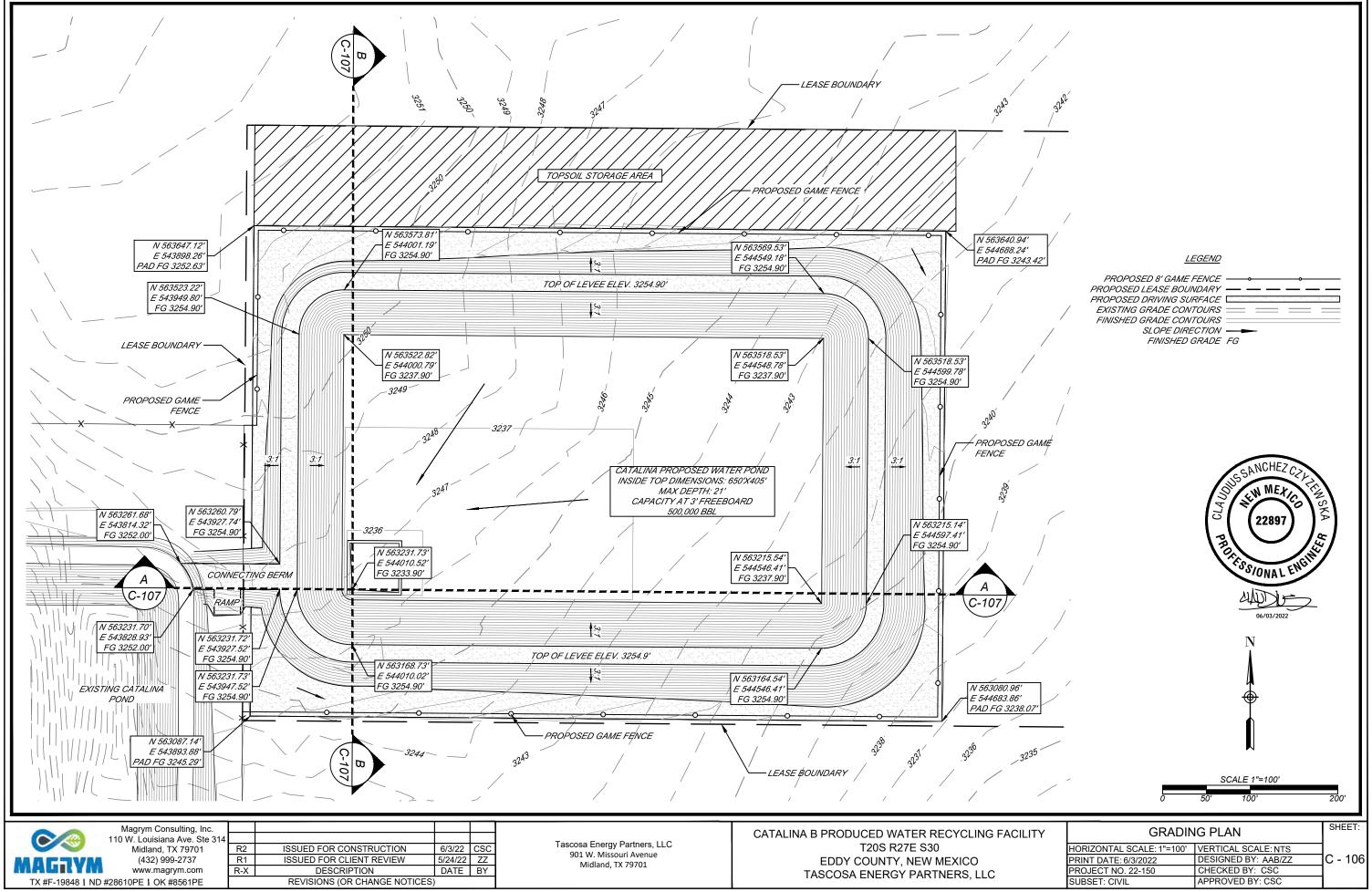
Tascosa Energy Partners, LLC 901 W. Missouri Avenue Midland, TX 79701

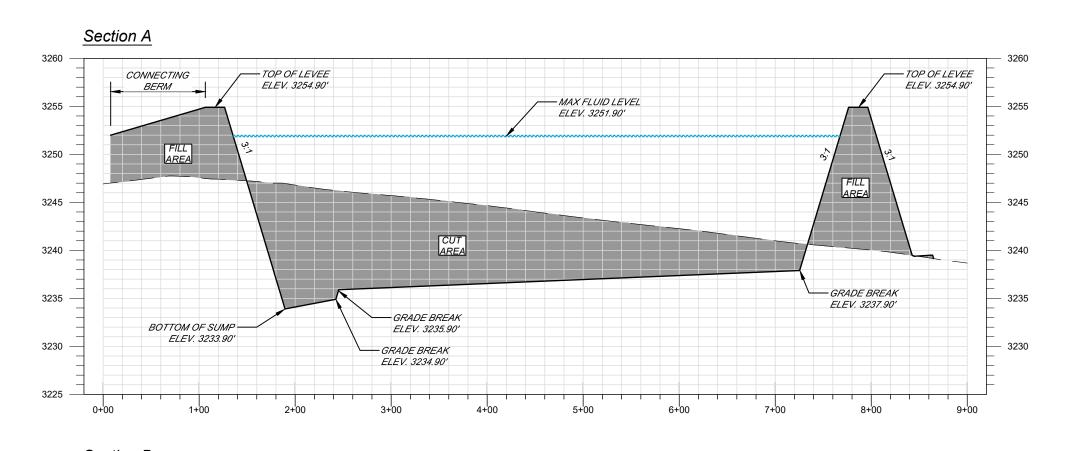
CATALINA B PRODUCED WATER RECYCLING FACILITY T20S R27E S30 EDDY COUNTY, NEW MEXICO TASCOSA ENERGY PARTNERS, LLC

SUMMARY OF QUANTITIES AND GENERAL NOTES VERTICAL SCALE: NTS HORIZONTAL SCALE: NTS DESIGNED BY: AAB/ZZ PRINT DATE: 6/3/2022 PROJECT NO. 22-150 CHECKED BY: CSC APPROVED BY: CSC SUBSET: CIVIL

C - 105

Drawing File: Z:\Shared\Projects\2022 Projects\222-150 Tascosa Catalina Containment B\04 CIVIL\Design\Drawings\MAG-22-150-CIV-Grading R1.dwg





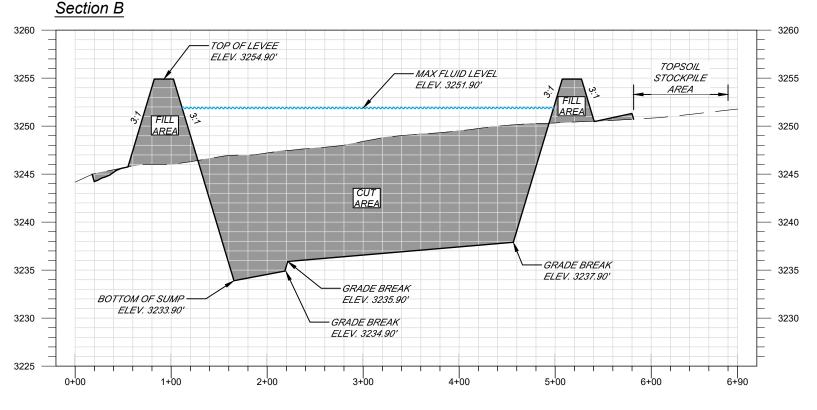


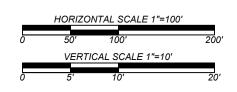
<u>LEGEND</u>

EXISTING GRADE FINISHED GRADE

<u>NOTES</u>

FOR LEVEE DETAILS SEE PLAN SHEET C - 109





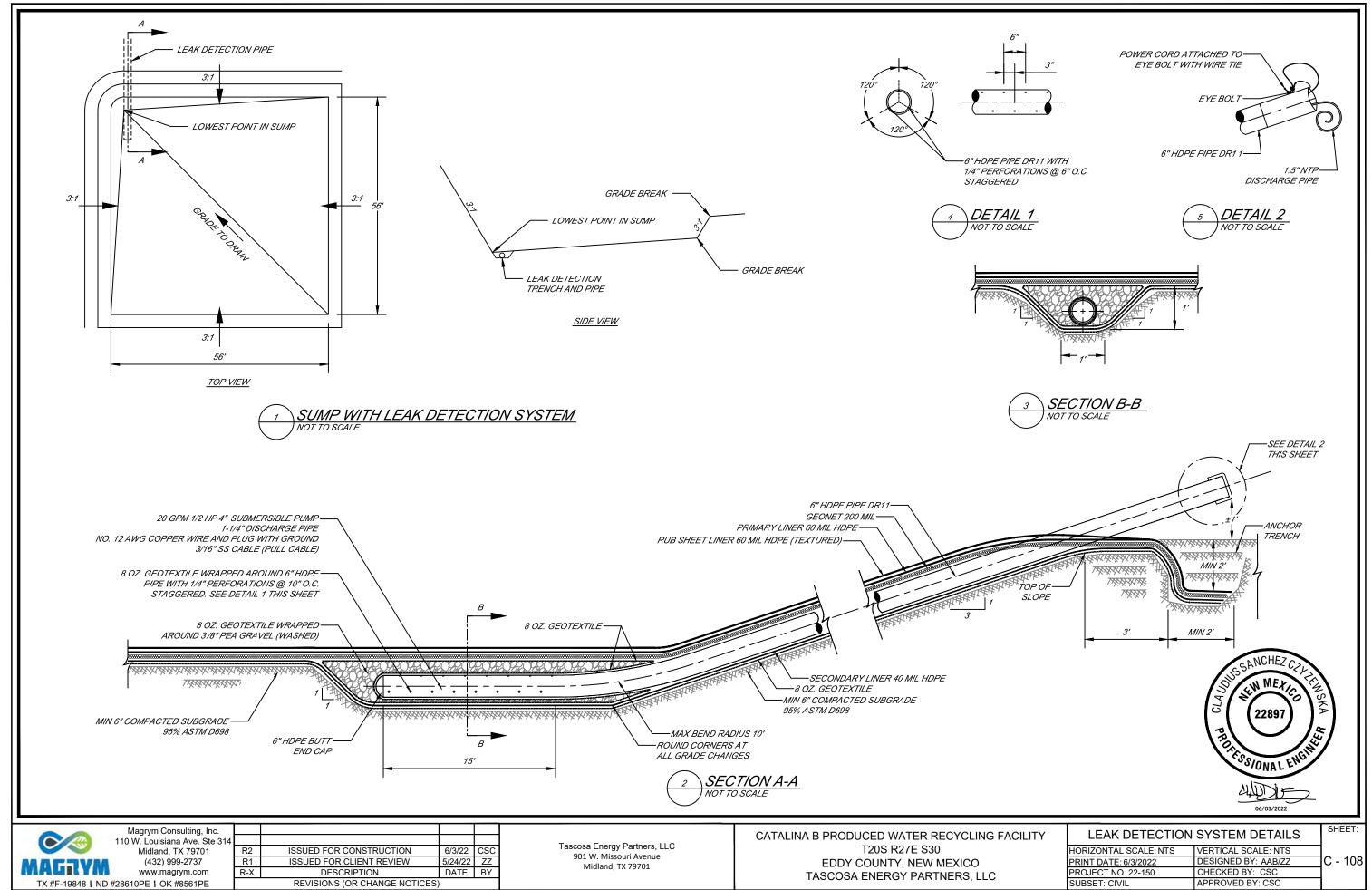
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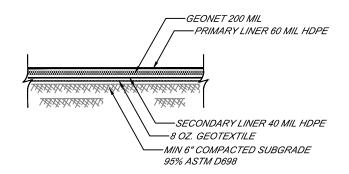
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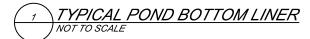
Tascosa Energy Partners, LLC 901 W. Missouri Avenue Midland, TX 79701

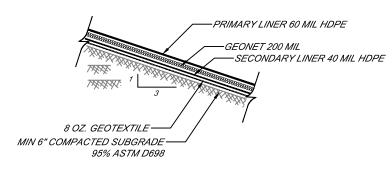
CATALINA B PRODUCED WATER RECYCLING FACILITY T20S R27E S30 EDDY COUNTY, NEW MEXICO TASCOSA ENERGY PARTNERS, LLC

CROSS S	ECTIONS	SHEET:
ORIZONTAL SCALE: 1"=100'	VERTICAL SCALE: 1"=10'	1
RINT DATE: 6/3/2022	DESIGNED BY: AAB/ZZ	C - 107
ROJECT NO. 22-150	CHECKED BY: CSC	
JBSFT: CIVII	APPROVED BY: CSC	l

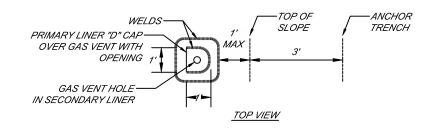


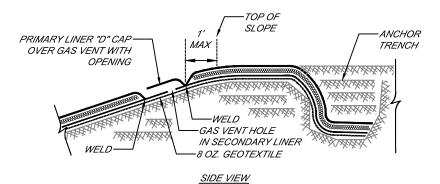












NOTE:
GAS VENT SPACING SHALL BE INSTALLED PER MANUFACTURER'S RECOMMENDATIONS





	Magrym Consulting, Inc
	110 W. Louisiana Ave. Ste
	Midland, TX 79701
MAGRYM	(432) 999-2737
AND NO COLUMN TO A TANK	www.magrym.com
TX #F-19848 ND :	#28610PE OK #8561PE

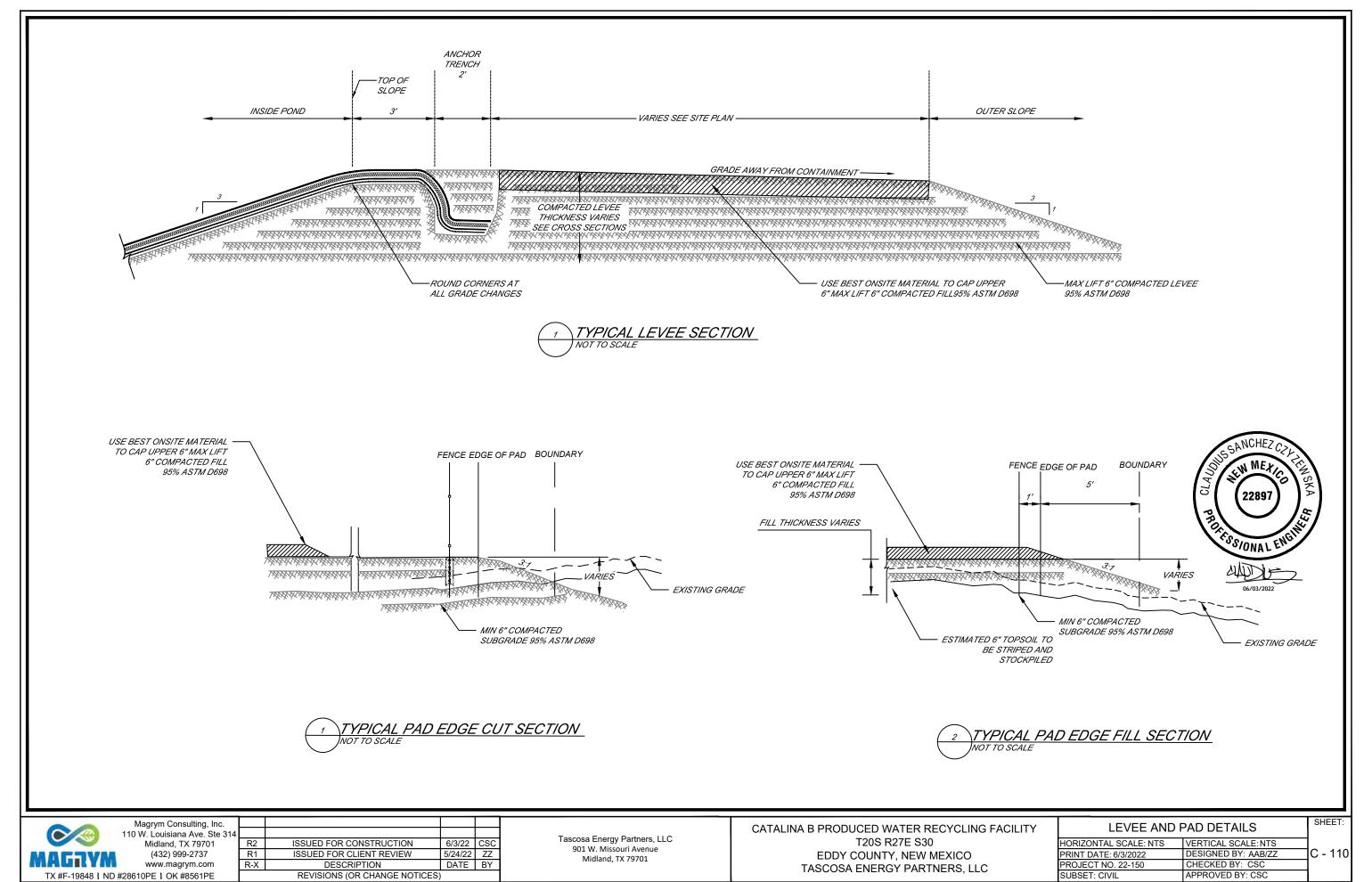
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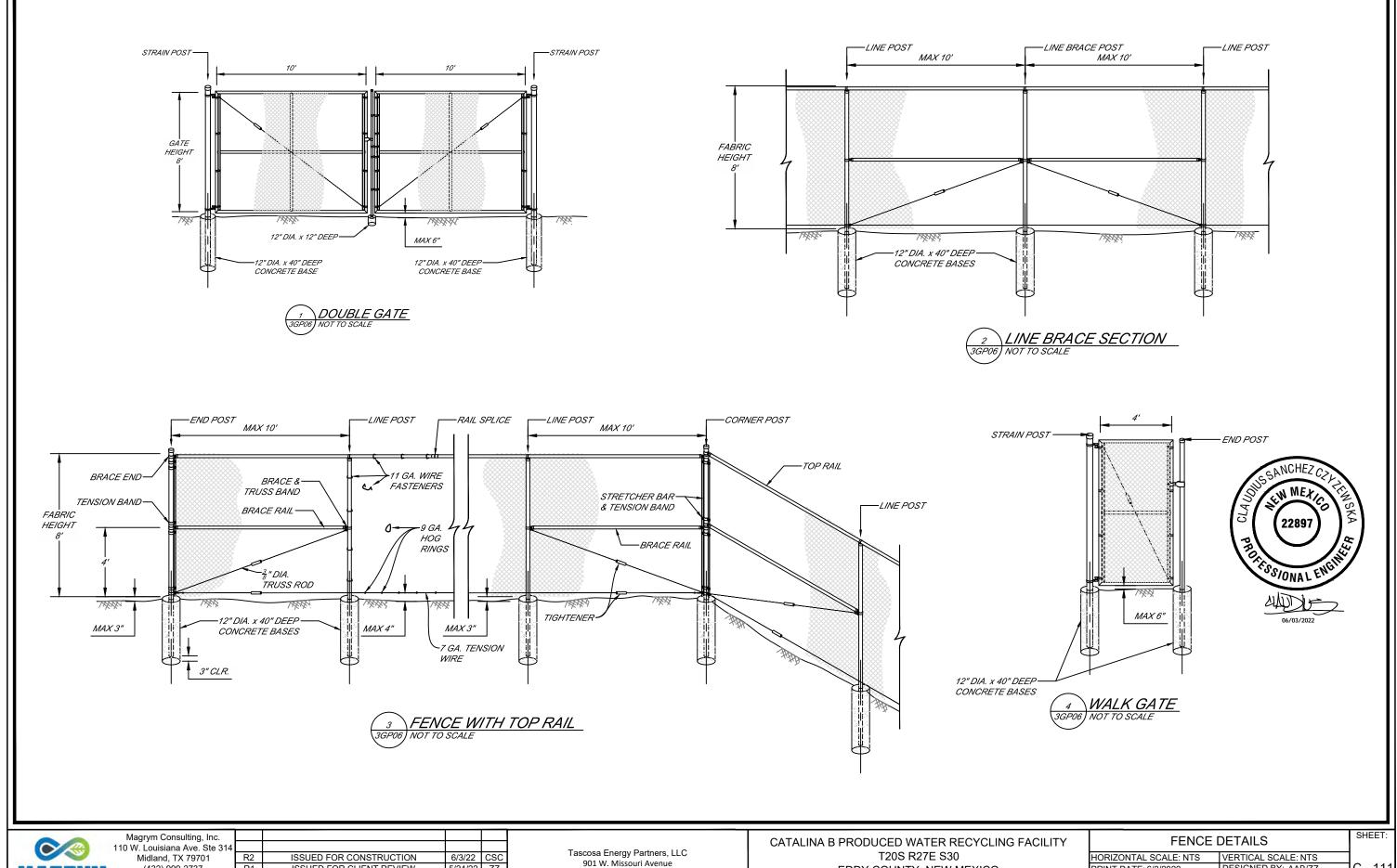
14				
	R2	ISSUED FOR CONSTRUCTION	6/3/22	CSC
	R1	ISSUED FOR CLIENT REVIEW	5/24/22	ZZ
	R-X	DESCRIPTION	DATE	BY
	REVISIONS (OR CHANGE NOTICES)			

Tascosa Energy Partners, LLC 901 W. Missouri Avenue Midland, TX 79701

CATALINA B PRODUCED WATER RECYCLING FACILITY T20S R27E S30 EDDY COUNTY, NEW MEXICO TASCOSA ENERGY PARTNERS, LLC

MISCELLANE	OUS DETAILS	SHEET:
HORIZONTAL SCALE: NTS	VERTICAL SCALE: NTS	1
PRINT DATE: 6/3/2022	DESIGNED BY: AAB/ZZ	C - 109
PROJECT NO. 22-150	CHECKED BY: CSC	
SUBSET: CIVIL	APPROVED BY: CSC	



