APPENDIX E
HYDROLOGY, GEOMETRY, AND METEROLOGICAL INPUT DATA FOR SSTEMP

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TABLE OF CONTENTS

TABLE OF CONTENTS ..... **I**

LIST OF TABLES ..... **I**

LIST OF FIGURES ..... **II**

LIST OF ACRONYMS ..... **III**

LIST OF ACRONYMS ..... **III**

E 1.0 INTRODUCTION 1
E 2.0 HYDROLOGY 1
E2.1 Segment Inflow *1*
E2.2 Inflow Temperature *4*
E2.3 Segment Outflow *4*
E2.4 Accretion Temperature *5*
E 3.0 GEOMETRY 6
E3.1 Latitude *6*
E3.2 Dam at Head of Segment *6*
E3.3 Segment Length *6*
E3.4 Upstream Elevation *7*
E3.5 Downstream Elevation *7*
E3.6 Width's A and Width's B Term *7*
E3.7 Manning's n or Travel Time *12*
E 4.0 METEOROLOGICAL PARAMETERS 13
E4.1 Air Temperature *13*
E4.2 Maximum Air Temperature *13*
E4.3 Relative Humidity *14*
E4.4 Wind Speed *15*
E4.5 Ground Temperature *15*
E4.6 Thermal Gradient *15*
E4.7 Possible Sun *16*
E4.8 Dust Coefficient *16*
E4.9 Ground Reflectivity *16*
E4.10 Solar Radiation *16*
E 5.0 SHADE 17
E 6.0 REFERENCES 18

LIST OF TABLES

Table E.1 Assessment Units and Modeled Dates 1
Table E.2 Drainage Areas for Estimating Flow by Drainage Area Ratios 2
Table E.3 Parameters for Estimating Flow using USGS Regression Model 3
Table E.4 Inflow 3
Table E.5 Mean Daily Water Temperature 4
Table E.6 Segment Outflow 4

Table E.7 Mean Annual Air Temperature as an Estimate for Accretion Temperature 5
Table E.8 Assessment Unit Latitude..... 6
Table E.9 Presence of Dam at Head of Segment..... 6
Table E.10 Segment Length..... 6
Table E.11 Upstream Elevations..... 7
Table E.12 Downstream Elevations..... 7
Table E.13 Width's A and Width's B Terms..... 8
Table E.14 Manning's n Values..... 12
Table E.15 Mean Daily Air Temperature 13
Table E.16 Mean Daily Relative Humidity 14
Table E.17 Mean Daily Wind Speed 15
Table E.18 Mean Annual Air Temperature as an Estimate for Ground Temperature..... 15
Table E.19 Mean Daily Solar Radiation..... 16
Table E.20 Percent Shade 17

LIST OF FIGURES

Figure E.1 Wetted Width versus Flow for Assessment Unit NM-2306.A_020 9
Figure E.2 Wetted Width versus Flow for Assessment Unit NM-2305.A_230 10
Figure E.3 Wetted Width versus Flow for Assessment Unit NM-2305.A_220 11

LIST OF ACRONYMS

4Q3	Four-consecutive day discharge that has a recurrence interval of three years
cfs	Cubic Feet per Second
GIS	Geographic Information Systems
GPS	Global Positioning System
IOWDM	Input and Output for Watershed Data Management
mi^2	Square Miles
^oC	Degrees Celcius
SEE	Standard Error of Estimate
SSTEMP	Stream Segment Temperature
SWSTAT	Surface-Water Statistics
TMDL	Total Maximum Daily Load
USDA	U.S. Department of Agriculture
USGS	U.S. Geological Survey
WinXSPRO	Windows-Based Stream Channel Cross-Section Analysis

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E 1.0 INTRODUCTION

This appendix provides site-specific hydrology, geometry, and meteorological data for input into the Stream Segment Temperature (SSTEMP) Model (Bartholow 2002). Hydrology variables include segment inflow, inflow temperature, segment outflow, and accretion temperature. Geometry variables are latitude, segment length, upstream and downstream elevation, Width's A-term, Width's B-term, and Manning's n. Meterological inputs to SSTEMP Model include air temperature, relative humidity, windspeed, ground temperature, thermal gradient, possible sun, dust coefficient, ground reflectivity, and solar radiation. In the following sections, these parameters are discussed in detail for each assessment unit to be modeled using SSTEMP Model. The assessment units were modeled on the day of the maximum recorded thermograph measurement. The assessment units and modeled dates are defined as follows:

Table E.1 Assessment Units and Modeled Dates

Assessment Unit ID	Assessment Unit Description	Modeled Date
NM-2306.A_020	Coyote Creek (Mora River to Black Lake)	7/8/2002
NM-2305.A_230	Vermejo River (York Canyon to headwaters)	7/8/2002
NM-2305.A_220	Vermejo River (Rail Canyon to York Canyon)	7/12/2002

E 2.0 HYDROLOGY

E2.1 Segment Inflow

This parameter is the *mean daily* flow at the top of the stream segment. If the segment begins at an effective headwater, the flow is entered into SSTEMP Model as zero. Flow data from USGS gages were used when available. To be conservative, the lowest four-consecutive-day discharge that has a recurrence interval of three years but that does not necessarily occur every three years (4Q3) was used as the inflow instead of the mean daily flow. These critical low flows were used to decrease assimilative capacity of the stream to adsorb and disperse solar energy. The 4Q3 would be determined for gaged sites using a log Pearson Type III distribution through "*Input and Output for Watershed Data Management*" (IOWDM) software, Version 4.1 (USGS 2002a) and "*Surface-Water Statistics*" (SWSTAT) software, Version 4.1 (USGS 2002b).

Discharges for ungaged sites on gaged streams were estimated based on methods published by Thomas *et al.* (1997). If the drainage area of the ungaged site is between 50 and 150 percent of the drainage area of the gaged site, the following equation is used:

$$Q_u = Q_g \left(\frac{A_u}{A_g} \right)^{0.5}$$

where,

Q_u = Area weighted 4Q3 at the ungaged site (cubic feet per second [cfs])
Q_g = 4Q3 at the gaged site (cfs)
A_u = Drainage area at the ungaged site (square miles [mi^2])
A_g = Drainage area at the gaged site (mi^2)

Drainage areas for assessment units to which this method was applied are summarized in the following table:

Table E.2 Drainage Areas for Estimating Flow by Drainage Area Ratios

Assessment Unit	USGS Gage	Drainage Area from Gage (mi^2)	Drainage Area from Top of AU (mi^2)	Drainage Area from Bottom of AU (mi^2)	Ratio of DA of Ungaged (upstream) to Gaged Site	Ratio of DA of Ungaged (downstream) to Gaged Site
NM-2306.A_020	07218000	215	24.05	243.49	**11%**[(b)]	113%
NM-2305.A_230	07203000	301	<0.3	171.26	**—**[(a)]	57%
NM-2305.A_220	07203000	301	171.26	343.32	57%	114%

Notes:
[(a)] Assessment unit begins at headwaters.
[(b)] The method developed by Thomas et al. (1997) is not applicable because the drainage area of the ungaged site is less than 50 percent of the drainage area of the gaged site. Therefore, the method developed by Waltemeyer (2002) was used to estimate flows for this assessment unit.

mi^2 = Square miles
USGS = U.S. Geological Survey
AU = Assessment Unit

4Q3 derivations for ungaged streams were based on analysis methods described by Waltemeyer (2002). Two regression equations for estimating 4Q3 were developed based on physiographic regions of New Mexico (i.e., statewide and mountainous regions above 7,500 feet in elevation). The following statewide regression equation is based on data from 50 gaging stations with non-zero discharge (Waltemeyer 2002):

$$4Q3 = 1.2856 \times 10^{-4}\ DA^{0.42}\ P_w^{\ 3.16}$$

where,

4Q3 = Four-day, three-year low-flow frequency (cfs)
DA = Drainage area (mi^2)
P_w = Average basin mean winter precipitation (inches)

The average standard error of estimate (SEE) and coefficient of determination are 126 and 48 percent, respectively, for this regression equation (Waltemeyer 2002). The following regression equation for mountainous regions above 7,500 feet in elevation is based on data from 40 gaging stations with non-zero discharge (Waltemeyer 2002):

$$4Q3 = 7.3287 \times 10^{-5}\ DA^{0.70}\ P_w^{\ 3.58}\ S^{1.35}$$

where,

4Q3 = Four-day, three-year low-flow frequency (cfs)
DA = Drainage area (mi^2)
P_w = Average basin mean winter precipitation (inches)
S = Average basin slope (percent)

The average SEE and coefficient of determination are 94 and 66 percent, respectively, for this regression equation (Waltemeyer 2002). The drainage areas, average basin mean winter precipitation, and average basin slope for assessment units where this regression method was used are presented in the following table:

Table E.3 Parameters for Estimating Flow using USGS Regression Model

Assessment Unit	Regression Model[(a)]	Average Elevation for Assessment Unit (feet)	Mean Basin Winter Precipitation (inches)	Average Basin Slope (unitless)
NM-2306.A_020	Mountainous	8,008	6.61	0.163
NM-2305.A_230	Mountainous	8,684	9.63	0.245
NM-2305.A_220	Mountainous	8,090	7.73	0.23

Notes:
mi^2 = Square miles
[(a)] Waltemeyer (2002)

Based on the methods described above, the following values were estimated for inflow:

Table E.4 Inflow

Assessment Unit	Ref.	4Q3 (cfs)	DAt (mi^2)	DAg (mi^2)	Pw (in)	S unitless	Inflow (cfs)
NM-2306.A_020	(a)	0.48[(1)]	24.05	215	6.61	0.163	0.05
NM-2305.A_230	N/A	–	<0.3	301	9.63	0.245	0.00[(2)]
NM-2305.A_220	(b)	0.99 [(2)]	171.26	301	7.73	0.23	0.56

Notes:
N/A = Not applicable, assessment unit begins at headwaters.
Ref. = Reference
[(a)] Waltemeyer (2002), mountainous
[(b)] Thomas et al. (1997)

cfs = cubic feet per second
mi^2 = Square miles
in = Inches
Pw = Mean winter precipitation
DAt = Drainage area from top of segment
DAb = Drainage area from bottom of segment
DAg = Drainage area from USGS gage
S = Average basin slope
[(1)] Based on period of record for USGS gage-Coyote Creek near Golondrinas, NM (07218000)
[(2)] Inflow is zero because assessment unit begins at headwaters.
[(3)] Based on period of record for USGS gage-Vermejo River near Dawson, NM (07203000)

E2.2 Inflow Temperature

This parameter represents the *mean daily* water temperature at the top of the segment. 2002 data from thermographs positioned at the top of the assessment unit were used when possible. If the segment began at a true headwater, the temperature entered was zero degrees Celcius (^{o}C) (zero flow has zero heat). The following inflow temperatures for impaired assessment units were modeled in SSTEMP:

Table E.5 Mean Daily Water Temperature

Assessment Unit	Upstream Thermograph Location	Inflow Temp. (^{o}C)	Inflow Temp. (^{o}F)
NM-2306.A_020	Coyote Creek at Coyote State Park above USGS gage[1]	17.7	63.9
NM-2305.A_230	None (headwaters)	0	32.0
NM-2305.A_220	Vermejo River above Caliente Canyon	21.6	70.9

Notes:
ºC = Degrees Celcius
ºF = Degrees Farenheit
[1] uppermost thermograph in AU

E2.3 Segment Outflow

Flow data from USGS gages were used when available. To be conservative, the 4Q3 was used as the segment outflow. These critical low flows were used to decrease assimilative capacity of the stream to adsorb and disperse solar energy. Outflow was estimated using the methods described in Section 2.1. The following table summarizes 4Q3s used in the SSTEMP Model:

Table E.6 Segment Outflow

Assessment Unit	Ref.	4Q3 (cfs)	DAb (mi^2)	DAg (mi^2)	Pw (in)	S unitless	Outflow (cfs)
NM-2306.A_020	(a)	0.48	243.49	215	6.61	0.163	0.54
NM-2305.A_230	(a)	0.99	171.26	301	9.63	0.245	0.56
NM-2305.A_220	(a)	0.99	343.32	301	7.73	0.23	1.13

Notes:
Ref. = Reference
(a) Thomas et al. (1997)

cfs = cubic feet per second
mi^2 = Square miles
in = Inches
Pw = Mean winter precipitation
DAb = Drainage area from bottom of segment
DAg = Drainage area from USGS gage
S = Average basin slope
(c) USGS gage-Coyote Creek near Golondrinas, NM (07218000)
(d) USGS gage-Vermejo River near Dawson, NM (07203000)

E2.4 Accretion Temperature

The temperature of the lateral inflow, barring tributaries, generally should be the same as groundwater temperature. In turn, groundwater temperature may be approximated by the mean annual air temperature. Mean annual air temperature for 2002 was used in the absence of measured data. The following table presents the mean annual air temperature for each assessment unit:

Table E.7 Mean Annual Air Temperature as an Estimate for Accretion Temperature

Assessment Unit	Ref.	Mean Annual Air Temperature (^oC)	Mean Annual Air Temperature (^oF)
NM-2306.A_020	(a)	12.36	54.24
NM-2305.A_230	(a)	12.36	54.24
NM-2305.A_220	(a)	12.36	54.24

Notes:
Ref. = References for Weather Station Data are as follows:
(a) *New Mexico State University Climate Network (Raton METAR, Elevation 1,936 meters; Latitude 36° 44' 0" N, Longitude 104° 30' 0" W),* ***2002***
ºF = Degrees Farenheit
ºC = Degrees Celcius

E 3.0 GEOMETRY

E3.1 Latitude

Latitude refers to the position of the stream segment on the earth's surface. Latitude is generally determined in the field with a global positioning system (GPS) unit. Latitude for each assessment unit is summarized below:

Table E.8 Assessment Unit Latitude

Assessment Unit	Latitude (decimal degrees)
NM-2306.A_020	36.09
NM-2305.A_230	36.90
NM-2305.A_220	36.74

E3.2 Dam at Head of Segment

The following assessment units have a dam at the upstream end of the segment with a constant, or nearly constant diel release temperature:

Table E.9 Presence of Dam at Head of Segment

Assessment Unit	Dam?
NM-2306.A_020	No
NM-2305.A_230	No
NM-2305.A_220	No

E3.3 Segment Length

Segment length was determined with National Hydrographic Dataset Reach Indexing GIS tool. The segment lengths are as follows:

Table E.10 Segment Length

Assessment Unit	Length (miles)
NM-2306.A_020	35.26
NM-2305.A_230	25.05
NM-2305.A_220	23.55

E3.4 Upstream Elevation

The following upstream elevations were determined with National Hydrographic Dataset Reach Indexing GIS tool.

Table E.11 Upstream Elevations

Assessment Unit	Upstream Elevation (feet)
NM-2306.A_020	8,528
NM-2305.A_230	10,740
NM-2305.A_220	7,105

E3.5 Downstream Elevation

The following downstream elevations were determined with National Hydrographic Dataset Reach Indexing GIS tool.

Table E.12 Downstream Elevations

Assessment Unit	Downstream Elevation (feet)
NM-2306.A_020	6,720
NM-2305.A_230	7,105
NM-2305.A_220	6,325

E3.6 Width's A and Width's B Term

Width's B Term was calculated as the slope of the regression of the natural log of width and the natural log of flow. Width-versus-flow regression analyses were prepared by entering cross-section field data into a Windows-Based Stream Channel Cross-Section Analysis (WINXSPRO 3.0) Program (U.S. Department of Agriculture [USDA] 2005). Theoretically, the Width's A Term is the untransformed Y-intercept. However, because the width versus discharge relationship tends to break down at very low flows, the Width's B-Term was first calculated as the slope and Width's A-Term was estimated by solving for the following equation:

$$W = A \times Q^{B}$$

where,

W = Known width (feet)
A = Width's A-Term (seconds per square foot)
Q = Known discharge (cfs)
B = Width's B-Term (unitless)

The following table summarizes Width's A- and B-Terms for assessment units requiring temperature TMDLs:

Table E.13 Width's A and Width's B Terms

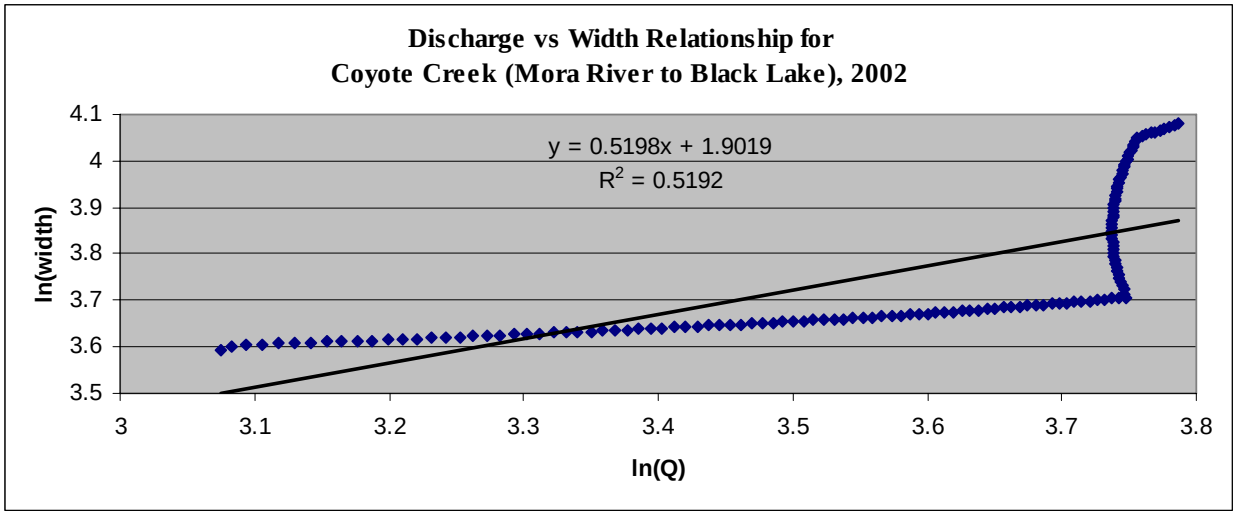
Assessment Unit	Width's B-Term	Width's A-Term [1]
NM-2306.A_020	0.520	7.35
NM-2305.A_230	1.11	0.337
NM-2305.A_220	1.49	0.082