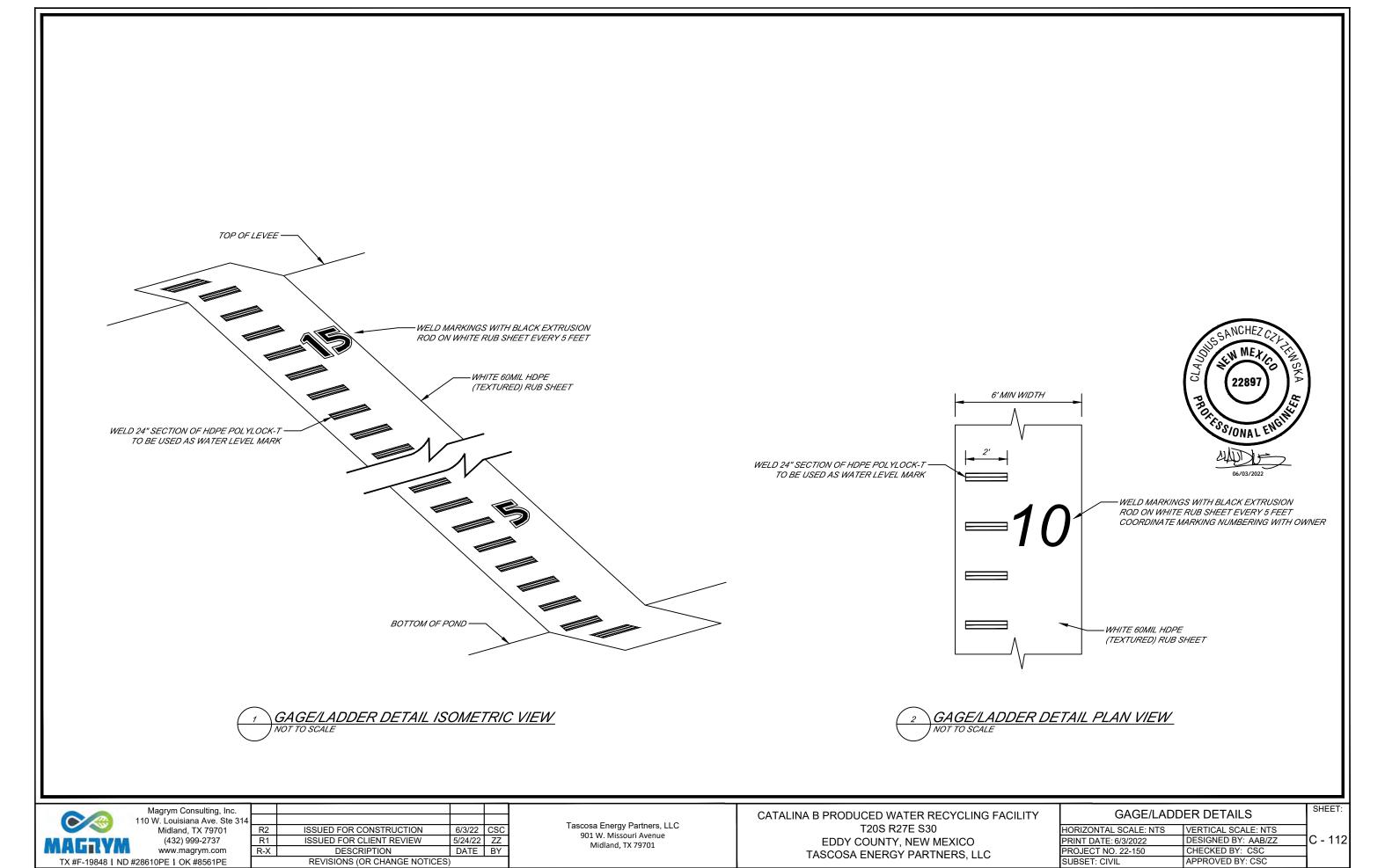


ISSUED FOR CONSTRUCTION R2 6/3/22 CSC 5/24/22 ZZ DATE BY ISSUED FOR CLIENT REVIEW DESCRIPTION REVISIONS (OR CHANGE NOTICES)

Midland, TX 79701

T20S R27E S30 EDDY COUNTY, NEW MEXICO TASCOSA ENERGY PARTNERS, LLC

FENCE I	DETAILS	SHEET:
HORIZONTAL SCALE: NTS	VERTICAL SCALE: NTS	
PRINT DATE: 6/3/2022	DESIGNED BY: AAB/ZZ	C - 111
PROJECT NO. 22-150	CHECKED BY: CSC	
SUBSET: CIVIL	APPROVED BY: CSC	





TECHNICAL DATA SHEET

PREMIUM HD Series, 40 mils

Black, Smooth

2801 Boul. Marie-Victorin Varennes, Quebec Canada J3X 1P7

Tel: (450) 929-1234 Sales: (450) 929-2544 Toll free in North America:1-800-571-3904 www.Solmax.com www.solmax.com

PROPERTY	TEST METHO	FREQUENCY(1)	UNIT Imperial	
SPECIFICATIONS				
Thickness (min. avg.)	ASTM D5199	Every roll	mils	40.0
Thickness (min.)	ASTM D5199	Every roll	mils	36.0
Melt Index - 190/2.16 (max.)	ASTM D1238	1/Batch	g/10 min	1.0
Sheet Density (8)	ASTM D792	Every 10 rolls	g/cc	≥ 0.94
Carbon Black Content	ASTM D4218	Every 2 rolls	%	2.0 - 3.0
Carbon Black Dispersion	ASTM D5596	Every 10 rolls	Category	Cat. 1 & Cat. 2
OIT - standard (avg.)	ASTM D3895	Per formulation	min	160
HPOIT - High Pressure (avg)	ASTM D5885	Per formulation	min	800
Tensile Properties (min. avg) (2)	ASTM D6693	Every 2 rolls		
Strength at Yield			ppi	84
Elongation at Yield			%	13
Strength at Break			ppi	152
Elongation at Break			%	750
Tear Resistance (min. avg.)	ASTM D1004	Every 5 rolls	lbf	28
Puncture Resistance (min. avg.)	ASTM D4833	Every 5 rolls	lbf	85
Dimensional Stability	ASTM D1204	Certified	%	± 2
Stress Crack Resistance (SP-NCTL) (avg.)	ASTM D5397	1/Batch	hr	1000
Multi-Axial Tensile (min. avg.)	ASTM D5617	Per formulation	%	15
Oven Aging - % retained after 90 days	ASTM D5721	Per formulation		
HP OIT (min. avg.)	ASTM D5885		%	80
UV Res % retained after 1600 hr	ASTM D7238	Per formulation		l
HP-OIT (min. avg.)	ASTM D5885		%	80

SUPPLY SPECIFICATIONS (Roll dimensions may vary ±1%)

NOTES

- 1. Testing frequency based on standard roll dimension and one batch is approximately 180,000 lbs (or one railcar).
- 2. Machine Direction (MD) and Cross Machine Direction (XMD or TD) average values should be on the basis of 5 specimens each direction.
- 8. Correlation table is available for ASTM D792 vs ASTM D1505. Both methods give the same results.
- * All values are nominal test results, except when specified as minimum or maximum.
- * The information contained herein is provided for reference purposes only and is not intended as a warranty of guarantee. Final determination of suitability for use contemplated is the sole responsability of the user. SOLMAX assumes no liability in connection with the use of this information.

Solmax is not a design professional and has not performed any design services to determine if Solmax's goods comply with any project plans or specifications, or with the application or use of Solmax's goods to any particular system, project, purpose, installation or specification.



Mustang Extreme

December 9, 2019



Attn:

Mr. Steven Roeder

Re:

40 mil HDPE Geomembrane - Hydraulic Conductivity

Dear Mr. Roeder:

Hydraulic Conductivity of HDPE geomembranes can be indirectly obtained through ASTM E96 method (Designing with Geosynthetics, page 437, fifth edition – Robert Koerner).

Based on our test results and the method pointed out in the above reference, it can be concluded that Solmax HDPE geomembranes have a typical Hydraulic Conductivity no higher than 10^{-12} cm/s

Should you need further information, please do not hesitate to contact us.

Sincerely,

Mauricio Ossa

Senior Technical Manager

Houston-Texas

R.K. FROBEL & ASSOCIATES

Consulting Engineers

Technical Memorandum: 40-mil HDPE as Alternative Secondary Liner System for In Ground Recycling Containment Facilities NMAC 19.15.34.12 A

I have investigated the suitability of application for 40 mil HDPE geomembrane as an equivalent secondary liner to 30 mil scrim reinforced LLDPE (LLDPEr) in the application for In Ground Recycling Containment facilities. *In summary, it is my professional opinion that the specified 40 mil HDPE geomembrane will provide a secondary liner system that is equal to or better than 30 mil scrim reinforced LLDPEr and will provide the requisite protection of fresh water, public health and the environment for many years when engineering design provides requisite site/soil/slope preparation and when used in concert with requisite primary liners and drainage layers.*

It is understood that the lining system under discussion is composed of a 60 mil HDPE Primary liner, geonet drainage layer and a 40 mil HDPE Secondary liner. *In consideration of the secondary lining system application, size of impoundment and depth, design details as well as the chemical nature of typical processed water, it is my professional opinion that the 40 mil HDPE geomembrane will provide the requisite barrier against processed water loss and will function effectively as a secondary liner.*

The following are discussion points that hopefully will exhibit the equivalency of a 40 mil HDPE secondary liner to that of a 30 mil LLDPEr.

The nature and formulation of the 40 mil HDPE resin is the same as the Primary 60 mil HDPE. The major difference is that the 40 mil HDPE is lower in thickness (more flexible and less puncture resistant). However, in covered conditions, HDPE will resist aging and degradation and remain intact for many decades. In fact, a secondary liner of 40 mil HDPE will outlast an exposed 60 mil HDPE liner. According to the Geosynthetic Research Institute (GRI) study on lifetime prediction (GRI Paper No. 6), the half life of HDPE (GRI GM 13) exposed is > 36 years and the half-life of HDPE covered or buried is greater than 100 years. It is understood that in order to ensure compliance of materials, the primary 60 mil HDPE to be used must meet or exceed GRI GM 13 Standards. Likewise, the secondary liner that is not exposed to the same environmental and chemical conditions must meet or exceed GRI GM 13 for non-reinforced HDPE. Adhering to the minimum requirements of the GRI Specifications, 40 mil HDPE when used as a secondary liner will be equally as protective as the primary 60 mil HDPE liner (reference: www.geosynthetic-institute.org/grispecs) and equally as protective as a 30 mil scrim reinforced LLDPEr liner.

<u>Durability of Geomembranes is directly affected by exposure conditions.</u> Buried or covered geomembranes are not affected by the same degradation mechanisms (UV, Ozone, Chemical, Stress, Temperature, etc) as are fully exposed geomembranes. In this regard, the secondary liner material and thickness can be much less robust than the fully exposed primary liner which in this case is 60 mil HDPE. This is also the case for

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landfill lining systems where the secondary geomembrane in a bottom landfill cell may be 40 mil HDPE.

Thermal Fusion Seaming Requirements. Thermal seaming and QC seam test requirements for geomembranes are product specific and usually prescribed by the sheet manufacturer. Dual wedge thermal fusion welding is commonly used on HDPE and QC testing by air channel (ASTM D 5820) is fully acceptable and recognized as an industry standard. In this regard, there should be no exception requirement for seaming and QC testing as both the Primary and Secondary geomembranes are HDPE. This is fully covered in comprehensive specifications for both the Primary and Secondary geomembranes (Reference: www.ASTM.org/Standards).

Potential for Leakage through the Primary and Secondary Liners. Leakage through geomembrane liners is directly a function of the height of liquid head above any hole or imperfection. The geonet drainage media provides immediate drainage to a low point or sump and thus no hydrostatic head or driving gradient is available to push leakage water through a hole in the secondary liner. In this regard, secondary geomembrane materials can be (and usually are) much less in thickness and also polymer type. Hydraulic Conductivity through the 40 mil HDPE liner material is extremely low due to the polymer type, structure and crystallinity and exceeds requirements of EPA SW-846 Method 9090A.

<u>Chemical Attack</u>. Chemical attack to polymeric geomembranes is directly a function of type of chemical, temperature and exposure time. Again, the HDPE Primary provides the chemically resistant liner and is QC tested to reduce potential defects or holes. If there is a small hole, the geonet drain takes any leakage water immediately to the sump for extraction. Thus, exposure time is very limited on a secondary liner in addition to low temperature, little volume and virtually no head pressure. In this regard, a chemically resistant geomembrane material such as 40 mil HDPE can be specified for the secondary and is a fully acceptable alternate to 30 mil scrim reinforced LLDPEr.

Mechanical Properties Characteristics. Geomembranes of different polymer and/or structure (i.e., reinforced vs non-reinforced) cannot be readily compared using such characteristics as tensile stress/strain, tear, puncture and polymer requirements. For a 40 mil HDPE liner material to function as a Secondary liner it should meet or exceed the manufacturers minimum requirements for Density, Tensile Properties, Tear, Puncture as well as other properties such as UV resistance. The sheet material must also meet or exceed GRI GM 13 minimum requirements. *In this regard, a 40 mil HDPE will be equivalent to a 30 mil LLDPEr as a secondary liner for the conditions listed below:*

- The subgrade or compacted earth foundation will be smooth, free of debris or loose rocks, dry, unyielding and will support the lining system.
- The side slopes for the containment shall be equal to or less than 3H:1V.
- The physical properties and condition of the subgrade or liner foundation

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(i.e., density slope, maisture) will be inspected and certified by a Professional Engineer that it meets or exceeds specification requirements,

- Immediately prior to installation, the installation contractor shall inspect and sign off on the subgrade conditions that they must or exceed the HDPE manufacturer and installers requirements.
- A protective geotextile will be placed on the finished and accepted subgrade between subgrade and the 40 nat IIDPE Secondary lines.
- A 200 nul geonet will be placed over the 40 nul HDPE Secondary Liner.
- A 60 wil HDPE Primary lines will be placed over the 200 mil geonet drainage layer

If you have any questions on the above technical memorandum or require further information, give me a call at 720-289-0300 or email geosynthetics a man com-

Sincerely Yours,

2X Frolick

Ronald K. Frobel, MSCE, PE

References:

NMAC (9.15.34.12 A. DESIGN AND CONSTRUCTION SPECIFICATIONS FOR A RECYCLING-CONTAINMENT

Geosynthetic Research Institute (GRI) Published Standards and Papers 2017 www.geosynthetic-institute.org

ASTM Geosymbetics' Standards 2017 www.ASTM.org Standards





infestations. Choose any or all of the 8 sounds, including predators to

give the birds even more of a sense of danger. Customize by choosing volume and silent time between sounds.

Mega Blaster PRO

Complete system includes the generating unit with two built-in highoutput amplifiers, 20-speaker tower with audio cables, 40 watt solar panel, battery clips and all mounting hardware.



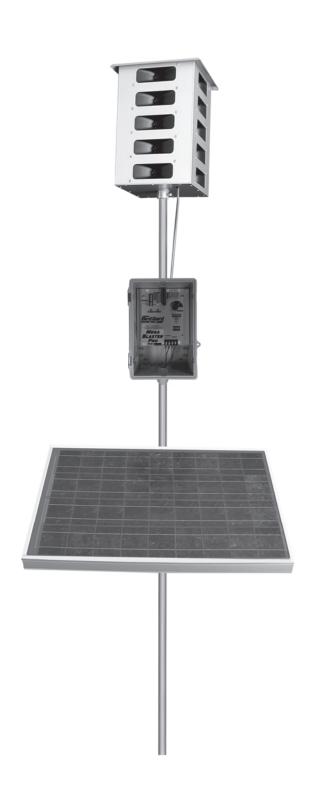


MEGA BLASTER PRO



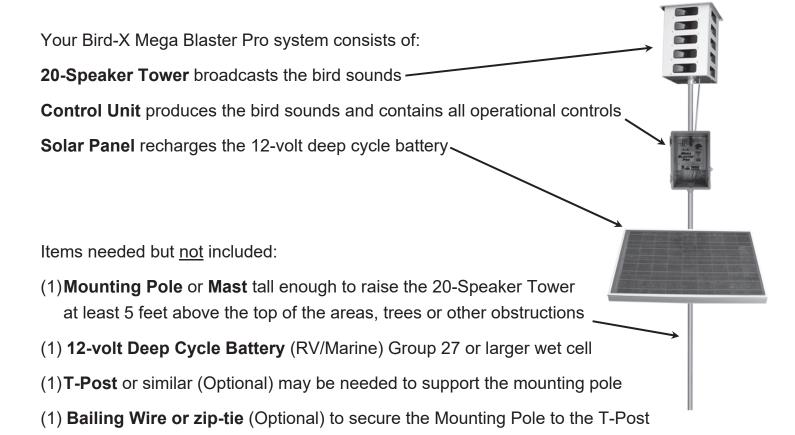
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Overview

The Bird-X Mega Blaster Pro utilizes the innate power of the natural survival instincts of birds to effectively repel them. Digital recordings of distressed and alarmed birds, along with the sounds made by their natural predators are broadcast through high fidelity weather-resistant speakers over the top of areas. This action triggers a primal fear and flee response. Pest birds soon relocate to where they can feed without feeling threatened.



CAUTION: THE MEGA BLASTER PRO IS CAPABLE OF PRODUCING SOUNDS UP TO 125 DECIBELS. PROPER HEARING PROTECTION MUST BE WORN ANYTIME THE UNIT IS TURNED ON.



Bird Control Management Guidelines

An active bird control management program is a key to successfully repelling pest birds. Bird feeding patterns may take several days or weeks to break. Follow all suggestions for maximum effectiveness. Read all instructions prior to installation.

For best results:

- It is extremely important to fully protect your entire area from birds. Any areas not fully protected will allow birds to begin feeding at the fringes of the sound coverage. They will soon become bolder and learn the sounds are nothing to fear. This will cause the effectiveness to diminish. Complete Bird-X product coverage forces birds to leave the area entirely.
- Install the Mega Blaster Pro unit at least two weeks before birds are attracted to your area. It is much easier to keep birds away before they have found a food source than it is to repel them once they have developed a feeding pattern.
- Most birds begin feeding from the perimeter of an area. Place Mega Blaster Pro units so the sound protection covers
 past the edges of the area.
- Birds will often use tall trees for roosting and observation. If birds are in bordering trees it is necessary to position the
 units so the sound protection covers the trees as well.
- Mount the 20-Speaker Tower at least five feet above trees, areas and structures for maximum coverage. The higher the better. Sound will disperse or reflect off structures or foliage. Mount control unit out of direct sun, if possible.
- When first installed, run Mega Blaster Pro units at FULL volume and on SHORT time off periods. This ensures maximum "bird stress" and creates a hostile environment.
- Watch for changes in bird activity and adjust the location of your Mega Blaster Pro unit if needed.
- Check the battery and unit settings often to insure continuous bird control. Be certain that the system is not turned down or has a dead battery. Field hands or harvesters may turn down the volume.
- Changing settings and switches often helps to prevent bird habituation. Periodically change the switch settings of the
 eight sounds (turning them ON or OFF). NEVER turn OFF the distress calls of the target birds you are trying to repel
 and always keep at least one predator bird sound turned ON.
- If different bird species enter the protected area and begin causing damage contact us immediately for an updated Sound Recording Card designed to repel the new invading birds.
- Remember that the Mega Blaster Pro system is a management tool, and should be used as part of your overall bird control strategy, sometimes in conjunction with other bird control techniques and devices.

Be aware that under extreme drought or other adverse conditions, birds will disregard all deterrents and risks in order to survive

DESIGN AND CONSTRUCTION PLAN OPERATION AND MAINTENANCE PLAN CLOSURE PLAN

g.

Recycling Facility and/or Containment Checklist:

Instructions: Each of the following items must be attached to the application. Indicate, by a check mark in the box, that the documents are attached.

- ☑ Design Plan based upon the appropriate requirements.
 ☑ Operating and Maintenance Plan based upon the appropriate requirements.
 ☑ Closure Plan based upon the appropriate requirements.
 ☑ Site Specific Groundwater Data ☑ Siting Criteria Compliance Demonstrations ☑ Certify that notice of the C-147 (only) has been sent to the surface owner(s)

Design and Construction Plan In Ground Containments

This plan addresses construction of the earthen containments.

Magrym Engineers is providing the design of the containment and their plans are presented in this submission.

Dike Protection and Structural Integrity

The design and operation provide for the confinement of produced water, prevention of releases and prevention of overtopping due to wave action or rainfall. Additionally, the design prevents run-on of surface water as the containment is surrounded by an above-grade levee (a berm) and/or diversion ditch (between the levee and the soil stockpile) to prevent run-on of surface water.

Stockpile Topsoil

Where topsoil is present, prior to constructing containment, the operator will strip and stockpile the topsoil for use as the final cover or fill at the time of closure.

Signage

The operator will place an upright sign no less than 12 inches by 24 inches with lettering not less than two inches in height in a conspicuous place on the fence surrounding the containment. The sign is posted in a manner and location such that a person can easily read the legend. The sign will provide the following information:

- the operator's name,
- the location of the site by quarter-quarter or unit letter, section, township and range, and
- emergency telephone numbers

Fencing

The operator will provide for a fence to enclose the recycling containment in a manner that deters unauthorized wildlife and human access. As specified in the design drawings, the operator will employ a chain-link or game fence in addition to a four foot, four-strand wire fence Because feral pigs, javelina and deer are present in the area, a chain link or game fence is required in order to comply with Section 19.15.34.12 D.1 of the Rule because pigs will move beneath the lower strand of a 4-strand, 4-foot high barbed wire fence and deer will jump over. However, 19.15.34.12 D.2 requires "a four-foot fence that has at least four strands of barbed wire evenly spaced in the interval between one foot and four feet above ground level". Therefore, the barbed wire specification is added to the game fence to avoid a variance. As stated in the O&M plan, the operator will ensure that all gates associated with the fence are closed and locked when responsible personnel are not onsite.