[1] *A=e^constant from regression*

The following figures present the detailed calculations for the Width's B-Term.

Measurements were collected at one site within these assessment units. The regression of natural log of width and natural log of flow for each location is as follows:

Figure E.1 Wetted Width versus Flow for Assessment Unit NM-2306.A_020



SUMMARY OUTPUT

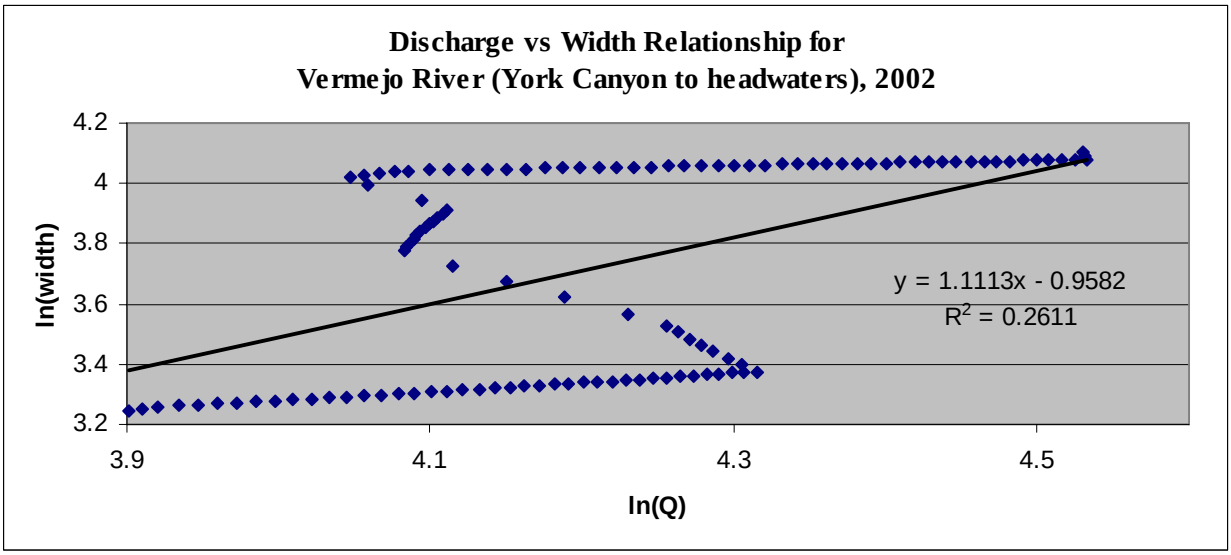
Regression Statistics	
Multiple R	0.720535668
R Square	0.519171648
Adjusted R Square	0.515712452
Standard Error	0.104807943
Observations	141

ANOVA

	df	*SS*	*MS*	*F*	*Significance F*
Regression	1	1.648633408	1.648633	150.0845	7.37051E-24
Residual	139	1.526873985	0.010985		
Total	140	3.175507393			

	Coefficients	*Standard Error*	*t Stat*	*P-value*	*Lower 95%*	*Upper 95%*	*Lower 95.0%*	*Upper 95.0%*
Intercept	1.901878299	0.151914739	12.51938	1.5E-24	1.601515866	2.202241	1.601515866	2.202240731
X Variable 1	0.519783763	0.042428225	12.2509	7.37E-24	0.435895624	0.603672	0.435895624	0.603671902