19.15.34.12 A Design and Construction Specifications

(1). The operator shall design and construct a recycling containment to ensure the confinement of produced water, to prevent releases and to prevent overtopping due to wave action or rainfall. (8). The operator of a recycling containment shall design the containment to prevent run-on of surface water. The containment shall be surrounded by a berm, ditch or other diversion to prevent run-on of surface water

19.15.34.12 B. Prior to constructing containment, the operator shall strip and stockpile the topsoil for use as the final cover or fill at the time of closure

19.15.34.12 C. Signs.

The operator shall post an upright sign no less than 12 inches by 24 inches with lettering not less than two inches in height in a conspicuous place on the fence surrounding the containment. The operator shall post the sign in a manner and location such that a person can easily read the legend. The sign shall provide the following information: the operator's name, the location of the site by quarter-quarter or unit letter, section, township and range, and emergency telephone numbers

19.15.34.12 D. Fencing

(1) The operator shall fence or enclose a recycling containment in a manner that deters unauthorized wildlife and human access and shall maintain the fences in good repair. The operator shall ensure that all gates associated with the fence are closed and locked when responsible personnel are not onsite.

(2) Recycling containments shall be fenced with a four-foot fence that has at least four strands of barbed wire evenly spaced in the interval between one foot and four feet above ground level.

Design and Construction Plan In Ground Containments

Netting and Protection of Wildlife

The perimeter game/chain-link fence will be effective in excluding stock and most terrestrial wildlife. If requested by the surface owner, the game fence can include a fine mesh from the base to 1 foot above the ground to exclude the small reptiles (e.g. dune sagebrush lizard).

The recycling containment will be protective of wildlife, including migratory birds_through the implementation of an Avian Protection Plan, routine inspections and the perimeter fence.

The avian protection plan includes the use of a Bird-X Mega Blaster Pro as a primary hazing program for avian species. The device will be equipped with sounds suitable for the Permian Basin environment. In addition to this sonic device, staff will routinely inspect the containment for the presence of avian species and, if detected, may use a blank cartridge or shell in a handgun, starter pistol or shotgun as additional hazing if necessary. Decoys of birds of prey may be placed on the game fence and other roosts around the open water to provide additional hazing.

The O&M plan calls for the operator to inspect for and, within 30 days of discovery, report the discovery of dead migratory birds or other wildlife to the appropriate wildlife agency and to the division district office in order to facilitate assessment and implementation of measures to prevent incidents from reoccurring.

This Avian Protection Plan meets the specific language of Rule 34 as it is "otherwise protective of wildlife, including migratory birds".

Earthwork

The containment will have a properly constructed foundation and interior slopes consisting of a firm, unyielding base, smooth and free of rocks, debris, sharp edges or irregularities to prevent the liner's rupture or tear. Geotextile is required under the liner when needed to reduce localized stress-strain or protuberances that otherwise may compromise the liner's integrity.

This volume provides the stamped drawings for the containment with the following design/construction specifications:

- a) levee has inside grade no steeper than two horizontal feet to one vertical foot (2H: 1V).
- b) levee outside grade is no steeper than three horizontal feet to one vertical foot (3H: 1V)

19.15.34.12 E Netting.

The operator shall ensure that a recycling containment is screened, netted or otherwise protective of wildlife, including migratory birds. The operator shall on a monthly basis inspect for and, within 30 days of discovery, report the discovery of dead migratory birds or other wildlife to the appropriate wildlife agency and to the division district office in order to facilitate assessment and implementation of measures to prevent incidents from reoccurring.

19.15.34.12 A

(2) A recycling containment shall have a properly constructed foundation and interior slopes consisting of a firm, unyielding base, smooth and free of rocks, debris, sharp edges or irregularities to prevent the liner's rupture or tear. Geotextile is required under the liner when needed to reduce localized stress-strain or protuberances that otherwise may compromise the liner's integrity...

19.15.34.12 A

(2) ...The operator shall construct the containment in a levee with an inside grade no steeper than two horizontal feet to one vertical foot (2H:1V). The levee shall have an outside grade no steeper than three horizontal feet to one vertical foot (3H:1V). The top of the levee shall be wide enough

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Design and Construction Plan In Ground Containments

- c) top of the levee is wide enough to install an anchor trench and provide adequate room for inspection and maintenance.
- d) The containment floor design calls for a slope toward the sump in the corner(s).

Liner and Drainage Geotextile Installation

The containment has a primary (upper) liner and a secondary (lower) liner with a leak detection system appropriate to the site's conditions.

The primary (upper) liner is a geomembrane liner composed of an impervious, synthetic material that is resistant to ultraviolet light, petroleum hydrocarbons, salts and acidic and alkaline solutions. It is 60-mil HDPE.

The secondary liner is specified in the design drawings and is 40-mil HDPE or thicker. Attached to the engineering drawings are specifications for this material, a professional opinion regarding the equivalency of 40-mil HDPE to 30-mil LLDPEr, and information on hydraulic conductivity. As stated in that opinion, liner compatibility meets or exceeds a subsequent relevant publication to EPA SW-846 method 9090A.

The recycling containment design has a leak detection system between the upper and lower geomembrane liners of 200-mil geonet to facilitate drainage. The leak detection system consists of a properly designed drainage and collection and removal system placed above the lower geomembrane liner in depressions and sloped to facilitate the earliest possible leak detection. The containment floor design calls for a slope toward the sump in the corner(s) of the containment, as shown in the design drawings. This slope combined with the highly transmissive geonet drainage layer provide for rapid leak detection.

The liners and drainage material will be installed consistent with the Manufacturer's specifications. In addition to any specifications of the Manufacturer, protocols for liner installation include measures to:

- i. minimizing liner seams and orient them up and down, not across, a slope of the levee.
- ii. use factory-welded seams where possible.
- iii. use field seams in geosynthetic material that are thermally seamed and prior to field seaming, overlap liners four to six inches.
- iv. minimize the number of field seams and comers and irregularly shaped areas.
- v. provide for no horizontal seams within five feet of the

to install an anchor trench and provide adequate room for inspection and maintenance.

19.15.34.12 A

(3) Each recycling containment shall incorporate, at a minimum, a primary (upper) liner and a secondary (lower) liner with a leak detection system appropriate to the site's conditions.

19.15.34.12 A

(4) All primary (upper) liners in a recycling containment shall be geomembrane liners composed of an impervious, synthetic material that is resistant to ultraviolet light, petroleum hydrocarbons, salts and acidic and alkaline solutions. All primary liners shall be 30-mil flexible PVC, 45-mil LLDPE string reinforced or 60-mil HDPE liners. Secondary liners shall be 30-mil LLDPE string reinforced or equivalent with a hydraulic conductivity no greater than 1 x 10-9 cm/sec. Liner compatibility shall meet or exceed the EPA SW-846 method 9090A or subsequent relevant publications.

19.15.34.12 A

(7) The operator of a recycling containment shall place a leak detection system between the upper and lower geomembrane liners that shall consist of 200-mil geonet or two feet of compacted soil with a saturated hydraulic conductivity of 1 x 10-5 cm/sec or greater to facilitate drainage. The leak detection system shall consist of a properly designed drainage and collection and removal system placed above the lower geomembrane liner in depressions and sloped to facilitate the earliest possible leak detection.

19.15.34.12 A

(5) The operator of a recycling containment shall minimize liner seams and orient them up and down, not across, a slope of the levee. Factory welded seams shall be used where possible. The operator shall ensure field seams in geosynthetic material are thermally seamed. Prior to field seaming, the operator shall overlap liners four to six inches...

19.15.34.12 A

(5) ...The operator shall minimize the number of field seams and corners and irregularly shaped areas. There shall be no horizontal seams within five feet of the slope's toe. Qualified personnel shall perform field welding and testing.

19.15.34.12 A

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Design and Construction Plan In Ground Containments

- slope's toe.
- vi. use qualified personnel to perform field welding and testing.
- vii. avoid excessive stress-strain on the liner
- viii. The edges of all liners are anchored in the bottom of a compacted earth-filled trench that is at least 18 inches deep

At points of discharge into the lined earthen containment the pipe configuration effectively protects the liner from excessive hydrostatic force or mechanical damage during filling.

The design shows that at any point of discharge into or suction from the recycling containment, the liner is protected from excessive hydrostatic force or mechanical damage. External discharge or suction lines do not penetrate the liner.

Pumping from the containment to hydraulic fracturing operations is the responsibility of stimulation contractors. Typically, lines are permanently placed in the containment with floats attached to prevent damage to the liner system. The containment may be equipped with permanent HDPE stinger (supported by a sacrificial liner or geotextile) for withdrawal of fluid if the owner deems necessary during operations.

Leak Detection and Fluid Removal System Installation
The leak detection system, contains the following design elements

- a. The 200-mil HyperNet Geonet drainage material between the primary and secondary liner that is sufficiently permeable to allow the transport of fluids to the observation ports (Appendix A).
- b. The containment floor is sloped towards the monitoring riser pipe to facilitate the earliest possible leak detection of the containment bottom. A pump may be placed in the observation port to provide for fluid removal.
- c. Piping will withstand chemical attack from any seepage, structural loading from stresses and disturbances from overlying water, cover materials, equipment operation or expansion or contraction (see Appendix A).

(3) The edges of all liners shall be anchored in the bottom of a compacted earth-filled trench. The anchor trench shall be at least 18 inches deep.

19.15.34.12 A

(6) At a point of discharge into or suction from the recycling containment, the operator shall insure that the liner is protected from excessive hydrostatic force or mechanical damage. External discharge or suction lines shall not penetrate the liner.

Overview

The operator will operate and maintain the lined earthen containment to contain liquids and solids (blow sand and minimal precipitates from the produced water) and maintain the integrity of the liner system in a manner that prevents contamination of fresh water and protects public health and the environment as described below. The purpose of the lined earthen containment is to facilitate recycling, reuse and reclamation of produced water derived from oil and gas wells. During periods when water for E&P operations is not needed, produced water will discharge to injection wells or to a pipeline for transfer to another recycling facility. The containment will not be used for the disposal of produced water or other oilfield waste.

The operation of the containment is summarized below.

- A. Produced water generated from nearby oil and gas wells is delivered to a treatment system located as indicated in the C-147.
- B. Unless specified in the transmittal letter, after treatment, the produced water discharges into the containment.
- C. When required, produced water is removed from the containment for E&P operations. At this time, produced water will be used for drilling beneath the freshwater zones (beneath surface casing), for well stimulation (e.g. hydraulic fracturing) and other E&P uses as approved by OCD.
- D. Whenever the maximum fluid capacity of the containment is reached, treatment and discharge to the containment ceases (see Freeboard and Overtopping Plan, below).
- E. The operator will keep accurate records and shall report monthly to the division the total volume of water received for recycling, with the amount of fresh water received listed separately, and the total volume of water leaving the facility for disposition by use on form C-148 (see attached example).
- F. The operator will maintain accurate records that identify the sources and disposition of all recycled water that shall be made available for review by the division upon request.

19.15.34.10 D Recycling containments may not be used for the disposal of produced water or other oilfield wastes.

19.15.34.9 E

The operator of a recycling facility shall keep accurate records and shall report monthly to the division the total volume of water received for recycling, with the amount of fresh water received listed separately, and the total volume of water leaving the facility for disposition by use on form C-148.

19.15.34.9 F

The operator of a recycling facility shall maintain accurate records that identify the sources and disposition of all recycled water that shall be made available for review by the division upon request.

G. The containment shall be deemed to have ceased operations if less than 20% of the total fluid capacity is used every six months following the first withdrawal of produced water for use. The operator will report cessation of operations to the appropriate division district office. The appropriate division district office may grant an extension to this determination of cessation of operations not to exceed six months.

The operation of the lined earthen containment will follow the mandates listed below:

- 1. The operator will not discharge into or store any hazardous waste (as defined by 40 CFR 261 and NMAC 19.15.2.7.H.3) in the containments.
- 2. If the containment's primary liner is compromised above the fluid's surface, the operator will repair the damage or initiate replacement of the primary liner within 48 hours of discovery or seek an extension of time from the division district office.
- 3. If the primary liner is compromised below the fluid's surface, the operator will remove all fluid above the damage or leak within 48 hours of discovery, notify the division district office and repair the damage or replace the primary liner.
- 4. If any penetration of the containment liner is confirmed by sampling of fluid in the leak detection system (see Monitoring, Inspection, and Reporting Plan; below), the operator will:
 - a. Begin and maintain fluid removal from the leak detection/pump-back system,
 - b. Notify the district office within 48 hours (phone or email) of the discovery,
 - c. Identify the location of the leak, and
 - d. Repair the damage or, if necessary, replace the containment liner.
- 5. The operator will install, or maintain on site, an oil absorbent boom or other device to contain an unanticipated release and the operator will remove any visible layer of oil from the surface of the recycling containment.
- 6. The operator will report releases of fluid in a manner consistent with NMAC 19.15.29
- 7. The containment will be operated to prevent the collection of surface water run-on.

19.15.34.13 C

A recycling containment shall be deemed to have ceased operations if less than 20% of the total fluid capacity is used every six months following the first withdrawal of produced water for use. The operator must report cessation of operations to the appropriate division district office. The appropriate division district office may grant an extension to this determination of cessation of operations not to exceed six months.

19.15.34.13 B

- (4) If the containment's primary liner is compromised above the fluid's surface, the operator shall repair the damage or initiate replacement of the primary liner within 48 hours of discovery or seek an extension of time from the division district office.

 (5) If the primary liner is
- (5) If the primary liner is compromised below the fluid's surface, the operator shall remove all fluid above the damage or leak within 48 hours of discovery, notify the division district office and repair the damage or replace the primary liner.

19.15.34.13 B

- (7) The operator shall install, or maintain on site, an oil absorbent boom or other device to contain an unanticipated release.
- (1) The operator shall remove any visible layer of oil from the surface of the recycling containment.
 19.15.34.8 A
- (6) All releases from the recycling and re-use of produced water shall be handled in accordance with 19.15.29 NMAC.

19.15.34.13

(6) The containment shall be operated to prevent the collection of surface water run-on.

- 8. The operator will maintain the containment free of miscellaneous solid waste or debris.
- 9. The operator will maintain at least three feet of freeboard for the containment and will use a free-standing staff gauge to allow easy determination of the required 3-foot of freeboard.
- 10. As described in the design/construction plan, the injection or withdrawal of fluids from the containment is accomplished through hardware that prevents damage to the liner by erosion, fluid jets or impact from installation and removal of hoses or pipes.
- 11. The operator shall ensure that all gates associated with the fence are closed and locked when responsible personnel are not onsite.
- 12. The operator will maintain the fences in good repair.

Monitoring, Inspection, and Reporting Plan

The operator will inspect the recycling containment and associated leak detection systems weekly while it contains fluids. The operator shall maintain a current log of such inspections and make the log available for review by the division upon request.

Weekly inspections consist of:

- reading and recording the fluid height of staff gauges,
- recording any evidence that the pond surface shows visible oil,
- visually inspecting the containment's exposed liners
- checking the leak detection system for any evidence of a loss of integrity of the primary liner.
- inspect diversion ditches and berms around the containment to check for erosion and collection of surface water run-on.
- inspect the leak detection system for evidence of damage or malfunction and monitor for leakage.

As stated above, if a liner's integrity is compromised, or if any penetration of the liner occurs, then the operator will take appropriate action within 48 hours, based on if above or below water surface, as noted above.

19.15.34.13 B

(2) The operator shall maintain at least three feet of freeboard at each containment.

19.15.34.13 B

(3) The injection or withdrawal of fluids from the containment shall be accomplished through a header, diverter or other hardware that prevents damage to the liner by erosion, fluid jets or impact from installation and removal of hoses or pipes.

19.15.34.12 D

(1) The operator shall fence or enclose a recycling containment in a manner that deters unauthorized wildlife and human access and shall maintain the fences in good repair. The operator shall ensure that all gates associated with the fence are closed and locked when responsible personnel are not onsite.

19.15.34.13 A

The operator shall inspect the recycling containment and associated leak detection systems weekly while it contains fluids. The operator shall maintain a current log of such inspections and make the log available for review by the division upon request.

Monthly, the operator will:

- A. Inspect the containment for dead migratory birds and other wildlife. Within 30 days of discovery, report the discovery of dead migratory birds or other wildlife to the appropriate wildlife agency and to the division district office in order to facilitate assessment and implementation of measures to prevent incidents from reoccurring.
- B. Report to the division the total volume of water received for recycling, with the amount of fresh water received listed separately, and the total volume of water leaving the facility for disposition by use on form C-148.
- C. Record sources and disposition of all recycled water.

The operator will maintain a log of all inspections and make the log available for the appropriate Division district office's review upon request. An example of the log is attached to this section of the permit application.

Freeboard and Overtopping Prevention Plan

The method of operation of the containment allows for maintaining freeboard with very few potential problems. When the capacity of the containment is reached (3-feet of freeboard), the discharge of produced water ceases and the produced water generated by nearby oil and gas wells is managed by an injection well(s).

If rising water levels suggest that 3-feet of freeboard will not be maintained, the operator will implement one or more of the following options:

- I. Cease discharging produced water to the containment.
- II. Accelerate re-use of the produced water for purposes approved by the Division.
- III. Transfer produced water from the containment to injection wells.

The reading of the staff gauge typically occurs daily when treatment operations are ongoing and weekly when discharge to the containment is not occurring.

19.15.34.12 E

The operator shall on a monthly basis inspect for and, within 30 days of discovery, report the discovery of dead migratory birds or other wildlife to the appropriate wildlife agency and to the division district office in order to facilitate assessment and implementation of measures to prevent incidents from reoccurring.

19.15.34.9 E

The operator of a recycling facility shall keep accurate records and shall report monthly to the division the total volume of water received for recycling, with the amount of fresh water received listed separately, and the total volume of water leaving the facility for disposition by use on form C-148.

19.15.34.9 F

The operator of a recycling facility shall maintain accurate records that identify the sources and disposition of all recycled water that shall be made available for review by the division upon request.

Protocol for Leak Detection Monitoring, Fluid Removal and Reporting

As shown in Appendix A, the leak detection system includes a monitoring system. Any fluid released from the primary liner will flow to the collection sump, where fluid level monitoring is possible at the monitoring riser pipe associated with the leak detection system.

Staff may employ a portable electronic water level meter to determine if fluid exists in the monitoring riser pipe. Obtaining accurate readings of water levels in a sloped pipe beneath a containment can be a challenge. An electrician's wire snake may be required to push the probe to the bottom of the port and the probe may be fixed in a 2-inch pipe "dry housing" to avoid false readings due to water condensation on the pipe. There are many techniques to determine the existence of water in the sumps – including low flow pumps and a simple small bailer affixed to an electrician's snake. The operator will use the method that works best for this containment.

If seepage from the containment into the leak detection system is suspected by a positive fluid level measurement, the operator will:

- 1. Re-measure fluid levels in the monitoring riser pipe on a daily basis for one week to determine the rate of seepage.
- 2. Collect a water sample from the monitoring riser pipe to confirm the seepage is produced water from the containment via electrical conductivity and chloride measurements.
- 3. Notify NMOCD of a confirmed positive detection in the system within 48 hours of sampling (initial notification).
- 4. Install a pump into the monitoring riser pipe sump to continually (manually on a daily basis or via automatic timers) remove fluids from the leak detection system into the containment until the liner is repaired or replaced.
- 5. Dispatch a liner professional to inspect the portion of the containment suspected of leakage during a "low water" monitoring event.
- 6. Provide NMOCD a second report describing the inspection and/or repair within 20 days of the initial notification.

If the point of release is obvious from a low water inspection, the liner professional will repair the loss of integrity. If the point of release cannot be determined by the inspection, the liner professional will develop a more robust plan to identify the point(s) of release. The inspection plan and schedule will be submitted to OCD with the second report. The operator will implement the plan upon OCD approval.

Quarterly Inspection Log Sheet - Containment

			, while fluids p		t); Monthly whe	n fluids <1 foot
Inspection	Inspector	Describe any 1. Tear of Liner 2. Proof in Porms and		Report Fluid Freeboard	Leak Detection System Functioning (yes/no)	
Date	(Initials)	2. Break in Berms and Run-on of Stormwater 3. Dead Wildlife 4. Oil on Fluid				Comments
		None	Yes			
		Observed	Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			
		None Observed	Yes Describe			

Weekly inspections consist of:

- reading and recording the fluid height of staff gauges,
- recording any evidence that the pond surface shows visible oil,
- visually inspecting the containment's exposed liners
- checking the leak detection system for any evidence of a loss of integrity of the primary liner
- inspect diversion ditches and berms around the containment to check for erosion and collection of surface water run-on.
- inspect the leak detection system for evidence of damage or malfunction and monitor for leakage.

Monthly, the operator will:

- A. Inspect the containment for dead migratory birds and other wildlife. Within 30 days of discovery, report the discovery of dead migratory birds or other wildlife to the appropriate wildlife agency and to the division district office in order to facilitate assessment and implementation of measures to prevent incidents from reoccurring.
- B. Report to the division the total volume of water received for recycling, with the amount of fresh water received listed separately, and the total volume of water leaving the facility for disposition by use on form C-148.
- C. Record sources and disposition of all recycled water.

Closure Plan In Ground Containments

Overview

After operations cease, the operator will remove all fluids within 60 days and close the containment within six months from the date the operator ceases operations from the containment for use.

The operator shall substantially restore the impacted surface area to

- a. the condition that existed prior to the construction of the recycling containment or
- to a condition imposed by federal, state trust land or tribal agencies on lands managed by those agencies as these provisions govern the obligations of any operator subject to those provisions,

The surface owner will impose a closure design that conforms to their needs for the site. The operator understands that a variance will be submitted to OCD to allow for any alternative closure protocol.

Excavation and Removal Closure Plan – Protocols and Procedures

The containment is expected to hold a small volume of solids, the majority of which will be windblown sand and dust with some mineral precipitates from the water

- 1. The operator will remove all liquids from the containment and either:
 - a. Dispose of the liquids in a division-approved facility, or
 - b. Recycle, reuse or reclaim the water for reuse in drilling and stimulation.
- 2. The operator will close the recycling containment by first removing all fluids, contents and synthetic liners and transferring these materials to a division approved facility.
- 3. After the removal of the containment contents and liners, soils beneath the containment will be tested by collection of a five-point (minimum) composite sample which includes stained or wet soils, if any, and that sample shall be analyzed for the constituents listed in Table I of 19.15.34.14.
- 4. After review of the laboratory results:
 - a. If any contaminant concentration is higher than the parameters listed in Table I, additional delineation may be required, and the operator must receive approval before proceeding with closure.

19.15.34.14 A

Once the operator has ceased operations, the operator shall remove all fluids within 60 days and close the containment within six months from the date the operator ceases operations from the containment for use.

19.15.34.14 E

The operator shall substantially restore the impacted surface area to the condition that existed prior to the construction of the recycling containment.

19.15.34.14 G

The re-vegetation and reclamation obligations imposed by federal, state trust land or tribal agencies on lands managed by those agencies shall supersede these provisions and govern the obligations of any operator subject to those provisions, provided that the other requirements provide equal or better protection of fresh water, human health and the environment.

19.15.34.14 B

The operator shall close a recycling containment by first removing all fluids, contents and synthetic liners and transferring these materials to a division approved facility.

19.15.34.14 C

The operator shall test the soils beneath the containment for contamination with a five-point composite sample which includes stained or wet soils, if any, and that sample shall be analyzed for the constituents listed in Table I below.

19.15.34.14 C

(1) If any contaminant concentration is higher than the parameters listed in Table I, the division may require additional delineation upon review of the results and the operator must receive approval before proceeding with closure.

Closure Plan In Ground Containments

- b. If all contaminant concentrations are less than or equal to the parameters listed in Table I, then the operator will proceed to
 - i. backfill with non-waste containing, uncontaminated, earthen material - Or
 - ii. undertake an alternative closure process pursuant to a variance request after approval by OCD.

Reclamation and Re-vegetation

- a. The operator will reclaim the containment's location to a safe and stable condition that blends with the surrounding undisturbed area.
- <u>b.</u> Topsoils and subsoils shall be replaced to their original relative positions and contoured so as to achieve erosion control, long-term stability and preservation of surface water flow patterns.
- c. The disturbed area shall then be reseeded in the first favorable growing season following closure of a recycling containment.

Closure Documentation

Within 60 days of closure completion, the operator shall submit a closure report on form C-147, including required attachments, to document all closure activities including sampling results and the details on any backfilling, capping or covering, where applicable. The closure report shall certify that all information in the report and attachments is correct and that the operator has complied with all applicable closure requirements and conditions specified in division rules or directives.

The operator shall notify the division when reclamation and revegetation are complete. Specifically the notice will document that all ground surface disturbing activities at the site have been completed, and a uniform vegetative cover has been established that reflects a life-form ratio of plus or minus fifty percent (50%) of predisturbance levels and a total percent plant cover of at least seventy percent (70%) of pre-disturbance levels, excluding noxious weeds.

19.15.34.14 C

(2) If all contaminant concentrations are less than or equal to the parameters listed in Table I, then the operator can proceed to backfill with non-waste containing, uncontaminated, earthen material.

19.15.34.14 E

Once the operator has closed the recycling containment, the operator shall reclaim the containment's location to a safe and stable condition that blends with the surrounding undisturbed area. Topsoils and subsoils shall be replaced to their original relative positions and contoured so as to achieve erosion control, long-term stability and preservation of surface water flow patterns. The disturbed area shall then be reseeded in the first favorable growing season following closure of a recycling containment.

19.15.34.14 D

Within 60 days of closure completion, the operator shall submit a closure report on form C-147, including required attachments, to document all closure activities including sampling results and the details on any backfilling, capping or covering, where applicable. The closure report shall certify that all information in the report and attachments is correct and that the operator has complied with all applicable closure requirements and conditions specified in division rules or directives.

19.15.34.14 H

The operator shall notify the division when reclamation and re-vegetation are complete.

19.15.34.14 F

Reclamation of all disturbed areas no longer in use shall be considered complete when all ground surface disturbing activities at the site have been completed, and a uniform vegetative cover has been established that reflects a life-form ratio of plus or minus fifty percent (50%) of predisturbance levels and a total percent plant cover of at least seventy percent (70%) of pre-disturbance levels, excluding noxious weeds.

C-147 Registration/Modification for Catalina Containment and Recycling Facility Addition of Containment #2 to 2RF-157 Section 30, T20S, R27E, Eddy County

Volume 2

Siting Criteria Demonstration Site Photographs 2020 and 2022 Appendix Well Logs



View south showing Catalina Containment #1 on the right just below the horizon. Catalina Containment #2 is proposed to the east (left) of Containment #1. The line of vegetation below the horizon is the mis-mapped USGS intermittent stream that is described in this registration.

Prepared for: Tascosa Energy LLC Midland, Texas

Prepared by: R.T. Hicks Consultants, Ltd. 901 Rio Grande NW F-142 Albuquerque, New Mexico

GENERAL SITING CRITERIA DEMONSTRATION AND SITE SPECIFIC GROUNDWATER DATA

& Siting Criteria for Recycling Containment	
Instructions: The applicant must provide attachments that demonstrate compliance for each siting criteria below as part of the appliexamples of the siting attachment source material are provided below under each criteria.	cation. Potential
General siting	
Ground water is less than 50 feet below the bottom of the Recycling Containment. NM Office of the State Engineer - iWATERS database search; USGS; Data obtained from nearby wells FIGURES 1-2	☐ Yes ⊠ No ☐ NA
Within incorporated municipal boundaries or within a defined municipal fresh water well field covered under a municipal ordinance adopted pursuant to NMSA 1978, Section 3-27-3, as amended. - Written confirmation or verification from the municipality; written approval obtained from the municipality FIGURE 3	☐ Yes ⊠ No ☐ NA
Within the area overlying a subsurface mine. - Written confirmation or verification or map from the NM EMNRD-Mining and Minerals Division FIGURE 4	☐ Yes ⊠ No
Within an unstable area. - Engineering measures incorporated into the design; NM Bureau of Geology & Mineral Resources; USGS; NM Geological Society; topographic map FIGURE 5	☐ Yes ⊠ No
Within a 100-year floodplain FEMA map FIGURE 6	☐ Yes ⊠ No
Within 300 feet of a continuously flowing watercourse, or 200 feet of any other significant watercourse, or lakebed, sinkhole, or playa lake (measured from the ordinary high-water mark). Topographic map; visual inspection (certification) of the proposed site FIGURE 7	☐ Yes ⊠ No
Within 1000 feet from a permanent residence, school, hospital, institution, or church in existence at the time of initial application. Visual inspection (certification) of the proposed site; aerial photo; satellite image FIGURE 8	☐ Yes ⊠ No
Within 500 horizontal feet of a spring or a fresh water well used for domestic or stock watering purposes, in existence at the time of initial application. FIGURES 1 and 7 NM Office of the State Engineer - iWATERS database search; visual inspection (certification) of the proposed site	☐ Yes ⊠ No
Within 500 feet of a wetland. FIGURE 9 US Fish and Wildlife Wetland Identification map; topographic map; visual inspection (certification) of the proposed site	☐ Yes ⊠ No

Introduction to C-147 Modification for Catalina #2 Containment

Except where identified, the text presented in the next sections is identical to the original 2021 submission that OCD signed on March 15, 2021. In general, large-scale features described herein are unchanged - such as depth to groundwater, karst and unstable ground, floodplains, etc. Neither the text nor the Figures are replaced for large-scale features – thus the term "containment" is singular to maintain consistency with the portion of this submission that OCD has previously approved. Below is a description of changes to the Siting Criteria Demonstration.

Figure 7a REV and 7b REV show the location of mapped watercourses relative to the Catalina Containments #1 and #2 Containment. The expanded facility remains more than 200 feet from the mapped watercourse and the mapped watercourse remains a mistake on the USGS 7.5 minute topographic map. The Appendix Site Photographs provides recent documentation of the absence of any bed or bank in this swale. The swale probably transmits water during large precipitation events.

The site photographs and Figure 7b provide evidence that small channels north of the Catalina Containment do not pose any risk of erosion. These channels are limited to the south facing bedrock hillside and the alluvial fan at the base of the hill. All of the observed channels die out 300-500 feet north of the containment where the change of slope causes flow to slow and allows infiltration of water into the alluvium. In Figure 7b, a change in vegetation marks the southern edge of the alluvial fan at the break in slope.

Figure 8 REV uses the same aerial image as the 2021 submission. Our field investigation and site photographs demonstrate that the area of Containment #2 has not changed. The Appendix Site Photos shows the location of the 2022 images. Containment #1 is present in these images.

Figure 9 REV presents mapped New Mexico wetlands, all of which are restricted to the Pecos River valley. In the 2021 submission, Figure 9 presented mapped wetlands from the USA database. Over the course of 2021, our site investigation routinely documented gross errors in the USA database while the New Mexico database was correct. This submission includes the 2021 version of Figure 9 after Figure 9 REV. The USA database indicates the erroneously mapped USGS intermittent stream is also a wetland. The Site Photos from 2021 and 2022 clearly show the error of the USA wetlands database.,

Geology

According to the State of New Mexico Geologic Map¹, Permian Age Tansill and Yates Formations (Pty) are exposed at the location of the proposed Catalina containment with Quaternary Alluvium (Qa) overlying Permian Salado Formation south of the containment location (Figure A1). In the northwest corner of the map, the map shows exposed Permian Seven Rivers Formation exposed on the south and eastern shore of (former) Lake McMillan. The Permian Salado Formation, which overlies the Tansill, is exposed along the east of the map. Also shown in Figure A1 are the Major Johnson Springs, along the Pecos River downstream from (former) Lake McMillian. Figure A2 shows Brantley Dam, Brantley Lake, and the absence of Lake McMillian on a recent air photograph.

¹ https://geoinfo.nmt.edu/publications/maps/geologic/state/home.cfml

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The Lake McMillan South 7.5-minute geologic quadrangle map² presents a slightly different interpretation of the geology and the differences are best understood by examining Figures 1a and 1b. The quadrangle map shows the containment is adjacent to and south of outcropping Tansill formation (Pt) and is within Quaternary (Pleistocene?) alluvium and eolian deposits. North of the containment location, the quadrangle map suggests the aeolian and alluvium is a thin veneer over the Tansill Formation (Qaes/Pt) and, further to the northwest, the veneer overlies the mixed gypsiferous facies of the Yates Formation (Pymg). In the eastern third of Figure 1b, the map shows the aeolian and alluvium overlying the Permian Salado Formation (Qaes/Ps) as well as exposed Salado. The contact between the Salado and underlying Tansill Formation (beneath the Quaternary veneer) is shown as a dashed line that runs through the northern boundary of the containment area.

The quadrangle map suggests that beneath the Quaternary deposits south of the proposed containment is probably the Salado Formation or the lower Rustler Formation — as the map does not differentiate between these two units in the legend. The legend describes these undifferentiated units as:

Irregular masses of gypsum, dolomite (Prc), and salt in large blocks scattered on surface and outcrops with chaotic bedding orientations. Exposed in eastern and southern part of quadrangle.

Finally, south of the containment area the map shows an elongated exposure of Quaternary (Pleistocene) alluvial gravel (Qqg). Our examination of this exposure confirms the presence of alluvial material that is consistent with the map description of Qagp2, which is presented below:

Qagp2-alluvial sand and gravel piedmont (Pleistocene) Gray to yellow gravel, poorly sorted, angular to subrounded dolomite clasts. Sand composed of quartz and locally carbonate cemented. Thickness 0->~75 m.

Figure SP-1 and SP-2 (Site Photographs) show the nature of the exposed alluvial material. Qagp2.

An important feature of the Tansill, Yates and Seven Rivers Formations is the two different depositional and therefore hydrogeologic facies that exist between Lake McMillan and Carlsbad. All of these stratigraphic units are composed dominantly of carbonate rocks adjacent to but northwest of the Capitan Reef (beneath Carlsbad). Further north and west of the Capitan Reef, which was a barrier reef of the deeper marine environment of the Delaware Basin, each of these three "back-reef" formations transition from shallow water carbonates rocks to shallower water shelf evaporites of the marine shelf that surrounds the basin. In the immediate area of the Catalina containment, the Tansill contains carbonate rocks (dolomite) and gypsum-rich siltstones, suggesting a transition or mix between the two facies.

²

 $[\]frac{\text{https://www.google.com/url?sa=t\&rct=j\&q=\&esrc=s\&source=web\&cd=\&cad=rja\&uact=8\&ved=2ahUKEwjeoZGvofHtAhUDOs0KHRHgAx4QFjAAegQIBBAC\&url=https%3A%2F%2Fgeoinfo.nmt.edu%2Fpublications%2Fmaps%2Fgeologic%2Fofgm%2Fdownloads%2F97%2FLakeMcMillanSouthReport.pdf&usg=AOvVaw1f9T38Bdxz0Sb37DnQTc71}$

We logged the cuttings of a 120-foot auger-drilled boring for the conductor pipe of the Catalina oil well that is adjacent to the proposed containment. The log of the boring is presented in Appendix Well Logs, and is presented below:

10-18 feet	Alluvium: brown, fine sand; caliche
18-63 feet	Tan, loose siltstone with 10-30% interbedded green-gray dolomite. Dolomite
	beds are massive (1 mm-5 cm vesicles observed at 40 ft, most filled with
	siltstone)
63-68 feet	Red, massive clay; minor tan silt, loose
68-74 feet	Red, massive clay; clast and veins of white and clear gypsum/selenite
74-94 feet	Massive purple-red clay interbedded with white and pink gypsum; <5% green
	"sugar" dolomite clasts
94-110 feet	Loose, medium red silt interbedded; 30% green/gray/yellow vesicular (1-2 mm)
	dolomite
110-113 feet	Red-brown silt with thin layers of red-brown siltstone and gypsum (1-2 mm thick)
113-120 feet	Dark red silt interbedded with 40% dolomite, green-gray, massive
120 feet	Dust dry cuttings

The geology of the area near the containment is also described in the Karst section of this submission.

Distance to Groundwater

Figures 1a, 1b, 2a and 2b, with the discussion below demonstrates that groundwater (fresh water as defined by NMOCD Rules) at the location is greater than 100 feet beneath the containment. A boring located several hundred feet due south of the proposed containment verify that groundwater is greater than 120 feet below land surface.

Figure 1a is topographic map with the New Mexico state geologic map that shows:

- 1. The Catalina containment identified by the turquoise square.
- 2. Water wells from the OSE database as a blue triangle inside colored circles that indicate well depth (CP and C). OSE wells are often miss-located in the WATERS database as older wells are plotted in the center of the quarter, quarter, quarter, of the Section Township and Range.
- 3. Water wells from the USGS database as large triangles color-coded to the formation from which the well draws water.
- 4. Water wells, which are not documented in the public databases but were identified by field inspection or other published reports as colored squares (MISC).
- 5. The depth-to-water from the most recent available measurement for each well is provided adjacent to the well symbol.

Figure 1b shows the same data as Figure 1a on a recent aerial photograph that shows Brantley Dam, Brantley Lake, and the absence of Lake McMillan.

Figure 2a is a water table elevation map that reproduces Plate 4 of in *Geology and Hydrology Between Lake McMillan and Carlsbad Springs Eddy County, New Mexico, Water Supply Paper 1828, 1967*³. Note that the two "zones" (2 and 4) are identified east of the Pecos River on

³ https://pubs.er.usgs.gov/publication/wsp1828

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the map between Lake McMillian (now silted in due to the development of Brantley Lake) and Lake Avalon.

Zone 2 is described in WSP 1828 as a karst aquifer in the evaporite faces of the Seven Rivers Formation that captures seepage from Lake McMillian, via sinkholes in some areas near and beneath the lake and transmits the water to Major Johnson Springs. WSP 1828 states that the eastern boundary of Zone 2 is defined by the transition from the evaporite facies to the carbonate facies of the Seven Rivers Formation. Because the hydraulic conductivity of the carbonate facies is many times lower than the karstic aquifer of the evaporite facies, groundwater water levels are almost 100 feet lower in wells to the southeast of the Zone 2 boundary, in Zone 6 and Zone 4. The transition zone between evaporite facies and carbonite facies of the Seven Rivers Formation is the location of Brantley Dam. The Bureau of Reclamation selected this location in order to minimize water loss via the karst aquifer of the Seven Rivers Formation. Zone 2 is not materially important to understanding the groundwater system beneath the Catalina containment.

The Catalina containment is within Zone 4, which is described as groundwater in the Yates and Tansill Formations between Major Johnson Springs (now Brantley Dam) and Lake Avalon. WSP 1828 indicates that the Tansill is above the regional water table and groundwater in the Yates flows generally through solution channels.

USGS-10009, plots 1.5 miles west of the Catalina containment. This location is in the USGS database, in WSP 1828, and was measured in 2015, but we found no evidence of this well on Google Earth. For reasons explained below, we believe this well does exist near the location plotted on the maps.

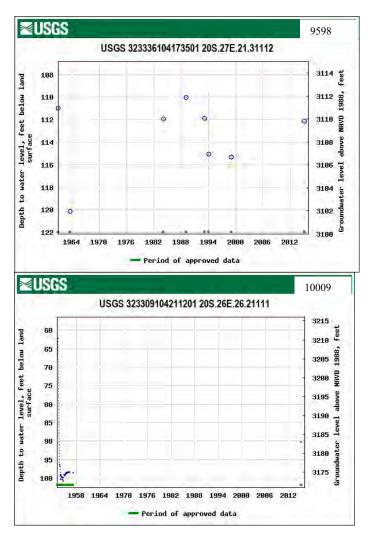
Figure 2b is the 7.5-minute quadrangle geologic map that shows:

- 1. The Catalina containment identified by the turquoise square with a measured surface elevation of 3242.
- 2. Water wells measured by the USGS, the year of the measurement and the calculated elevation of the groundwater surface.
- 3. Isocontour lines displaying the elevation of the groundwater surface in Permian the Yates and Tansill Formations east of the Pecos River. Note that the contour interval is 10 feet.

We relied upon the most recent data measured by the USGS and published data. Field examination of wells with older measurements indicated that a current measurement of depth to groundwater was not feasible. Water level data from the OSE database rely upon observed water levels by drillers during the completion of the water well. The OSE dataset provides some useful data in certain areas, but these data were not used to develop the groundwater elevation data of Figure 2b. Based upon our field survey and examination of Google Earth images, we are confident that the wells shown Figure 2b are located less than ½ mile of the plotted point, except as noted above for USGS-1009.

Because much of the groundwater elevation data on Figure 2b are decades old, we evaluated historical data from USGS-9598⁴, which is presented in the graph to the right. The water elevation in this well varies by 10 feet over the 55-year measurement record. Because Figure 2b presents a contour interval of 10 or 60 feet, this variation of measurement observed in USGS-9598 is not material.

As indicated above, we could not find USGS-10009 in the field. The graph below shows that historic observations agree with detailed water level measurements required in advance of selection of a location for Brantley Dam. The measurements also show, with the exception of the first measurement in March of 1953 (which we suspect was obtained immediately after drilling this well), that groundwater levels vary by 10 feet between the early measurements and the 2015 measurement. Like well USGS-10009, groundwater elevations are stable over time.



These data and the 120-foot-deep auger boring conducted for the conductor pipe for the oil well adjacent to the containment (see Appendix Well Logs) allow us to confidently conclude:

- 1. Groundwater elevation beneath the proposed containment is lower than 3115 feet above sea level.
- 2. The surface elevation of the 120-foot conductor pipe boring for the Catalina 30 EH State 1H is 3244.
- 3. At 120-feet, the auger boring cuttings were dust dry.
- 4. The containment is located north (uphill) of this well.
- 5. The depth from the proposed bottom of a 25-foot-deep containment is greater than 120 feet.

⁴ https://nwis.waterdata.usgs.gov/nwis/gwlevels/?site no=323336104173501

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Distance to Municipal Boundaries and Fresh Water Fields

Figure 3 demonstrates that the location is not within incorporated municipal boundaries or within defined municipal fresh water well fields covered under a municipal ordinance adopted pursuant to NMSA 1978, Section 3-27-3, as amended.

- The closest municipality is Carlsbad, NM approximately 12.5 miles to the south.
- The closest public well is CP-0076 and is located 6.9 miles to the southeast.
- The closest well fields are west of Carlsbad.

Distance to Subsurface Mines

Figure 4 and our general reconnaissance of the area demonstrate the proximity of surface mines to the containment. This location is not within an area overlying a subsurface mine.

• The nearest mapped surface mine is approximately 3.3 miles to the southwest of the Catalina containment.

Distance to High or Critical Karst Areas

The presence of karst features within an area proposed for the storage of treated recycle water for E&P (e.g., hydraulic stimulation) can be problematic for two reasons. First, as suggested in Part 34.11 of OCD Rules, a produced water recycling containment must be located within a stable area. For the benefit of our clients, a portion of Part 34 is presented below with **emphasis** <u>added</u>:

19.15.34.11 SITING REQUIREMENTS FOR RECYCLING CONTAINMENT:

- A. An operator shall **not locate a recycling containment**:
- (8) within an unstable area unless the operator demonstrates that it <u>has incorporated</u> engineering measures into the design to ensure that the containment's integrity is not compromised;

Unstable area is defined in 19.15.2.7 as

U.(6) "Unstable area" means a location that is susceptible to natural or human-induced events or forces capable of impairing the integrity of some or all of a division-approved facility's structural components. **Examples of unstable areas are** areas of poor foundation conditions, areas susceptible to mass earth movements and **karst terrain** areas where karst topography is developed as a result of dissolution of limestone, dolomite, or other soluble rock. Characteristic physiographic features of karst terrain include sinkholes, sinking streams, caves, large springs, and blind valleys.

In addition to potential instability of the containment foundation, karst features, such as sinkholes, open fractures or other conduits can provide a direct link between the surface and groundwater. Thus, a release from the containment within an area of high karst could introduce a large volume of saline water to an underlying water table aquifer over a relatively short time.