Figure E.2 Wetted Width versus Flow for Assessment Unit NM-2305.A_230



SUMMARY OUTPUT

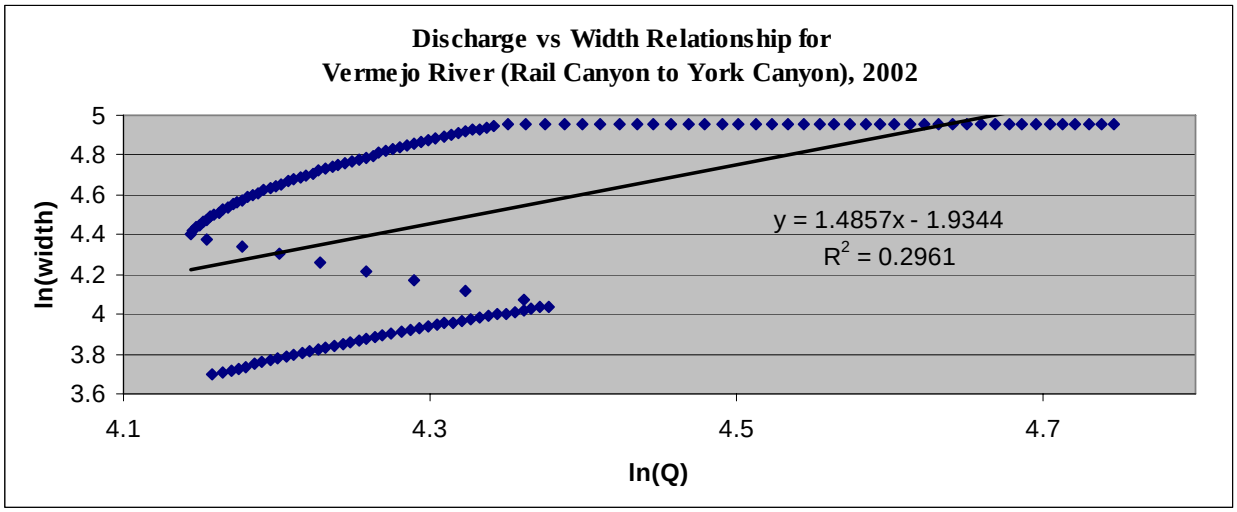
Regression Statistics	
Multiple R	0.511010308
R Square	0.261131534
Adjusted R	0.254650232
Standard E	0.294979955
Observatio	116

ANOVA

	df	*SS*	*MS*	*F*	*Significance F*
Regressior	1	3.505758953	3.505759	40.28998	4.5963E-09
Residual	114	9.91950185	0.087013		
Total	115	13.4252608			

	Coefficients	*Standard Error*	*t Stat*	*P-value*	*Lower 95%*	*Upper 95%*	*Lower 95.0%*	*Upper 95.0%*
Intercept	-0.958185456	0.738032046	-1.298298	0.196805	-2.420221208	0.50385	-2.420221208	0.503850296
X Variable	1.111263287	0.175072707	6.347439	4.6E-09	0.764445614	1.458081	0.764445614	1.458080959

Figure E.3 Wetted Width versus Flow for Assessment Unit NM-2305.A_220



SUMMARY OUTPUT

Regression Statistics	
Multiple R	0.544138535
R Square	0.296086745
Adjusted R	0.291022621
Standard E	0.379835714
Observatio	141

ANOVA

	df	*SS*	*MS*	*F*	*ignificance F*
Regressior	1	8.435410383	8.43541	58.46751	3.09E-12
Residual	139	20.05424856	0.144275		
Total	140	28.48965895			

	Coefficients	*Standard Error*	*t Stat*	*P-value*	*Lower 95%*	*Upper 95%*	*Lower 95.0%*	*Upper 95.0%*
Intercept	-1.934390545	0.843171856	-2.294183	0.023279	-3.601491	-0.26729	-3.60149113	-0.267289959
X Variable	1.485702409	0.194300768	7.646405	3.09E-12	1.101535	1.86986955	1.101535265	1.869869552

E3.7 Manning's n or Travel Time

Site-specific values generated from WINXSPRO were used for Manning's n. The following table summarizes the input values:

Table E.14 Manning's n Values

Assessment Unit	Manning's n
NM-2306.A_020	0.019
NM-2305.A_230	0.028 [a]
NM-2305.A_220	0.049 [b]

[a] data from site below confluence with Leandro Creek
[b] data from site below York Canyon Creek