Caverns, interconnected cavities, sinkholes, and strata deformation due to dissolution of the limestone, dolomite, and gypsum are described in *Geology and Hydrology Between Lake McMillan and Carlsbad Springs Eddy County, New Mexico, Water Supply Paper 1828, 1967* within all of the Permian strata in the area of the proposed containment. WSP 1828 describes groundwater flow through interconnected karst features in the Seven Rivers Formation in the area that is now covered by Brantley Lake. WSP 1828 states that interconnected solution

features in carbonate rocks of the Tansill and Yates Formations transmit groundwater between Major Johnson Springs (now beneath Brantley Lake) and Lake Avalon and thence to Carlsbad Springs. However, WSP 1828 also indicates that the Tansill Formation is generally above the water table in the area north and west of Lake Avalon, except where perched water may exist in drainages, such as Dagger Draw.

The area of the proposed containment is correctly mapped by the BLM as high karst potential as it relates to drilling surface casing for an oil well and the potential for lost circulation into open fractures or cavities. However, the data and discussion below permit a conclusion that geologic evidence does not support a classification of this area as "high karst potential" <u>as it applies to the two characteristics described above</u>: near-surface ground instability and conduits between the ground surface and groundwater.

Figures 5a and 5b show the location of the Catalina storage containment with respect to BLM Karst areas. The proposed containment is located within an area mapped by BLM as "high" potential karst area (Figure 5a). About 1.5 miles east of the proposed containment BLM maps the area as moderate potential karst and critical karst is about 2 miles south. Figure 5a shows the containment within the exposed Permian Tansill and underlying Yates Formations (Pty). East of the containment, the Permian Salado Formation (Psl) is exposed. The Permian Seven Rivers Formation underlies the Yates Formation and is mapped in the northwest quadrant of Figure 5a. Quaternary Alluvium is in the Pecos River Valley and the Dagger Draw, which are south and east of the proposed containment. The large-scale State of New Mexico geologic map is the source of the data for Figure 5a.

Figure 5b shows the geology from the Lake McMillian South 7.5-minute geologic map⁵, which is a more detailed presentation than the state map. The boundaries between High, Moderate and Critical karst areas are also shown on the map. On Figure 5b, the containment lies on the contact between the upper Tansill and overlying Salado Formation. North and west (down section) from the containment, the map shows Quaternary alluvial and eolian deposits are a relatively thin veneer over the Tansill (Pt) and Yates Formations (Pymg, mixed silty gypsiferous facies). In the northwestern corner of Figure 5b the Azotea Tongue dolomite crops out.

With respect to ground instability and susceptibility of a water table aquifer to deleterious impacts from the containment, the nature of the Tansill Formation is most important and, to a lesser degree, the overlying alluvium, and underlying Yates Formation. The lithology of the two Permian bedrock units is described below verbatim from the Lake McMillan South geologic map.

Ptmsg---Tansill Formation—mixed silty gypsiferous facies (Guadalupian)--Mixed dolomite, sandy siltstone, and gypsum. White to light gray dolomite, thinly to medium bedded, vesicular, associated with yellow sandy dolomite and dolomitic sandstones in float. Well sorted, sublitharenite, chert grains, orange-red, interbedded with gypsum and white to light gray dolomite. Poorly exposed.

 $\frac{https://www.google.com/url?sa=t\&rct=j\&q=\&esrc=s\&source=web\&cd=\&cad=rja\&uact=8\&ved=2ahUKEwiumJKZ\\kNbtAhWVKM0KHaw9AmsQFjABegQIBRAC\&url=https%3A%2F%2Fgeoinfo.nmt.edu%2Fpublications%2Fmaps%2Fgeologic%2Fofgm%2Fdetails.cfml%3Fvolume%3D97\&usg=AOvVaw1IIvDIrDSQn8s2aB_s5yfN}$

⁵

_

Pymg---Yates Formation—mixed gypsiferous facies (Guadalupian)--Gypsum with minor dolomite, siltstone, and sandstone. green to white to red gypsiferous siltstone to silty gypsum to pure gypsum in 2-m-thick intervals interbedded with orange-red siltstone or dolomite. Gypsum is typically massive or has fibrous radiating crystals up to cms in dia. Locally brecciated. Gypsum is also interbedded with dolomite in thin beds. Gypsum veins also present. Dolomite is pink to salmon to very light gray, massive to vesicular, thinly bedded, and exhibits local chicken wire textures, rippenstein weathering, and crinkly laminations. Sandstone is yellow, locally silica cemented. Gypsum interbedded with dol and siltstone on a m scale. Folded into domes and basins. This facies makes up the strike valley and low hills paralleling, and SE of, the Lake McMillan escarpment. Forms caverns.

(Pyms or) Psd---(Yates Formation—mixed facies or) Azotea Tongue dolomite (of Kelley 1971) (Guadalupian)--Dolomite with interbedded siltstone, sandstone, and gypsum. Dolomite is thinly to thickly bedded, massive, yellow to light gray to pink to orange, vesicular, silty, clayey, very finely crystalline to sugary, undulose bedding, paper lams, crinkly lams, interbedded with thin to medium beds of pink dolomitic siltstone or green shale or yellow sandstone. Some very thin beds of gypsum.

As stated above, caverns form in the Yates Formation within the Lake McMillan South map. The description does not suggest caverns within the Tansill Formation. The map description indicates the lithology of the Tansill is dolomite and sandy siltstone with (probably) a lesser volume of more soluble gypsum. The boring to 120-feet agrees with the map description. Gypsum is the dominant lithology of the upper Yates Formation. Thicknesses of these two units are not provided in the legend for the Lake McMillian South map. However, the geologic cross-section with the map suggests the Tansill Formation is about 200 feet thick and the thickness of the underlying Yates Formation is approximately 300 feet.

The alluvium mapped in Figure 5b that is relevant to this analysis is Qaes and Qag. As indicated in the geology section, Qagp2 is exposed south of the containment and the description of this unit is repeated below.

Qagp2-alluvial sand and gravel piedmont (Pleistocene) Gray to yellow gravel, poorly sorted, angular to subrounded dolomite clasts. Sand composed of quartz and locally carbonate cemented. Thickness 0->~75 m.

The alluvium mapped as Qaes is described below from the Lake McMillan South Geologic Map. Qaes-alluvial and eolian deposits (Pleistocene (?) to Holocene)-Brown (7.5 YR 6/4), silty clay to silt to sand, well sorted, subangular to subrounded grains composed of 70% quartz and 30% carbonate and chert. Unit locally weathers into badlands and exhibits piping. Common veneer on nearly all Quaternary deposits in the map area and commonly overlies Psg and Pymg. Thickness ≤10 m.

As suggested in the title, *Geology and Hydrology Between Lake McMillan and Carlsbad Springs Eddy County, New Mexico, Water Supply Paper1828, 1967* provides some good information regarding the geohydrology of the area. However, the geologic map of this report does not agree with the 7.5-minute quadrangle referenced above or the New Mexico state geologic map. The location of the containment, Section 30 (20S 27E), is shown as underlain by the Yates Formation in WSP 1828 and the Tansill Formation in the 7.5-minute quadrangle and the state geologic map.

While we are skeptical of the mapping and cross-section provided in WSP 1828, we believe the lithologic descriptions, which appear to be based upon outcrop, are be accurate. We are confident that the descriptions of the different facies of the Tansill and Yates Formations are accurate as it would be based upon previous studies of others and observations within the area of study. Moreover, the description of the two facies, carbonate and evaporite, make perfect sense with respect to their depositional environment. However, the location of the facies changes for the various formations described in the report cannot be accurate, because the geologic mapping is not accurate.

WSP 1828 accurately describes how the facies of the Tansill and underlying Yates formation change from a dominate carbonate lithology in the shelf immediately behind the Capitan barrier reef complex that defines the margin of the Delaware Basin to a shallow water evaporite facies that is dominated by calcium sulfate evaporites (e.g., gypsum). As the lithologic descriptions presented above testify, around the proposed containment, the Tansill is comprised of dolomite, siltstone, and gypsum (mixed silty gypsiferous facies) and the underlying upper Yates is dominantly gypsum (mixed gypsiferous facies).

As stated earlier, the lithology of the boring is consistent with the description of the Tansill Formation mixed silty gypsiferous facies from the South McMillan Lake 7.5-minute geologic quadrangle map. The boring did not encounter any large voids. We believe the description of the underlying Yates Formation from the 7.5-minute quadrangle map (above) is accurate. The boring also confirms that depth to groundwater near the containment exceeds 120 feet from ground surface.

Although solution cavities in dolomite (carbonate facies) of the Tansill Formation transmit groundwater from Lake Avalon to Carlsbad Springs, WSP 1828 indicates that the containment lies within the carbonate facies of the Tansill and is obviously below the water table.

Our surface investigation found no evidence of karst geomorphology overlying the Tansill Formation or the Quaternary deposits.

The discussion above supports the following conclusions regarding the area near the proposed containment Section 30 (20S 27E):

- 1. About 20 feet of alluvium and caliche overlie the Tansill Formation at the site of the containment
- 2. At least 100-feet of unsaturated Tansill Formation exist beneath the Quaternary deposits.
- 3. The depth to groundwater near the containment is greater than 120 feet.
- 4. The interbedded dolomite, siltstone, and gypsum of the Tansill do not exhibit any open solution features that could transmit water from near surface to groundwater.
- 5. There is no evidence from examination of the ground surface, or the lithology observed in the boring that Permian Tansill Formation
 - a. is or could be unstable.
 - b. Does not exhibit solution features that could transmit fluid from the surface to groundwater.

The State Land Office requested an examination of the area south of the proposed containment for near-surface karst features where Tascosa proposes a natural gas pipeline between the new well and larger pipeline system. The presence of the sand and gravel outcrop (Qagp2) near the proposed pipeline testifies to the presence, probably in the Pleistocene, of a water flow. The subrounded dolomite cobbles observed in the gravel match the dolomite observed in the mapped exposure of Salado Formation to the east. Alluvial sand and gravel overlying the lowermost Salado Formation suggests to us that Pleistocene surface water flow or groundwater flow dissolved and removed any soluble constituents of the Salado in this area. Thus, it is not surprising that we found no evidence of subsidence or unstable ground in this area of the proposed pipeline.

We conclude with a high degree of scientific certainty that the proposed right of way for the pipeline lies within stable ground.

Distance to 100-Year Floodplain

Figure 6 demonstrates that the location is not located in a 100-year floodplain.

• The nearest 100-year floodplain is located approximately 1 mile to the east.

Distance to Surface Water

OCD Rule 34 establishes a 200-foot setback distance from "significant watercourse", which is defined in Rule 17 as:

P. "Significant watercourse" means a watercourse with a defined bed and bank either named or identified by a dashed blue line on a USGS 7.5-minute quadrangle map or the next lower order tributary with a defined bed and bank of such watercourse.

And 19.15.2.7 of OCD Rules define watercourse as:

(4) "Watercourse" means a river, creek, arroyo, canyon, draw or wash or other channel having definite banks and bed with visible evidence of the occasional flow of water.

The USGS defines bank in https://water.usgs.gov/water-basics_glossary.html as: Bank - The sloping ground that borders a stream and confines the water in the natural channel when the water level, or flow, is normal.

The USGS Glossary provides no definition for streambed. Definitions that use the term bed or stream bed, which are presented below, assume a "stream bed or streambed is the channel bottom of a stream or river, the physical confine of the normal water flow". The definition in quotations is from Wikipedia and the terms in the USGS glossary that employ "streambed" are:

- Bed material Sediment composing the streambed.
- Bed sediment The material that temporarily is stationary in the bottom of a stream or other watercourse.
- Bedload Sediment that moves on or near the streambed and is in almost continuous contact with the bed.

We understand that the USGS employs topographic maps, aerial photographs, and general knowledge of the various areas of the United States to map ephemeral streams. EPA noted that

the mapping protocol can underestimate the number of ephemeral streams. In New Mexico, Hicks Consultants ground surveys identified several instances where the USGS mapping was not accurate. As discussed below, we conclude the mapped watercourse in the area of concern is one such error in mapping.

We carefully examined the mapped watercourse on the ground in November 2020 and in 2022 paying special attention to areas of concern for siting of Containment #1 (2020) and Containment #2 (2022). The subject area of field investigation includes one mapped watercourse shown in Figure 7a REV. This topographic map shows most of the drainage basin and the mapped watercourse. About 220 feet north of the watercourse is the area where Tascosa Energy constructed the in-ground Catalina Containment #1 and will construct Catalina Containment #2. Figure 7b REV is larger scale image of a recent air photograph showing the mapped watercourse and erosional channels to the east and north.

Figures SP-3 and SP-4 in the 2020 Site Photos Appendix show the nature of the lowest elevation areas of the mapped watercourse. No bed or bank exists and there is no evidence of water flow. We conclude that the USGS mapping of an ephemeral stream in this channel is incorrect. Stormwater flows in the channel only during large precipitation events. Neverhless, the area in of the containment(s) meets the 200-foot setback requirement of Rule 34. Figure 22SP-5 of the 2022 Site Photos also demonstrates the lack of a stream or a wetland (Figure 9 REV).

Figure SP-5 (2020) shows the nature of an area that appears on Google Earth as a possible "next order tributary" of the mapped watercourse. The swale in which the cattle track lies is barely perceptable and there is no evidence of flow. During a 100-year or 500-year precipitation event, some water may flow in this swale. The engineering design diverts possible flow from this swale to the north, into a larger swale that is also a cattle track.

In 2022, we examined channels north and uphill of the proposed Catalina Containment #2. Channels indicative of water flow exist within the active alluvial fan, which is defined in the Appendix Site Photographs for 2022. No channels extend south of the break in slope between the distal edge of the fan and the north edge of the area surveyed for Containment #2.

Distance to Permanent Residence or Structures

Figure 8 REV and the site visit demonstrates that the location is not within 1000 feet from an occupied permanent residence, school, hospital, institution, church, or other structure in existence at the time of initial application.

- No occupied permanent residences, schools, hospitals, institutions, churches, or other structures are located within 1000 feet of the site.
- The closest structure to the proposed Catalina #2 Containment is the existing Catalina Containment #1

Distance to Non-Public Water Supply

Figures 1 and 7 REV demonstrates that the location is not within 500 horizontal feet of a spring or fresh water well used for domestic or stock watering purposes, in existence at the time of initial application.

• Figure 1 shows the locations of all area water wells, active or plugged.

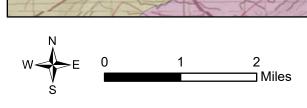
- The nearest well is USGS-9938, which is located .85 miles northwest of the site.
- There are no known domestic water wells located within 1,000 feet of the proposed pits.
- No springs were identified within the mapping area (see Figure 7)

Distance to Wetlands

Figure 9 REV demonstrates the location is within 300 feet of wetlands.

- The nearest designated wetland is a "riverine" wetland of the New Mexico wetlands database. This wetland area is associated with the Pecos River.
- The USA wetland database map is presented as Figure 9 (2021) following Figure 9 REV. As documented in the Appendix Site Photos, the dry swale that is mapped by the USGS as an intermittent stream exhibits no qualities of a wetland.

Figures

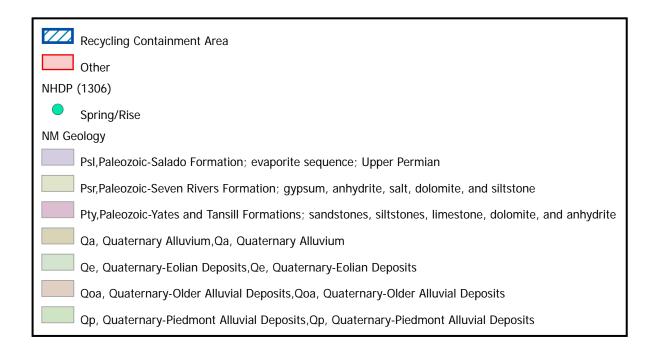


R.T. Hicks Consultants, Ltd 901 Rio Grande Blvd NW Suite F-142 Albuquerque, NM 87104 Ph: 505.266.5004 Regional Geology over 1978 Topographic Map

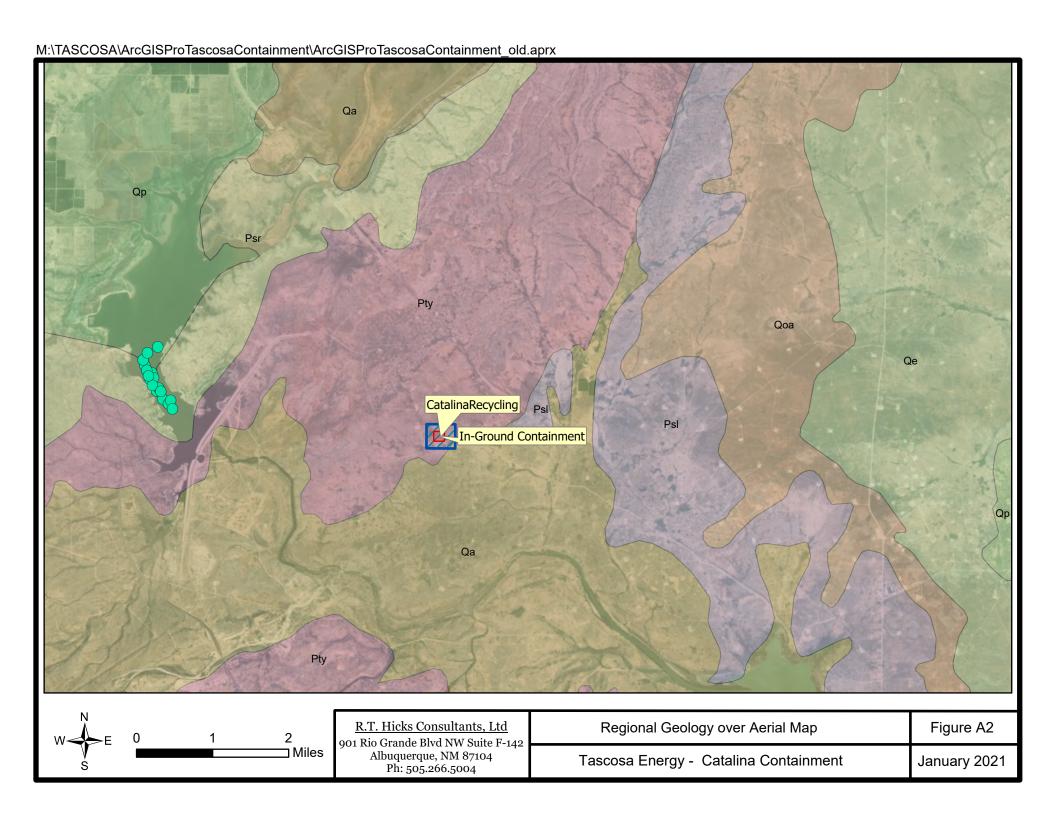
Tascosa Energy - Catalina Containment

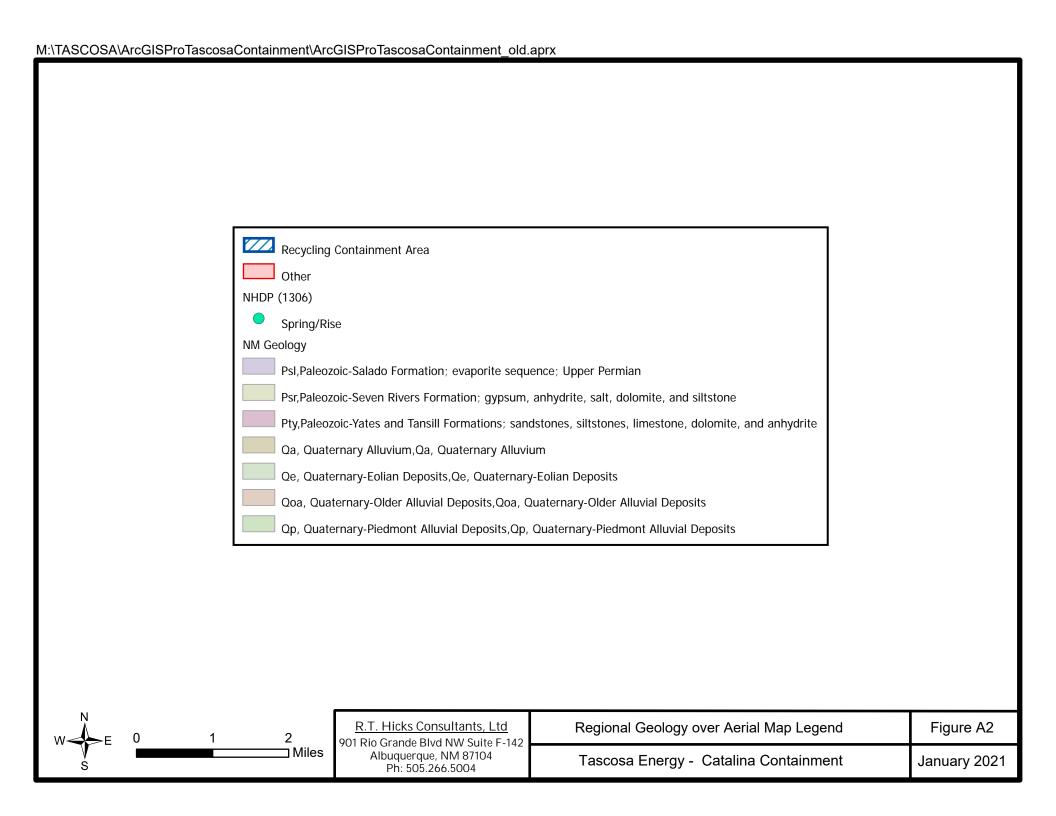
Figure A1

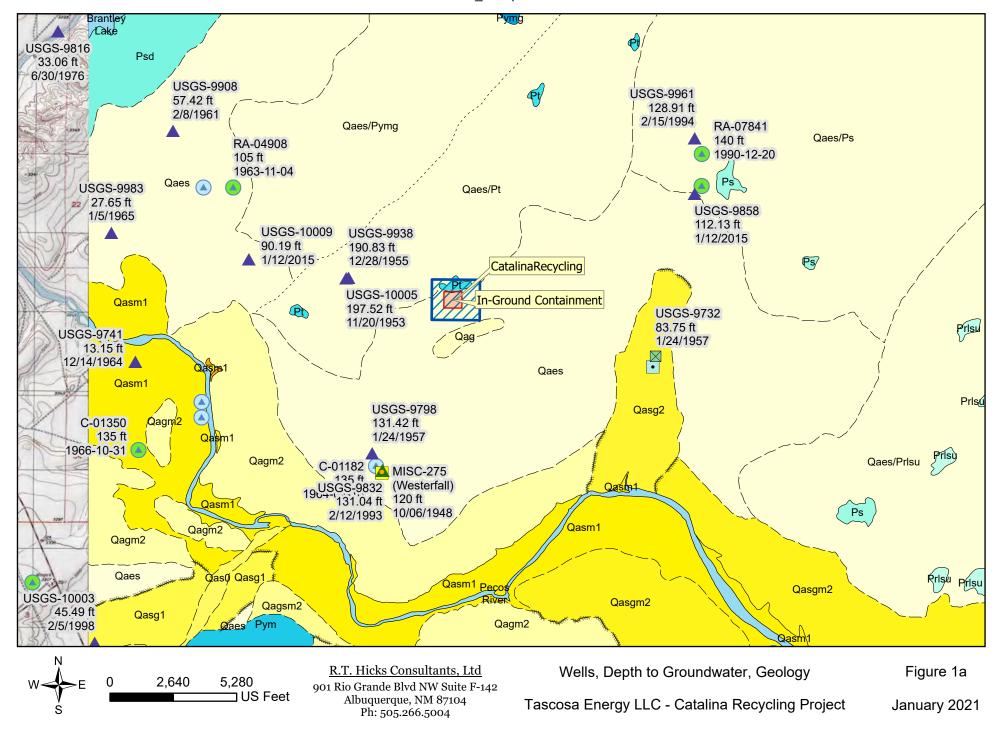
January 2021

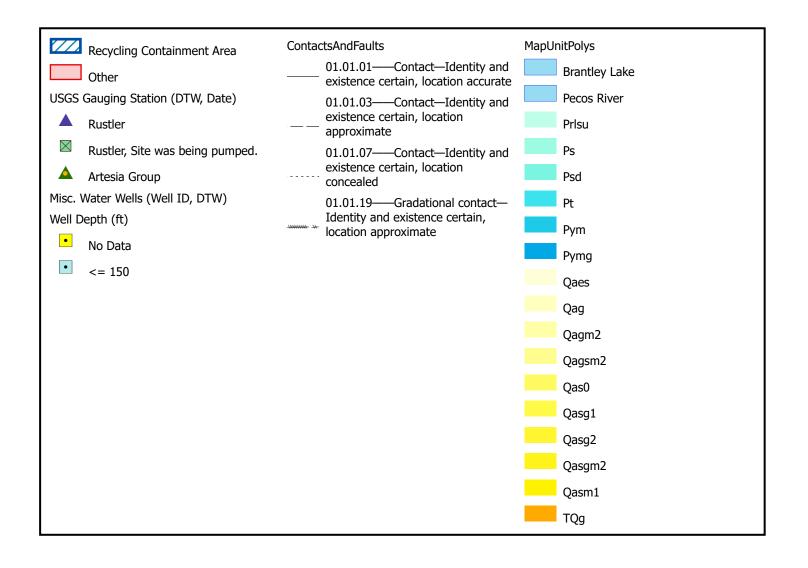




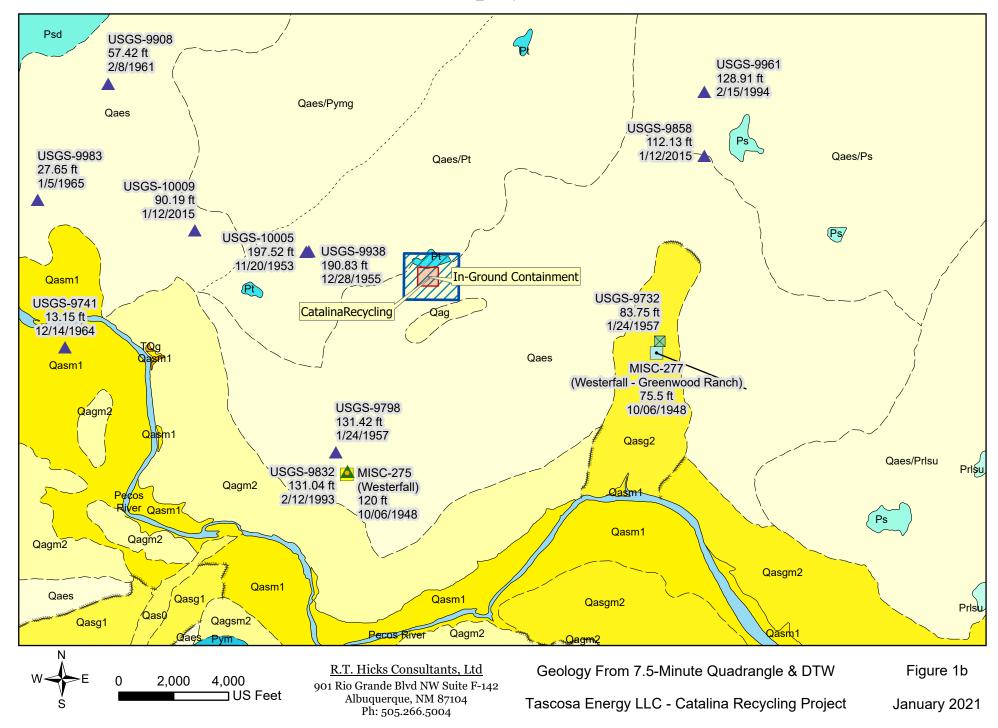


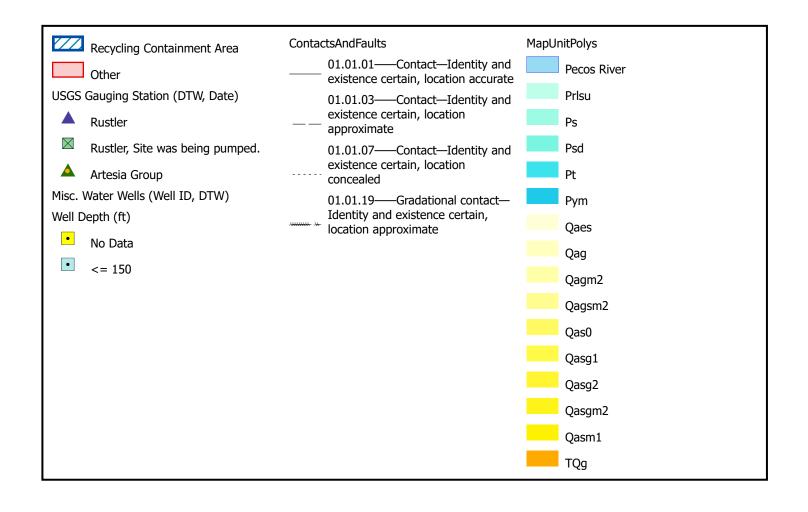




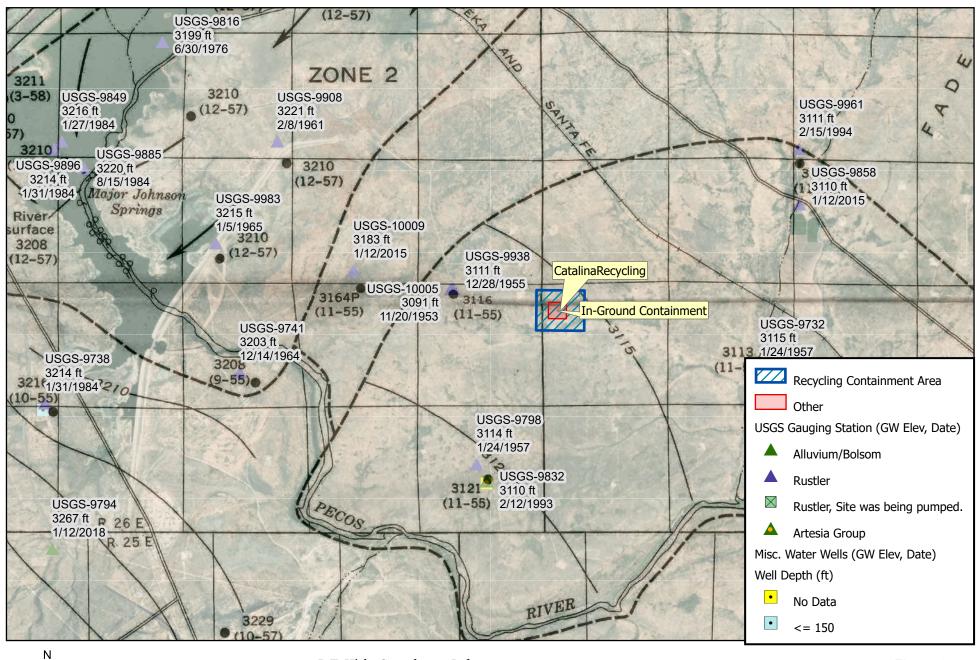












W E 0 2,640 5,280 US Feet

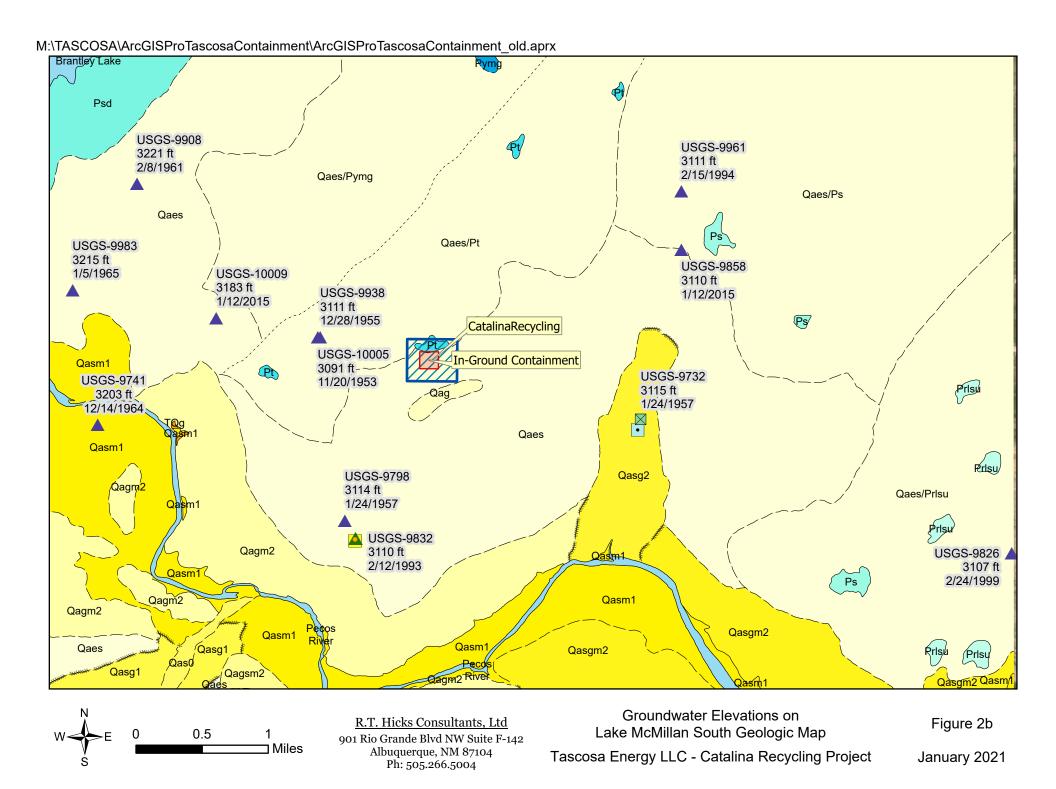
R.T. Hicks Consultants, Ltd 901 Rio Grande Blvd NW Suite F-142 Albuquerque, NM 87104 Ph: 505.266.5004

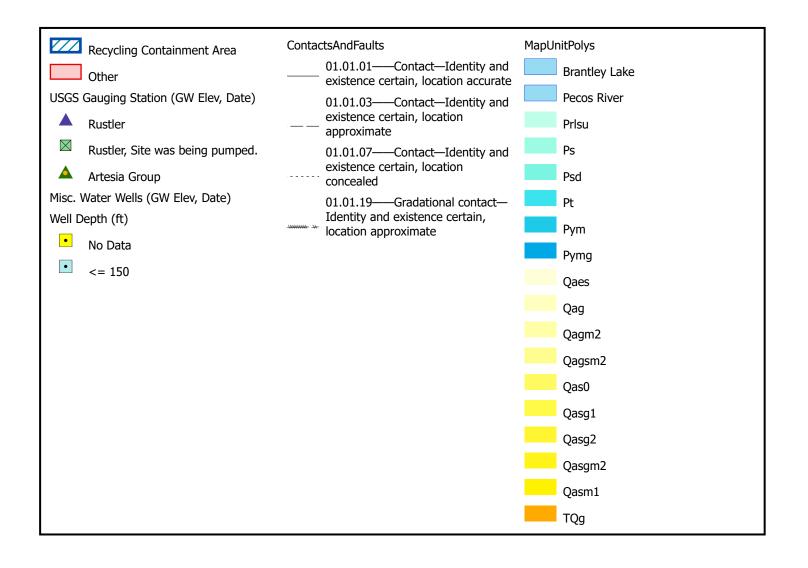
Groundwater Elevation from Plate 4 USGS WSP 1828

Figure 2a

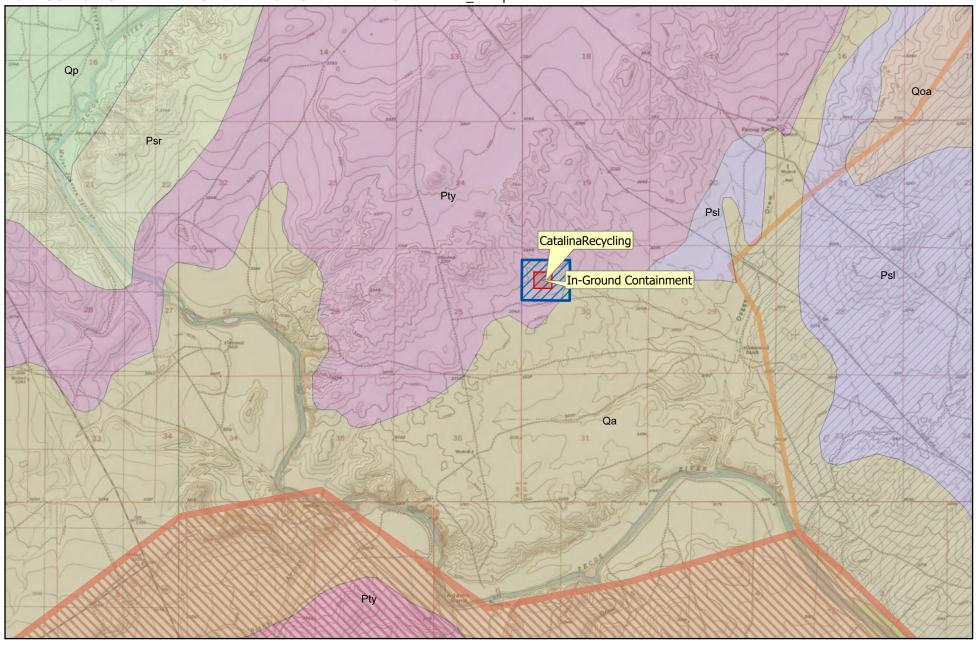
Tascosa Energy LLC - Catalina Recycling Project

January 2021











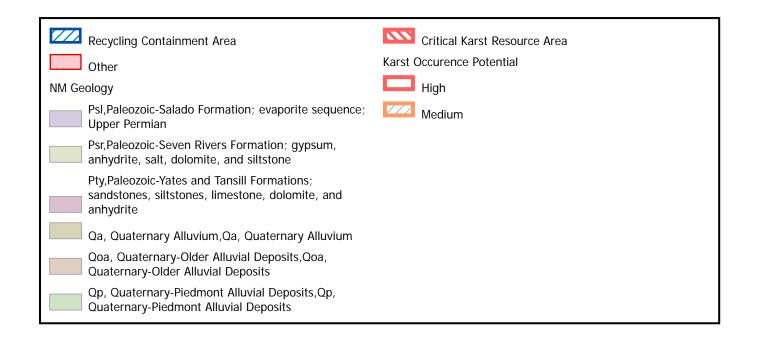
R.T. Hicks Consultants, Ltd 901 Rio Grande Blvd NW Suite F-142 Albuquerque, NM 87104 Ph: 505.266.5004

BLM Karst Potential Map

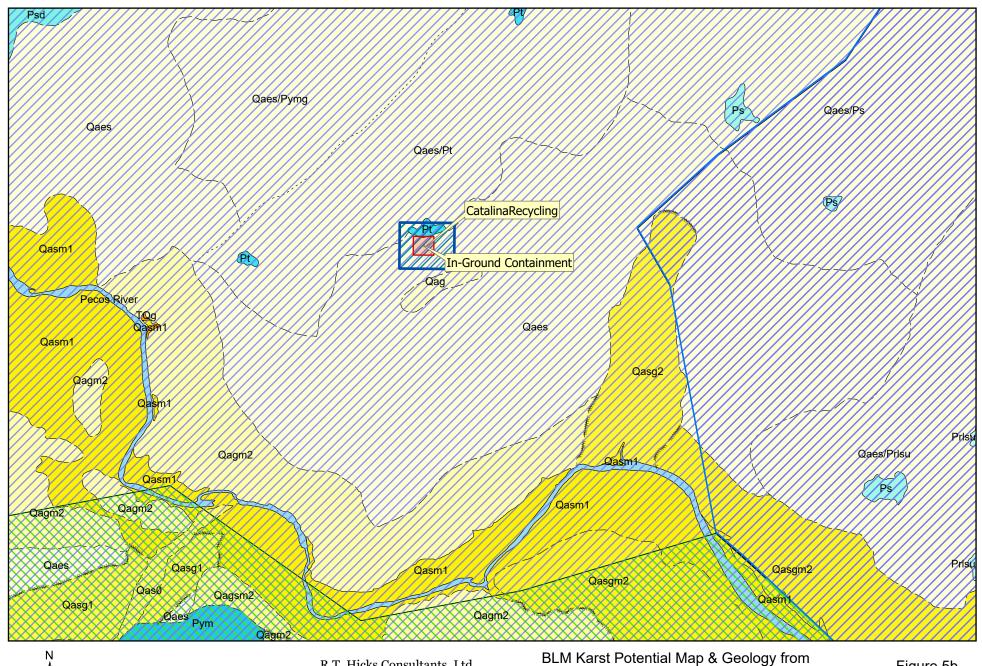
January 2021

Figure 5a

Tascosa Energy LLC - Catalina Recycling Project







W E 0 2,000 4,000 US Feet

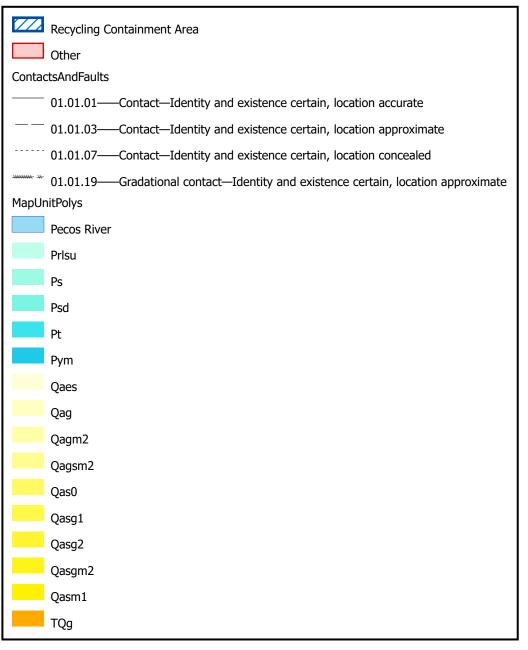
R.T. Hicks Consultants, Ltd 901 Rio Grande Blvd NW Suite F-142 Albuquerque, NM 87104 Ph: 505.266.5004

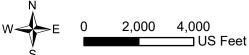
BLM Karst Potential Map & Geology from Lake McMillan South Quadrangle