E 4.0 METEOROLOGICAL PARAMETERS

E4.1 Air Temperature

This parameter is the mean daily air temperature for the assessment unit (or average daily temperature at the mean elevation of the assessment unit). Air temperature will usually be the single most important factor in determining mean daily water temperature. Air temperatures are usually measured directly (in the shade) using air thermographs and adjusted to what the temperature would be at the mean elevation of the assessment unit. However, there were no air thermographs deployed in 2002 during this study. The following table summarizes mean daily air temperatures for each assessment unit (for its modeled date) requiring a temperature Total Maximum Daily Load (TMDL):

Table E.15 Mean Daily Air Temperature

Assessment Unit	Elevation at Air Thermograph[1] Location (meters)	Measured Mean Daily Air Temperature (°C)	Mean Elevation for Assessment Unit (meters)	Adjusted Mean Daily Air Temperature (°C)	Adjusted Mean Daily Air Temperature (°F)
NM-2306.A_020	1,936	22.56	2,440	19.25	66.65
NM-2305.A_230	1,936	22.56	2,646	17.90	64.22
NM-2305.A_220	1,936	23.30	2,465	19.83	67.69

Notes:
°F = Degrees Farenheit
°C = Degrees Celcius
[1] *No air thermographs deployed. New Mexico State University Climate Network (Raton METAR, Elevation 1,936 meters; Latitude 36° 44' 0" N, Longitude 104° 30' 0" W),* ***2002***

The adiabatic lapse rate was used to correct for elevational differences from the met station:

$$T_a = T_o + C_t \times (Z - Z_o)$$

where,

T_a = air temperature at elevation E (°C)
T_o = air temperature at elevation E_o (°C)
Z = mean elevation of segment (meters)
Z_o = elevation of station (meters)
C_t = moist-air adiabatic lapse rate (-0.00656 °C/meter)

E4.2 Maximum Air Temperature

Unlike the other variables, the maximum daily air temperature overrides only if the check box is checked. If the box is not checked, the SSTEMP Model estimates the maximum daily air temperature from a set of empirical coefficients (Theurer et al., 1984 as cited in Bartholow 2002)

and will print the result in the grayed data entry box. A value cannot be entered unless the box is checked.

E4.3 Relative Humidity

Relative humidity data were obtained from the New Mexico State University Climate Network (http://weather.nmsu.edu/data/data.htm). The data were corrected for elevation and temperature using the following equation:

$$R_h = R_o \times \left(1.0640^{(To-Ta)}\right) \times \left(\frac{T_a + 273.16}{T_o + 273.16}\right)$$

where,

R_h = relative humidity for temperature T_a (decimal)
R_o = relative humidity at station (decimal)
T_a = air temperature at segment (°C)
T_o = air temperature at station (°C)

The following table presents the adjusted mean daily relative humidity for each assessment unit:

Table E.16 Mean Daily Relative Humidity

Assessment Unit	Ref.	Mean Daily Air Temp. at Weather Station (°C)	Mean Daily Air Temperature at AU (°C)	Mean Daily Relative Humidity at Weather Station (percent)	Mean Daily Relative Humidity for AU (percent)
NM-2306.A_020	(a)	22.56	19.25	49.095	59.61
NM-2305.A_230	(a)	22.56	17.90	49.095	64.52
NM-2305.A_220	(b)	23.30	19.83	45.673	55.98

Notes:
Ref. = References for Weather Station Data are as follows:
(a) *New Mexico State University Climate Network (Raton METAR, Elevation 1,936 meters; Latitude 36° 44' 0" N, Longitude 104° 30' 0" W),* ***July 8, 2002***
(b) *New Mexico State University Climate Network (Raton METAR, Elevation 1,936 meters; Latitude 36° 44' 0" N, Longitude 104° 30' 0" W),* ***July 12, 2002***
AU = Assessment Unit
°C = Degrees Celcius

E4.4 Wind Speed

Average daily wind speed data were obtained from the New Mexico State University Climate Network (http://weather.nmsu.edu/data/data.htm). The following table presents the mean daily wind speed for each assessment unit:

Table E.17 Mean Daily Wind Speed

Assessment Unit	Ref.	Mean Daily Wind Speed (miles per hour)	Date
NM-2306.A_020	(a)	12.814	7/8/2002
NM-2305.A_230	(a)	12.814	7/8/2002
NM-2305.A_220	(a)	7.862	7/12/2002