Tascosa Energy LLC - Catalina Recycling Project

Figure 5b

Dec 2020



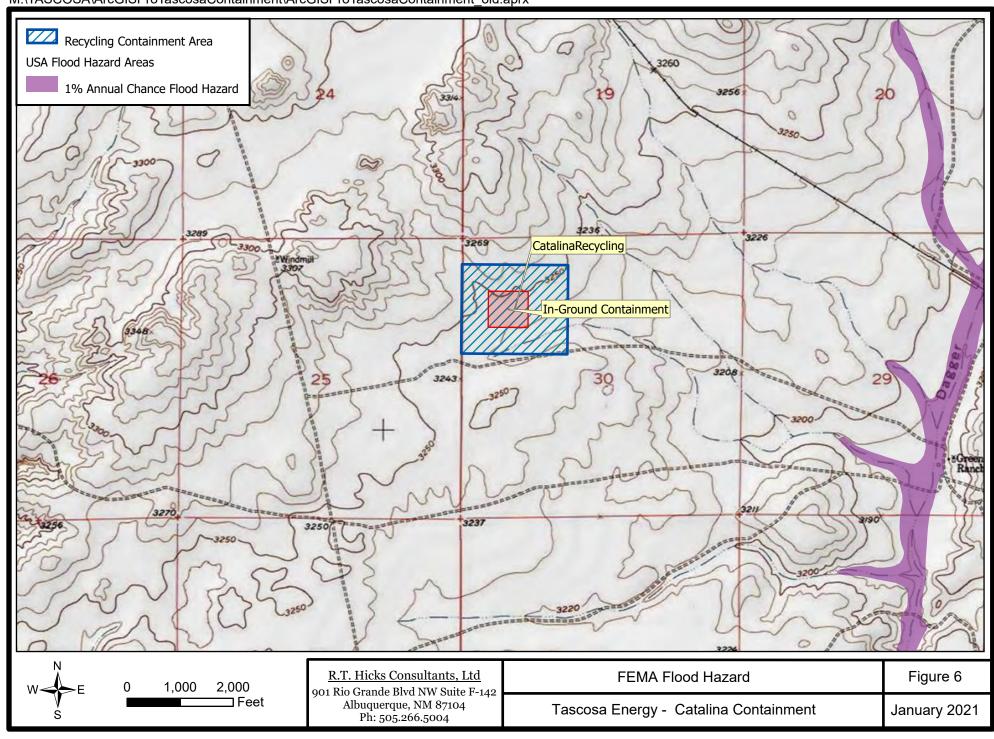


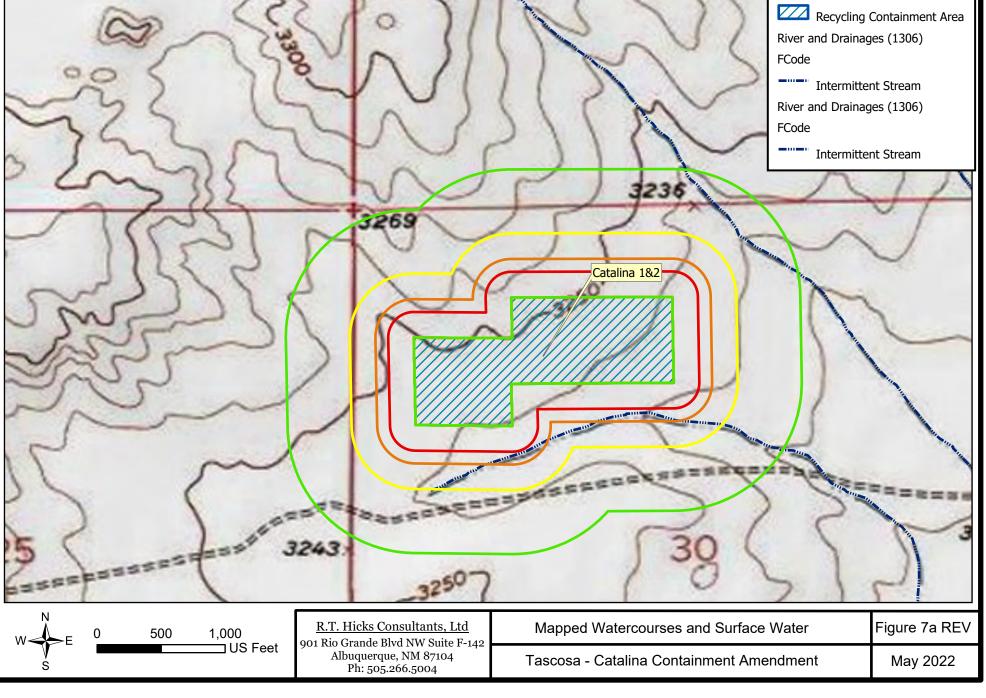
R.T. Hicks Consultants, Ltd 901 Rio Grande Blvd NW Suite F-142 Albuquerque, NM 87104 Ph: 505.266.5004 BLM Karst Potential Map & Geology from Lake McMillan South Quadrangle Legend

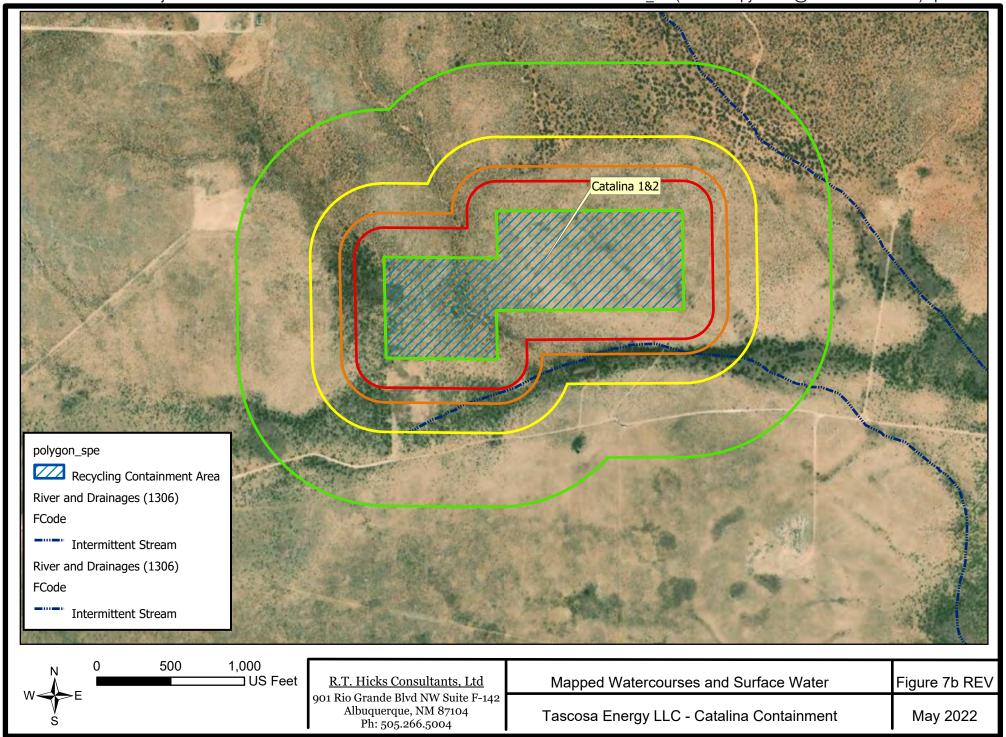
Tascosa Energy LLC - Catalina Recycling Project

Figure 5b

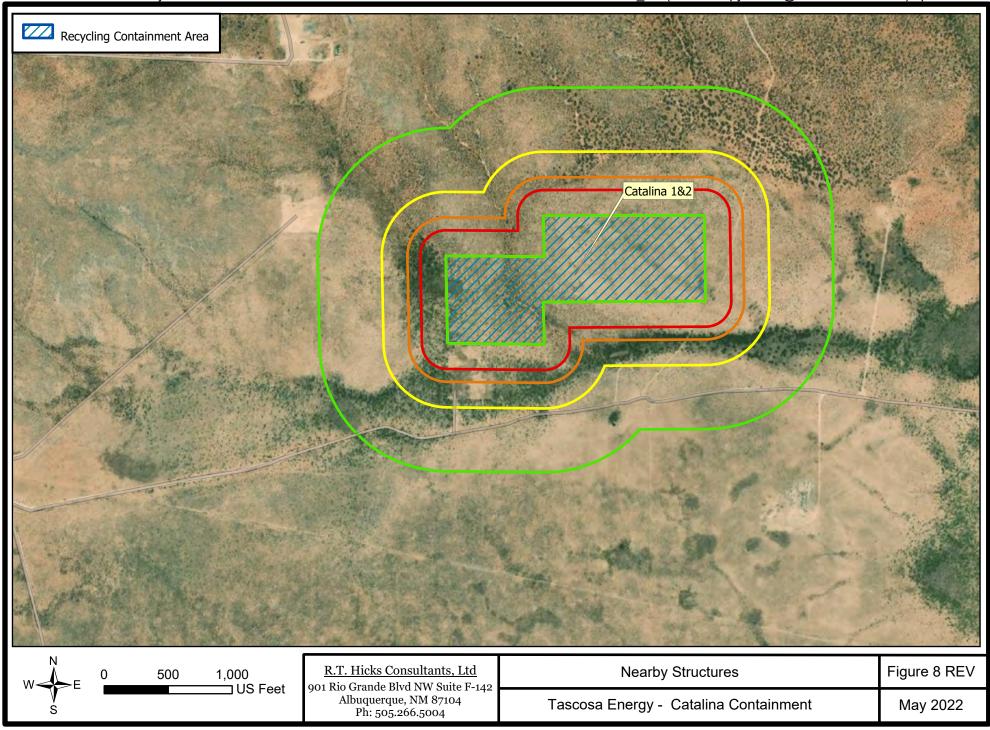
January 2021



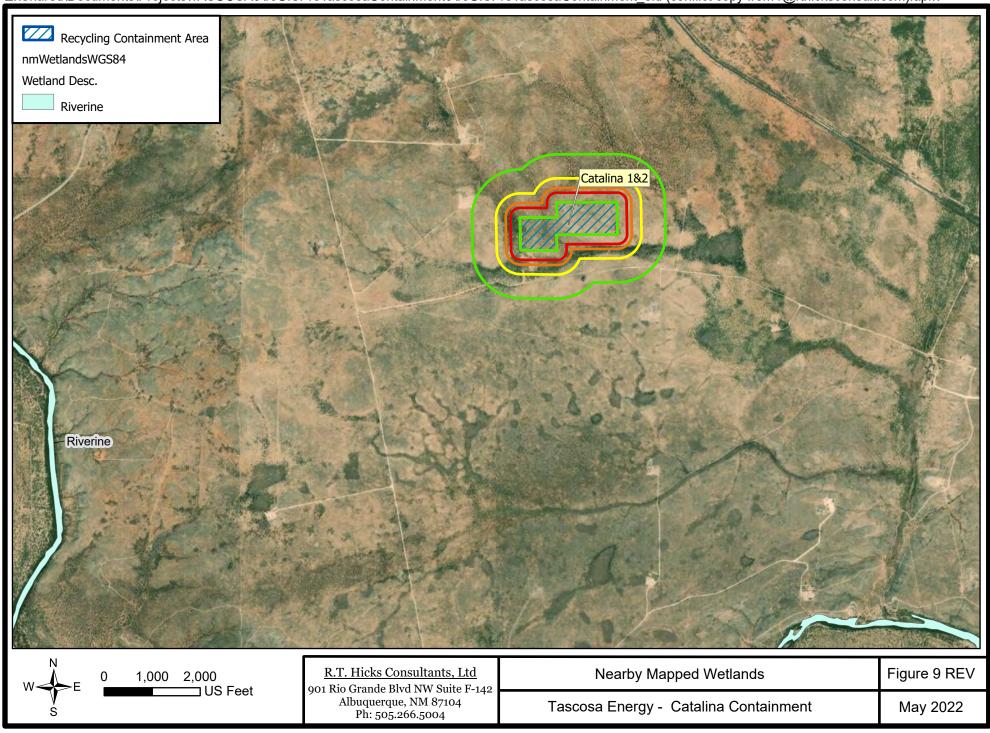


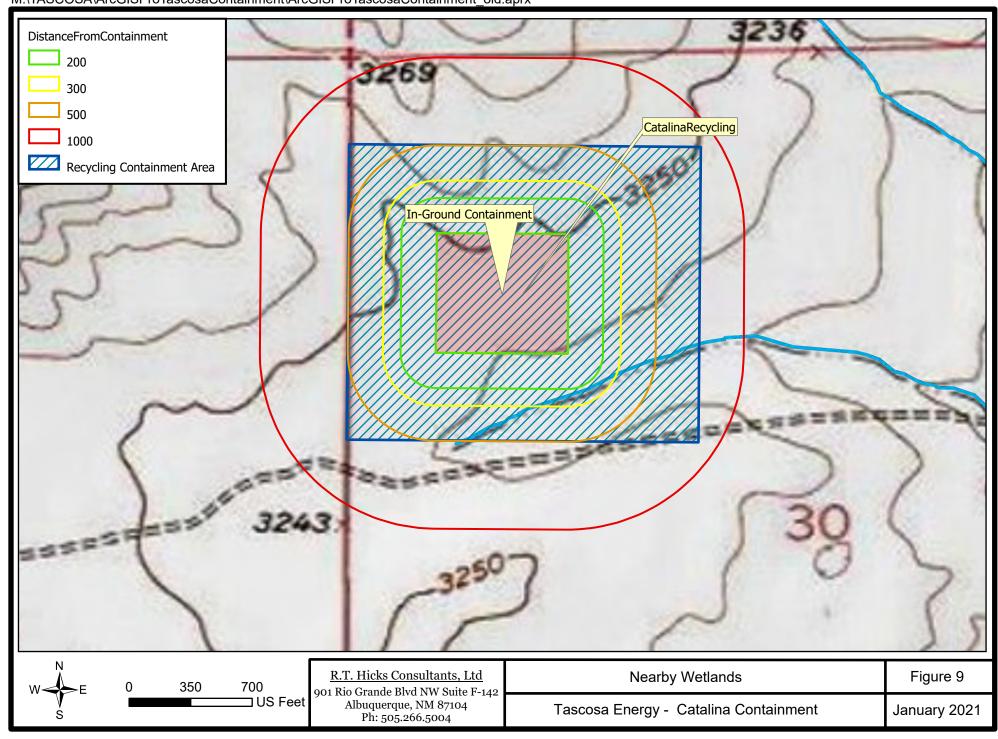


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R. T. HICKS CONSULTANTS, LTD.

901 Rio Grande Blvd NW ▲ Suite F-142 ▲ Albuguergue, NM 87104 ▲ 505.266.5004 ▲ Fax: 505.266-0745

Memorandum

From: Kristin Pope

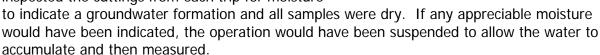
Date: December 30, 2020

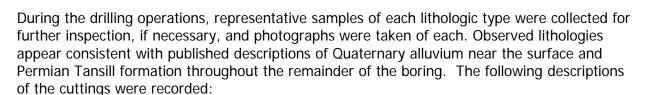
RE: Tascosa Energy - Catalina 30 EH St. #001H, Conductor Hole Evaluation

The subject well site has a surface elevation of 3,244 feet and is located approximately 3 miles east from Brantley Lake. East of the Pecos River, groundwater is present in Permian units, such as the Seven Rivers, Yates, and Tansill formations.

On December 17, 2020 I witnessed the drilling of the conductor hole at the Catalina 30 EH St. #001H, located approximately 10 miles northwest of Carlsbad, New Mexico. Byrd Oilfield Services of Midland, Texas performed the work using a trackmounted auger drilling rig as shown in the adjacent photograph of the auger spinning the cuttings after the final trip out of the hole. A cellar 10-feet deep was previously installed and when I arrived and drilling of the conductor hole began at 11:40 a.m. MST. Beginning at 10 feet below the well pad surface, cuttings were continuously monitored for moisture and lithology with each trip out of the hole. No water or drilling fluids were used to drill this conductor hole.

Over the next 2.75 hours the boring was advanced to a total depth of 120 feet with no issue. I inspected the cuttings from each trip for moisture





10-18 feet	Alluvium: brown, fine sand; caliche
18-63 feet	Tan, loose siltstone with 10-30% interbedded green-gray dolomite. Dolomite
	beds are massive (1 mm-5 cm vesicles observed at 40 ft, most filled with siltstone)
63-68 feet	Red, massive clay; minor tan silt, loose
68-74 feet	Red, massive clay; clast and veins of white and clear gypsum/selenite



74-94 feet Massive purple-red clay interbedded with white and pink gypsum; <5% green

"sugar" dolomite clasts

94-110 feet Loose, medium red silt interbedded; 30% green/gray/yellow vesicular (1-2 mm)

dolomite

110-113 feet Red-brown silt with thin layers of red-brown siltstone and gypsum (1-2 mm

thick)

113-120 feet Dark red silt interbedded with 40% dolomite, green-gray, massive





110-ft sample

50-ft sample



115-ft sample

Based on these observations, I am certain that no groundwater is present below the surface of this well site to 120 feet below ground surface (3,124 feet above sea level).







Figure SP-1 View west from southwest corner of staked containment showing nature of vegetation and local topography.



Figure SP-2 View east from southwest corner stake shown above.



Figure SP-3 View east from center of mapped watercourse about 220 feet due south of proposed Catalina containment area.



Figure SP-4 View west from same area as SP-3 showing nature of center of channel mapped as a watercourse. Equipment is parked on former production pad located south of the proposed containment area.



Figure SP-5 View north (uphill) of Cattle trail within small swale that, on Google Earth images, could be mistaken as a watercourse.



SP-6 View north from mapped outcrop of Qagp2 sand and gravel. Rig in background is drilling the Catalina 30 EH State 1H oil well, which is the location of the conductor pipe boring.



Figure SP-7 Close up showing nature of alluvial deposit with sub-rounded dolomite cobbles, within a matrix of smaller rounded clasts and some angular clasts.



Figure 22SP-1 – View north from southeast corner of Catalina Recycling Containment #1. 32 32 49.34, -104 19 30.21



Figure 22SP-2 View south from northeast corner of Catalina Containment #1



22SP-3 View west showing nature of slope and vegetation east of Catalina Containment #1, which is defined in this image as the area between the red arrows. The USGS-mapped intermittent stream is south (left) in this image.



22SP-4 View south toward the USGS mapped intermittent stream from same location as SP3. 32 32 51.72, -104 19 19.03



22SP-5 – View upstream near the Catalina Containment #1 from the center of the USGS-mapped intermittent stream. This image is typical of the drainage that show no evidence of a bed or bank. 32 32 46.96, -104 19 27.38



22SP6- View west showing nature of slope and vegetation about 1400 feet east of the Catalina Containment #1, which is defined by the red arrows. Location is 32 32 56.04, -104 19 13.04



22SP-7 View to northwest (uphill) showing one of many similar small channels that compose the alluvial fan in this area. This channel is unusual because it trends NW to SE and may be an old, abandoned channel that is now more of a cattle track. None of these small channels exist south of the break in slope that is obvious in the Google Earth image. The location of this image is 32 33 4.30, -104 19 21.01



22SP-8 View uphill to the northwest showing nature of channel in the active alluvial fan. Scrub brush about 4-6 feet tall are common within the alluvial fan. 32 33 4.93, -104 19 25.84



22SP-9 – View to south-southwest showing the Catalina Containment #1 on the right of the image (red arrow) and the slope and nature of vegetation from location 32 33 4.58, -104 19 27.05. Image 22SP-8 is about 100 feet over the left shoulder of the photographer, within the active alluvial fan. Note the scrub bush vegetation continues where the slope flattens.



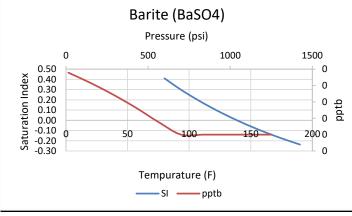
22SP-10 View south-southeast from the lowermost portion of the bedrock hill that exists north Containment #1 (in right of image). The scrub brush vegetation shown in 22SP-9 is on the upper left of the image. 32 33 5.06, -104 19 30.57

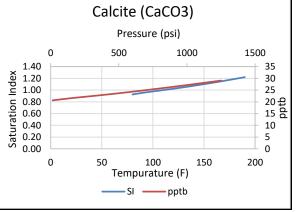
5400 North Big Spring Street Suite A Midland, TX 79705

Complete Water Analysis

Company	TASCOSA ENERGY PARTNERS	Account Manager	TRAVIS TEMPLETON
Lease	CATALINA 30 EH STATE	Sample Date	9/27/2022
Well	1H	Analysis Date	9/29/2022
Sample Point	WELLHEAD	Sample ID	AT12354
Batch Number	2022-09-28-005	Report Date	9/29/2022

	nditions	Sample Co		Analytical Lab Data					
Result		Analyte			Anions	OES	ions by ICP	Ca	
6.85	рН	-		ppm	Analyte	ppm	/te	Anal	
3.4	iss. H2S (ppm)			76,700	Chloride (CI)	5,458	alcium (Ca)	С	
80	iss. CO2 (ppm)	D		656	Sulfate (SO4)	945.35	esium (Mg)	Magn	
183.0	te (ppm HCO3)	Bicarbona			-	1.04	arium (Ba)	E	
0.0	ate (ppm CO3)	Carbon		vity	Specific Grav	515.20	ntium (Sr)	Str	
0.0	Diss. O2 (ppm)			g/mL	1.090	1,386.38	assium (K)	Po	
190.0	emperature (F)	Initial To				1.15	Iron (Fe)		
80.0	emperature (F)	Final To				0.95	nese (Mn)	Mang	
1,250.0	l Pressure (psi)	Initia				39.99	Boron (B)		
15.0	l Pressure (psi)	Fina				6.58	Zinc (Zn)		
						0.32	minum (Al)	Alu	
				0.00	Phosphate	0.00 Cal	phorus (P)	Pho	
						16.10	Silicon (Si)		
7.67	Calc. Resistivity (ohms/cm)				36.71	ithium (Li)			
130,400	ctivity (uS/cm)					0.00	Lead (Pb)		
17,520	ess (as CaCO3)	ılc. Total Hardn	Ca			0.25	mium (Cr)	Chr	
126,565	Calc. TDS (ppm)	C				40,656	(Na) (calc.)	Sodium	
	CaCO3)	Calcite (C				Barite (BaSO4)			
pptb	SI	PSI	Temp. (F)	tb	ppt	SI	PSI	Temp. (F)	
20.6	0.93	15	80	4	0.4	0.41	15	80	
21.6	0.96	152	92	3	0.3	0.31	152	92	
22.4	0.99	289	104	2	0.3	0.22	289	104	
23.2	1.02	427	117	2	0.3	0.13	427	117	
24.1	1.05	564	129	1	0.:	0.06	564	129	
25.0	1.08	701	141	0	0.0		701	141	
26.0	1.11	838	153	0	0.0		838	153	
27.0	1.15	976	166	0	0.0	-0.13	976	166	
28.0	1.18	1,113	178	0	0.0	-0.19	1113	178	
29.0	1.22	1,250	190	0	0.0	-0.24	1250	190	

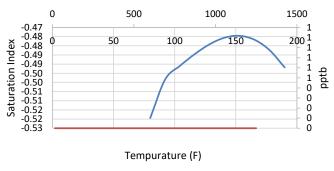




Gypsum (CaSO4 - 2H20)			Anhydrite (CaSO4)				
Temp. (F)	PSI	SI	pptb	Temp. (F)	PSI	SI	pptb
80	15	-0.52	0.0	80	15	-0.73	0.0
92	152	-0.50	0.0	92	152	-0.66	0.0
104	289	-0.49	0.0	104	289	-0.60	0.0
117	427	-0.48	0.0	117	427	-0.54	0.0
129	564	-0.48	0.0	129	564	-0.48	0.0
141	701	-0.48	0.0	141	701	-0.42	0.0
153	838	-0.47	0.0	153	838	-0.36	0.0
166	976	-0.48	0.0	166	976	-0.31	0.0
178	1113	-0.48	0.0	178	1113	-0.25	0.0
190	1250	-0.49	0.0	190	1250	-0.19	0.0

Gypsum (CaSO4 - 2H2O)

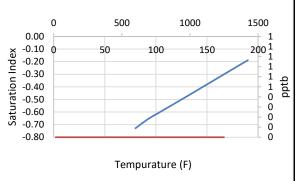
Pressure (psi)



—SI ——pptb

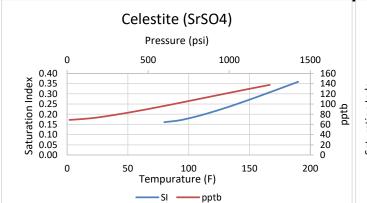
Anhydrite (CaSO4)

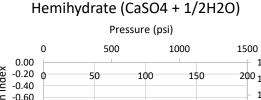


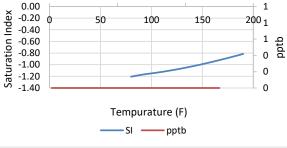


——SI	 p	ptb

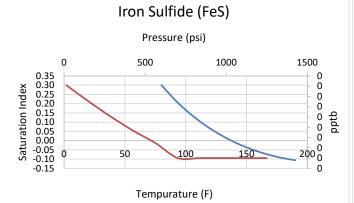
Celestite (SrSO4)			Hemihydrate (CaSO4 + 1/2H20)				
Temp. (F)	PSI	SI	pptb	Temp. (F)	PSI	SI	pptb
80	15	0.16	68.8	80	15	-1.21	0.0
92	152	0.17	72.2	92	152	-1.17	0.0
104	289	0.19	78.4	104	289	-1.14	0.0
117	427	0.21	85.9	117	427	-1.11	0.0
129	564	0.23	94.1	129	564	-1.07	0.0
141	701	0.25	102.7	141	701	-1.02	0.0
153	838	0.28	111.5	153	838	-0.98	0.0
166	976	0.31	120.4	166	976	-0.93	0.0
178	1113	0.33	129.1	178	1113	-0.87	0.0
190	1250	0.36	137.6	190	1250	-0.82	0.0



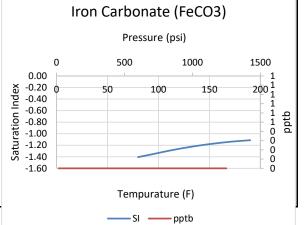




Iron Sulfide (FeS)			Iron Carbonate (FeCO3)				
Temp. (F)	PSI	SI	pptb	Temp. (F)	PSI	SI	pptb
80	15	0.30	0.1	80	15	-1.40	0.0
92	152	0.30	0.1	92	152	-1.36	0.0
104	289	0.14	0.1	104	289	-1.32	0.0
117	427	0.08	0.1	117	427	-1.27	0.0
129	564	0.03	0.0	129	564	-1.24	0.0
141	701	-0.01	0.0	141	701	-1.20	0.0
153	838	-0.04	0.0	153	838	-1.17	0.0
166	976	-0.07	0.0	166	976	-1.15	0.0
178	1113	-0.09	0.0	178	1113	-1.13	0.0
190	1250	-0.11	0.0	190	1250	-1.11	0.0



_____ SI _____ pptb

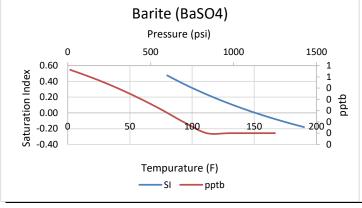


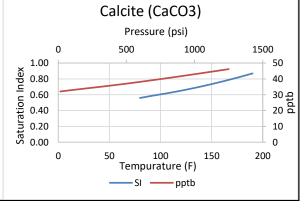
5400 North Big Spring Street Suite A Midland, TX 79705

Complete Water Analysis

Company	TASCOSA ENERGY PARTNERS	Account Manager	MASON LONG
Lease	CATALINA 25 30 STATE COM	Sample Date	10/7/2022
Well	2H	Analysis Date	10/11/2022
Sample Point	WELLHEAD	Sample ID	AT12880
Batch Number	2022-10-07-005	Report Date	10/11/2022

		Analytical Lal	Data				Sample Co	nditions	
Ca	tions by ICF	P-OES		Anions			Analyte		Result
Ana	lyte	ppm	1	Analyte	ppm			рН	6.09
(Calcium (Ca)	6,709		Chloride (Cl)	90,700		[Diss. H2S (ppm)	20.0
Magr	esium (Mg)	1,201.93		Sulfate (SO4)	613		Ε	Diss. CO2 (ppm)	310
	Barium (Ba)	1.42			•		Bicarbona	te (ppm HCO3)	305.0
St	rontium (Sr)	689.60		Specific Gra	vity		Carbor	nate (ppm CO3)	0.0
Po	otassium (K)	1,725.52		1.105	g/mL			Diss. O2 (ppm)	0.0
	Iron (Fe)	8.47			•		Initial T	emperature (F)	190.0
Mang	ganese (Mn)	1.33					Final T	emperature (F)	80.0
	Boron (B)	42.52					Initia	ıl Pressure (psi)	1,250.0
	Zinc (Zn)	8.72					Fina	ıl Pressure (psi)	15.0
Alı	ıminum (Al)	0.78							
Pho	sphorus (P)	5.49	Calc.	Phosphate	16.82				
	Silicon (Si)	11.80							
	Lithium (Li)	46.23				Calc. Resistivity (ohms/cm)		7.09	
	Lead (Pb)	0.24				Conductivity (uS/cm)		uctivity (uS/cm)	141,100
Chi	romium (Cr)	0.20				C	alc. Total Hardr	ness (as CaCO3)	21,701
Sodium	(Na) (calc.)	47,511					(Calc. TDS (ppm)	149,528
		Barite (Bas	04)				Calcite (CaCO3)	
Temp. (F)	PSI	SI		рр	tb	Temp. (F)	PSI	SI	pptb
80	15	0.48		0.	.6	80	15	0.56	32.1
92	152	0.38		0.	.5	92	152	0.59	33.5
104	289	0.29		0.	.4	104	289	0.61	34.8
117	427	0.20		0.	.3	117	427	0.64	36.2
129	564	0.12		0.	.2	129	564	0.67	37.7
141	701	0.05		0.	.1	141	701	0.71	39.3
153	838	-0.01		0.	.0	153	838	0.74	40.9
166	976	-0.07		0.	.0	166	976	0.78	42.7
178	1113	-0.13		0.	.0	178	1,113	0.83	44.4
190	1250	-0.18		0.	.0	190	1,250	0.87	46.2

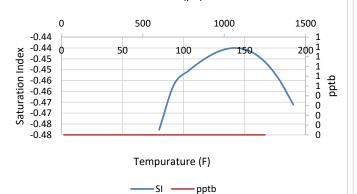




Gypsum (CaSO4 - 2H20)			Anhydrite (CaSO4)				
Temp. (F)	PSI	SI	pptb	Temp. (F)	PSI	SI	pptb
80	15	-0.48	0.0	80	15	-0.67	0.0
92	152	-0.46	0.0	92	152	-0.60	0.0
104	289	-0.45	0.0	104	289	-0.54	0.0
117	427	-0.45	0.0	117	427	-0.49	0.0
129	564	-0.44	0.0	129	564	-0.43	0.0
141	701	-0.44	0.0	141	701	-0.37	0.0
153	838	-0.44	0.0	153	838	-0.32	0.0
166	976	-0.45	0.0	166	976	-0.26	0.0
178	1113	-0.45	0.0	178	1113	-0.20	0.0
190	1250	-0.47	0.0	190	1250	-0.15	0.0

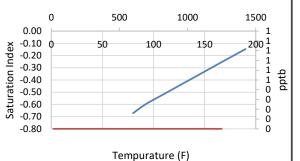
Gypsum (CaSO4 - 2H2O)

Pressure (psi)



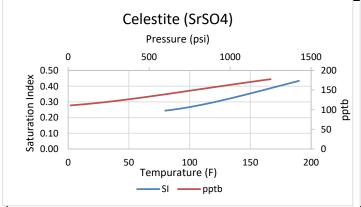
Anhydrite (CaSO4)

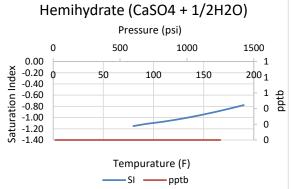




—SI — pptb

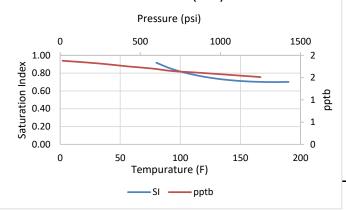
Celestite (SrSO4)			Hemihydrate (CaSO4 + 1/2H20))	
Temp. (F)	PSI	SI	pptb	Temp. (F)	PSI	SI	pptb
00	4.5	0.24	111 1		1 1 5		0.0
80	15	0.24	111.1	80	15	-1.15	0.0
92	152	0.26	116.0	92	152	-1.11	0.0
104	289	0.27	122.3	104	289	-1.09	0.0
117	427	0.29	129.5	117	427	-1.05	0.0
129	564	0.31	137.3	129	564	-1.02	0.0
141	701	0.34	145.4	141	701	-0.98	0.0
153	838	0.36	153.7	153	838	-0.93	0.0
166	976	0.38	162.0	166	976	-0.88	0.0
178	1113	0.41	170.1	178	1113	-0.83	0.0
190	1250	0.43	177.9	190	1250	-0.78	0.0



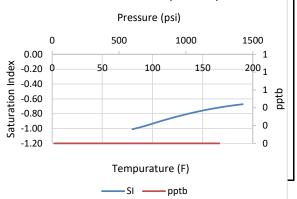


Iron Sulfide (FeS)			Iron Carbonate (FeCO3)				
Temp. (F)	PSI	SI	pptb	Temp. (F)	PSI	SI	pptb
						ī	
80	15	0.92	1.9	80	15	-1.01	0.0
92	152	0.85	1.8	92	152	-0.97	0.0
104	289	0.80	1.8	104	289	-0.92	0.0
117	427	0.77	1.7	117	427	-0.87	0.0
129	564	0.74	1.7	129	564	-0.82	0.0
141	701	0.72	1.6	141	701	-0.78	0.0
153	838	0.71	1.6	153	838	-0.75	0.0
166	976	0.70	1.6	166	976	-0.72	0.0
178	1113	0.70	1.5	178	1113	-0.69	0.0
190	1250	0.70	1.5	190	1250	-0.67	0.0

Iron Sulfide (FeS)



Iron Carbonate (FeCO3)



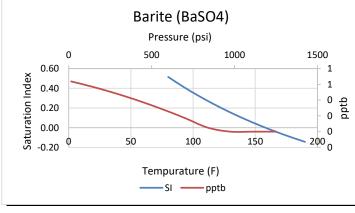
Notes

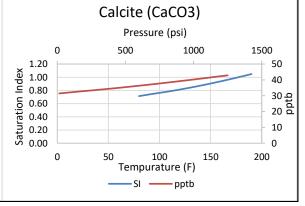
5400 North Big Spring Street Suite A Midland, TX 79705

Complete Water Analysis

Company	TASCOSA ENERGY PARTNERS	Account Manager	MASON LONG
Lease	CATALINA 25 30 STATE COM	Sample Date	10/7/2022
Well	3H	Analysis Date	10/11/2022
Sample Point	WELLHEAD	Sample ID	AT12881
Batch Number	2022-10-07-005	Report Date	10/11/2022

	nditions	Sample Co		Analytical Lab Data					
Result		Analyte			Anions	OES	Cations by ICP-OES		
6.28	рН			ppm	\nalyte	ppm	yte	Ana	
14.0	Diss. H2S (ppm)			89,000	Chloride (CI)	7,033	alcium (Ca)	C	
) 280	oiss. CO2 (ppm)			620	Sulfate (SO4)	1,215.49	0 (0,)		
268.0	te (ppm HCO3)	Bicarbona				1.54	arium (Ba)		
0.0	nate (ppm CO3)	Carbor		vity	Specific Gra	718.89	Strontium (Sr) 718.89		
0.0	Diss. O2 (ppm)			g/mL	1.104	1,760.14	Potassium (K) 1,760.14		
190.0	emperature (F)	Initial T				33.41	Iron (Fe)		
80.0	emperature (F)	Final T				1.40	anese (Mn)	Mang	
1,250.0	l Pressure (psi)	Initia				41.03	Boron (B)		
15.0	l Pressure (psi)	Fina				8.79	Zinc (Zn)		
						1.10	minum (Al)	Alu	
				0.00	Phosphate	0.00 Calc	sphorus (P)	Pho	
						11.36	Silicon (Si) 11.36		
,	vity (ohms/cm)	Calc. Resisti				46.72	Lithium (Li) 46.72		
) 152,000	ictivity (uS/cm)	Condu				0.00	Lead (Pb)		
22,566	ess (as CaCO3)	alc. Total Hardn	Ca			0.27	omium (Cr)	Chr	
146,664	Calc. TDS (ppm)	(45,953	Sodium (Na) (calc.) 45,953		
	CaCO3)	Calcite (0				Barite (BaSO4)			
pptb	SI	PSI	Temp. (F)	tb	pp.	SI	PSI	Temp. (F)	
31.5	0.71	15	80	6	0.	0.52	15	80	
32.6	0.74	152	92	6	0.	0.42	152	92	
33.6	0.77	289	104	5	0.	0.32	289	104	
34.8	0.80	427	117	4	0.	0.24	427	117	
36.0	0.84	564	129	3	0.	0.16	564	129	
37.3	0.88	701	141	0.2		0.09	701	141	
38.6	0.92	838	153	1	0.	0.02	838	153	
40.0	0.96	976	166	0	0.0		976	166	
41.4	1.00	1,113	178	0.0		-0.09	1113	178	
42.9	1.05	1,250	190	0	0.	-0.14	1250	190	

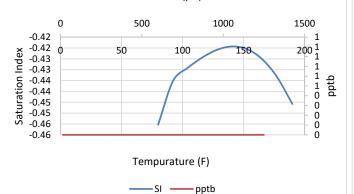




	(Gypsum (CaSO4 - 2H20	0)		Anhydrite	(CaSO4)	
Temp. (F)	PSI	SI	pptb	Temp. (F)	PSI	SI	pptb
80	15	-0.46	0.0	80	15	-0.65	0.0
92	152	-0.44	0.0	92	152	-0.58	0.0
104	289	-0.43	0.0	104	289	-0.52	0.0
117	427	-0.42	0.0	117	427	-0.47	0.0
129	564	-0.42	0.0	129	564	-0.41	0.0
141	701	-0.42	0.0	141	701	-0.35	0.0
153	838	-0.42	0.0	153	838	-0.30	0.0
166	976	-0.43	0.0	166	976	-0.24	0.0
178	1113	-0.43	0.0	178	1113	-0.18	0.0
190	1250	-0.45	0.0	190	1250	-0.13	0.0

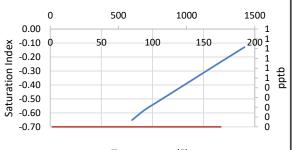
Gypsum (CaSO4 - 2H2O)

Pressure (psi)



Anhydrite (CaSO4)

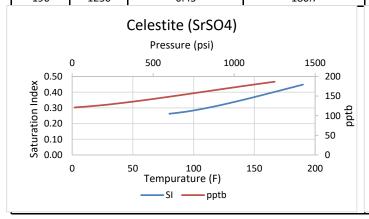


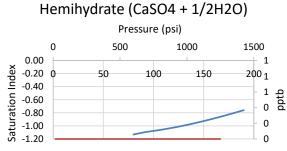


Tempurature (F)

— SI —	g	ptb
J.	М	PLD

		Celestite (SrSO4)		Hei	mihydrate (Ca	SO4 + 1/2H20)
Temp. (F)	PSI	SI	pptb	Temp. (F)	PSI	SI	pptb
22	4.5	0.26	101.1	22	45	1	0.0
80	15	0.26	121.1	80	15	-1.13	0.0
92	152	0.27	125.6	92	152	-1.09	0.0
104	289	0.29	131.6	104	289	-1.07	0.0
117	427	0.31	138.7	117	427	-1.04	0.0
129	564	0.33	146.4	129	564	-1.00	0.0
141	701	0.35	154.5	141	701	-0.96	0.0
153	838	0.38	162.7	153	838	-0.91	0.0
166	976	0.40	170.9	166	976	-0.86	0.0
178	1113	0.42	178.9	178	1113	-0.81	0.0
190	1250	0.45	186.7	190	1250	-0.76	0.0

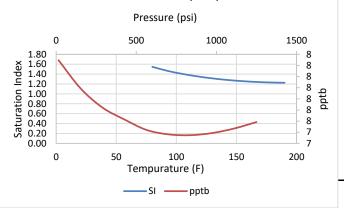




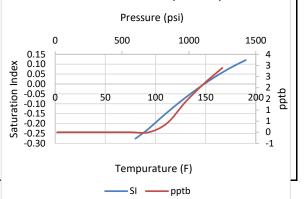
Tempurature (F)
—— SI —— pptb

		Iron Sulfide (FeS)			Iron Carbona	te (FeCO3)	
Temp. (F)	PSI	SI	pptb	Temp. (F)	PSI	SI	pptb
80	15	1.55	7.8	80	15	-0.28	0.0
92	152	1.47	7.6	92	152	-0.23	0.0
104	289	1.41	7.6	104	289	-0.18	0.0
117	427	1.36	7.5	117	427	-0.12	0.0
129	564	1.32	7.5	129	564	-0.07	0.0
141	701	1.28	7.4	141	701	-0.03	0.0
153	838	1.26	7.4	153	838	0.02	0.4
166	976	1.24	7.4	166	976	0.06	1.4
178	1113	1.23	7.5	178	1113	0.09	2.2
190	1250	1.23	7.5	190	1250	0.12	2.9





Iron Carbonate (FeCO3)



Notes



New Mexico Environment Department Ground Water Quality Bureau

Produced Water Pilot Project Notice of Intent to Discharge

For Department Use Only:

Agency Interest Number	
PRD Assigned	

1.	Name and mailing address of person or group perfor	ming research (Responsible Person):					
Gag	ge Herrmann	Work Phone: (432) 288-4622					
901	1 W Missouri Ave	Cell/Home Phone: (432) 288-4622					
Mic	idland TX, 79701	Fax:					
		Email: gherrmann@tascosaep.com					
2.	Name and position of person completing form:						
G	Gage Herrmann – Midstream Manager	Work Phone: (432) 288-4622					
	age Hermani – Musucani Manager	Work Priorie. (1887) 1882 1882					
		Cell/Home Phone: (432) 288-4622					
12		Fax:					
		Email: gherrmann@tascosaep.com					
3.	Research Focus (PWRC Research Category):						
4.	Is the proposed use of the treated produced water to industry? $\underline{^{Inside}}$	be used inside or outside of the oil and gas					
5. 6.	Does the location for testing the technology take place inside or outside of the oil and gas field? Inside Physical location of the research site including size and boundaries of site (include, street address,						
	township, range, section, county, distance from clos Provide as an attachment.						
7.	Topographic and aerial map(s) showing: (please see	attached)					
	land status and adjacent land status	,					
	 100-year flood plain, 						
	 dwellings and occupied establishments, 						
	 watercourses including irrigation ditche 	s, wetlands, lakes, karst and soils					
	 water wells (types) or springs 						
	site security						
	site plan showing locations of relevants	structures					
8.	List any regulatory, governmental and non-governmental agencies, including municipalities or counties that have authority on the testing location. Provide as an attachment.						
9.	Provide a description of your signage plan for the te	sting site. Provide as an attachment.					
10.	Provide a description of your site security plan, inclu	uding training and site restriction methods.					
11.	See attached List of adjacent landowners and confirmation that ac proposed pilot project. Provide as an attachment.	ljacent landowners have been notified of the					
12.	List the source(s) of the produced water including basin of origin. Describe how the produced water will						

be transported to and from the site including origin and disposal locations and onsite storage safety

precautionary methods. Provide as an attachment.



Produced Water Pilot Project Notice of Intent to Discharge

For Department Use Only:

Agency Interest Number	
PRD Assigned	
	11.5-3

- 13. Provide the disposal and decommissioning plan for the expected byproducts, waste products and other potentially contaminated materials. Plan should include disposition of equipment, soils, plants and piping requiring disposal and the expected disposal locations for each. Provide as an attachment.
- 14. Describe the expected contaminants in the untreated produced water and the treated produced water (e.g. contaminants being studied, known contaminants, known additives). Include estimated concentrations if known, and copies of laboratory analyses of untreated and treated produced water. Provide as an attachment.
- 15. Describe all components of the produced water processing, treatment, storage, secondary containment, and produced water system (e.g., pre-treatment units, above ground storage tanks, etc.). Include sizes, site layout map, closed loop processing plans, and specifications. Provide as an attachment.
- 16. Describe your disposal plan for all produced water, treated produced water, permeate or brine concentrate into a SWD. Provide as an attachment.

17.	Describe your final closure plan after completi	on of the pilot project. Provide as an attachment.				
18.		Source of information				
19.	. Current Total Dissolved Solids Concentration in Groundwater					
Sig Prir	nature: <u>Jacque Herrmann</u> nted name: <u>Gage Herrmann</u>	Date: 4/20/2023 Title: Midstroum Manager				
I, _	tification by Responsible Person The Dumber of the American Street and accurate service and experience.	, hereby certify that the information and data as possible, to the best of my knowledge and professional				
Sig		pon my oath or affirmation, before a notary of the State of				

Please return this form to:

NMED Ground Water Quality Bureau
P.O. Box 5469

Santa Fe, New Mexico 87502-5469

Telephone: 505-827-2900 Fax: 505-827-2965