Notes:
Ref. = References for Weather Station Data are as follows:
(a) *Wind speed data not available for Raton METAR. New Mexico State University Climate Network (Clayton, Elevation 1,515 meters; Latitude 36° 28' 4.02" N, Longitude 103° 5' 17.88" W)*

E4.5 Ground Temperature

Mean annual air temperature data for 2002 were used in the absence of measured data. The following table presents the mean annual air temperature for each assessment unit:

Table E.18 Mean Annual Air Temperature as an Estimate for Ground Temperature

Assessment Unit	Ref.	Mean Annual Air Temperature (^oC)	Mean Annual Air Temperature (^oF)
NM-2306.A_020	(a)	12.36	54.24
NM-2305.A_230	(a)	12.36	54.24
NM-2305.A_220	(a)	12.36	54.24

Ref. = References for Weather Station Data are as follows:
(b) *New Mexico State University Climate Network (Raton METAR, Elevation 1,936 meters; Latitude 36° 44' 0" N, Longitude 104° 30' 0" W),* ***2002***

^oF = Degrees Farenheit
^oC = Degrees Celcius

E4.6 Thermal Gradient

The default value of 1.65 was used in the absence of measured data.

E4.7 Possible Sun

Percent possible sun for Albuquerque is found at the Western Regional Climate Center web site http://www.wrcc.dri.edu/htmlfiles/westcomp.sun.html#NEW%20MEXICO. The percent possible sun is 76 percent for July for Albuquerque as there were no data for the Clayton station.

E4.8 Dust Coefficient

If a value is entered for solar radiation, SSTEMP Model will ignore the dust coefficient and ground reflectivity and "override' the internal calculation of solar radiation. Solar radiation data are available from the New Mexico State University Climate Network (see Section 4.10).

E4.9 Ground Reflectivity

If a value is entered for solar radiation, SSTEMP Model will ignore the dust coefficient and ground reflectivity and "override' the internal calculation of solar radiation. Solar radiation data are available from the New Mexico State University Climate Network (see Section 4.10).

E4.10 Solar Radiation

Because solar radiation data were obtained from an external source of ground level radiation, it was assumed that about 90% of the ground-level solar radiation actually enters the water. Thus, the recorded solar measurements were multiplied by 0.90 to get the number to be entered into the SSTEMP Model. The following table presents the measured solar radiation at Clayton for 2002 as there were no data available for the Raton METAR station:

Table E.19 Mean Daily Solar Radiation

Assessment Unit	Ref.	Date	Mean Solar Radiation (L/day)	Mean Solar Radiation x 0.90 (L/day)
NM-2306.A_020	(a)	7-8-2002	735	661.5
NM-2305.A_230	(a)	7-8-2002	735	661.5
NM-2305.A_220	(a)	7-12-2002	733.992	660.59

Ref. = References for Weather Station Data are as follows:

(a) *Solar radiation data not available for Raton METAR. New Mexico State University Climate Network (Clayton, Elevation 1,515 meters; Latitude 36° 28' 4.02" N, Longitude 103° 5' 17.88" W)*

E 5.0 SHADE

Percent shade was estimated for the assessment units using field estimations per geomorphological survey field notes from 2002. The measurements may have also been averaged along with visual estimates using USGS digital orthophoto quarter quadrangles downloaded from New Mexico Resource Geographic Information System Program (RGIS), online at http://rgis.unm.edu/. This parameter refers to how much of the segment is shaded by vegetation, cliffs, etc. The following table summarizes percent shade for each assessment unit:

In a 2002 study, Optional Shading Parameters and concurrent densiometer readings were measured at seventeen stations in order to compare modeling results from the use of these more extensive data sets to modeling results using densiometer readings as an estimate of Total Shade. The estimated value for Total Shade was within 15% of the calculated value in all cases. Estimated values for Maximum Temperatures differed by less than 0.5% in all cases. The Optional Shading Parameters are dependent on the exact vegetation at each cross section, thus requiring multiple cross sections to determine an accurate estimate for vegetation at a reach scale. Densiometer readings are less variable and less inclined to measurement error in the field. Aerial photos are examined and considered whenever available.

Table E.20 Percent Shade

Assessment Unit	Percent Shade
NM-2306.A_020	<1% and 42% [a]
NM-2305.A_230	0% [b]
NM-2305.A_220	0% [c]

[a] data from site at Thal Ranch and Harold Brock Fishing Area
[b] data from site below confluence with Leandro Creek
[c] data from site below York Canyon Creek

E 6.0 REFERENCES

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